

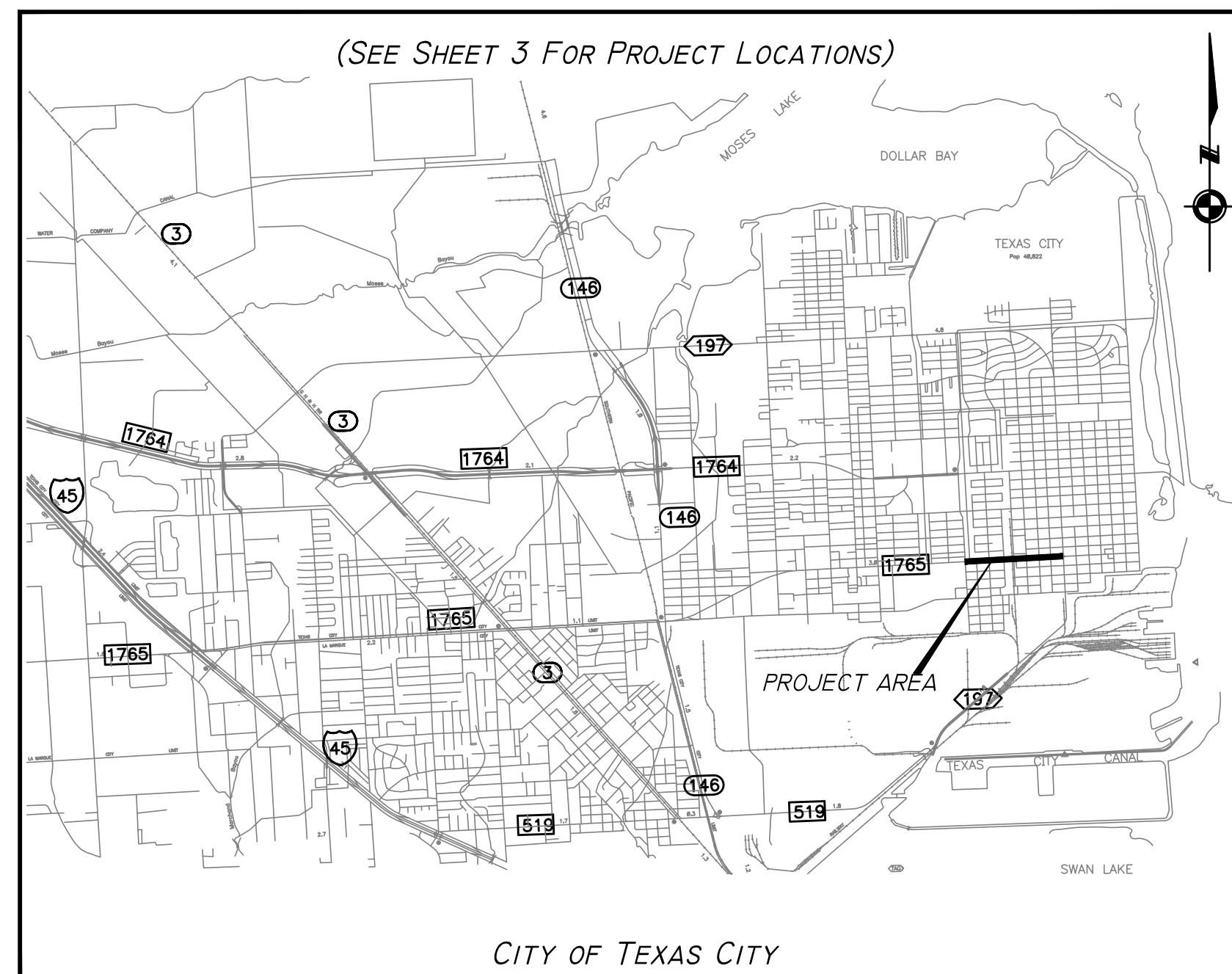
Galveston County, Texas

Texas Avenue Reconstruction

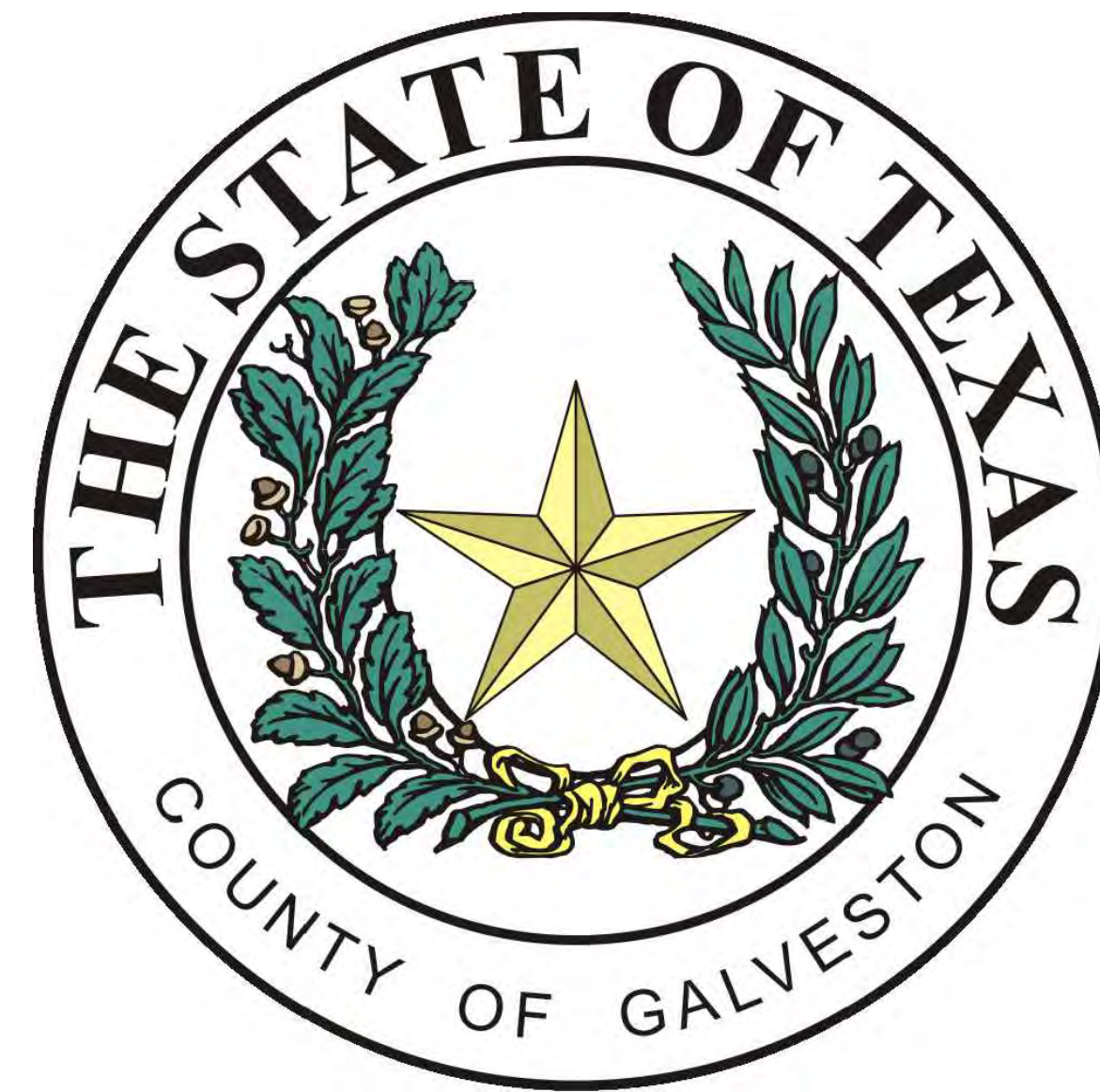
14th Street to Loop 197

October, 2019

DRAWINGS INDEX



LOCATION MAP
Not to Scale



COUNTY JUDGE

Mark Henry

COMMISSIONERS

Darrell Appfel - Precinct 1
Joe Giusti - Precinct 2

Stephen D. Holmes - Precinct 3
Ken Clark - Precinct 4

COUNTY ENGINEER

Michael C. Shannon, P.E.

ASSISTANT COUNTY ENGINEER

Nancy Baher, P.E.

<u>SHEET NO.</u>	<u>DESCRIPTION</u>
1.	COVER SHEET
2.	GENERAL NOTES I
3.	GENERAL NOTES II
4.	OVERALL LAYOUT PLAN I
5.	SURVEY CONTROL MAP I
6.	DRAINAGE AREA MAP
6A.	DRAINAGE CALCULATIONS
6B.	TYPICAL SECTION
7.	TEXAS AVENUE P&P (STA. 1+00 TO STA. 6+00)
8.	TEXAS AVENUE P&P (STA. 6+00 TO STA. 10+50)
9.	TEXAS AVENUE P&P (STA. 10+50 TO STA. 15+50)
10.	TEXAS AVENUE P&P (STA. 15+50 TO STA. 19+50)
11.	TEXAS AVENUE P&P (STA. 19+50 TO STA. 24+00)
12.	TEXAS AVENUE P&P (STA. 24+00 TO STA. 28+50)
13.	TEXAS AVENUE P&P (STA. 28+50 TO STA. 33+00)
14.	TEXAS AVENUE P&P (STA. 33+00 TO STA. 37+50)
15.	TEXAS AVENUE P&P (STA. 37+50 TO END)
16.	13TH STREET P&P (STA. 0+00 TO END)
17.	12TH STREET P&P (STA. 0+00 TO END)
18.	11TH STREET P&P (STA. 0+00 TO END)
19.	10TH STREET P&P (STA. 0+00 TO END)
20.	8TH STREET P&P (STA. 0+00 TO END)
21.	7TH STREET P&P (STA. 0+00 TO END)
22.	SWPPP
23.	SWPPP DETAILS
24.	TRAFFIC LAYOUT PHASE I - SHEET I
25.	TRAFFIC LAYOUT PHASE I - SHEET II
26.	TRAFFIC LAYOUT PHASE I - SHEET III
27.	TRAFFIC LAYOUT PHASE II - SHEET I
28.	TRAFFIC LAYOUT PHASE II - SHEET II
29.	TRAFFIC LAYOUT PHASE II - SHEET III
30.	TRAFFIC LAYOUT PHASE III
31.	TRAFFIC LAYOUT PHASE IV
32.	TRAFFIC SIDE STREET LAYOUT & DETOUR
33.	TRAFFIC CONTROL DETAILS
34.	STRIPING LAYOUT I
35.	STRIPING LAYOUT II
36.	STRIPING DETAILS
37.	PAVEMENT DETAILS I
38.	PAVEMENT DETAILS II
39.	PAVEMENT DETAILS III
40.	DRAINAGE DETAILS I
41.	DRAINAGE DETAILS II
42.	DRAINAGE DETAILS III
43.	DRAINAGE DETAILS IV
44.	JUNCTION BOX A1
45.	JUNCTION BOX A2
46.	JUNCTION BOX A3
47.	JUNCTION BOX A4
48.	JUNCTION BOX A5
49.	JUNCTION BOX A6
50.	STRUCTURAL GENERAL NOTES
51.	STRUCTURAL TYPICAL DETAILS
52.	PROJECT SIGN DETAIL

TO ARRANGE FOR LINES TO BE TURNED OFF OR MOVED, CALL CENTERPOINT ENERGY AT 713-207-2222

NOTICE:
For your safety, you are required by Texas Law to call 811 at least 48 hours before you dig so that underground line can be marked. This verification does not fulfill your obligation to call 811.

VERIFICATION OF PRIVATE UTILITY LINES

Date _____

CenterPoint Energy/Natural Gas Facilities Verification ONLY.
(This signature verifies that you have shown CNP Natural Gas lines correctly - not to be used for conflict verification.) (Gas service lines are not shown.)
Signature valid for six months.

Date _____

Texas New Mexico Power Co.
(Approved Only for Crossing Underground Ductlines, Unless Otherwise Noted.)
Valid at Time of Review Only.

AT&T

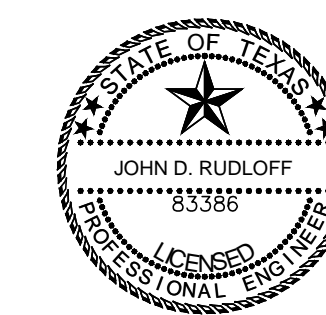
Date _____

Approval for AT&T Texas/SWBT underground conduit facilities only.
Signature valid for one year.

ARKK ENGINEERS

7322 Southwest Freeway, Suite 1040 • Houston, Texas 77074
(713) 400-2755 • Fax (713) 400-2754 • www.arkkengineers.com • TX PE Firm No. 13872

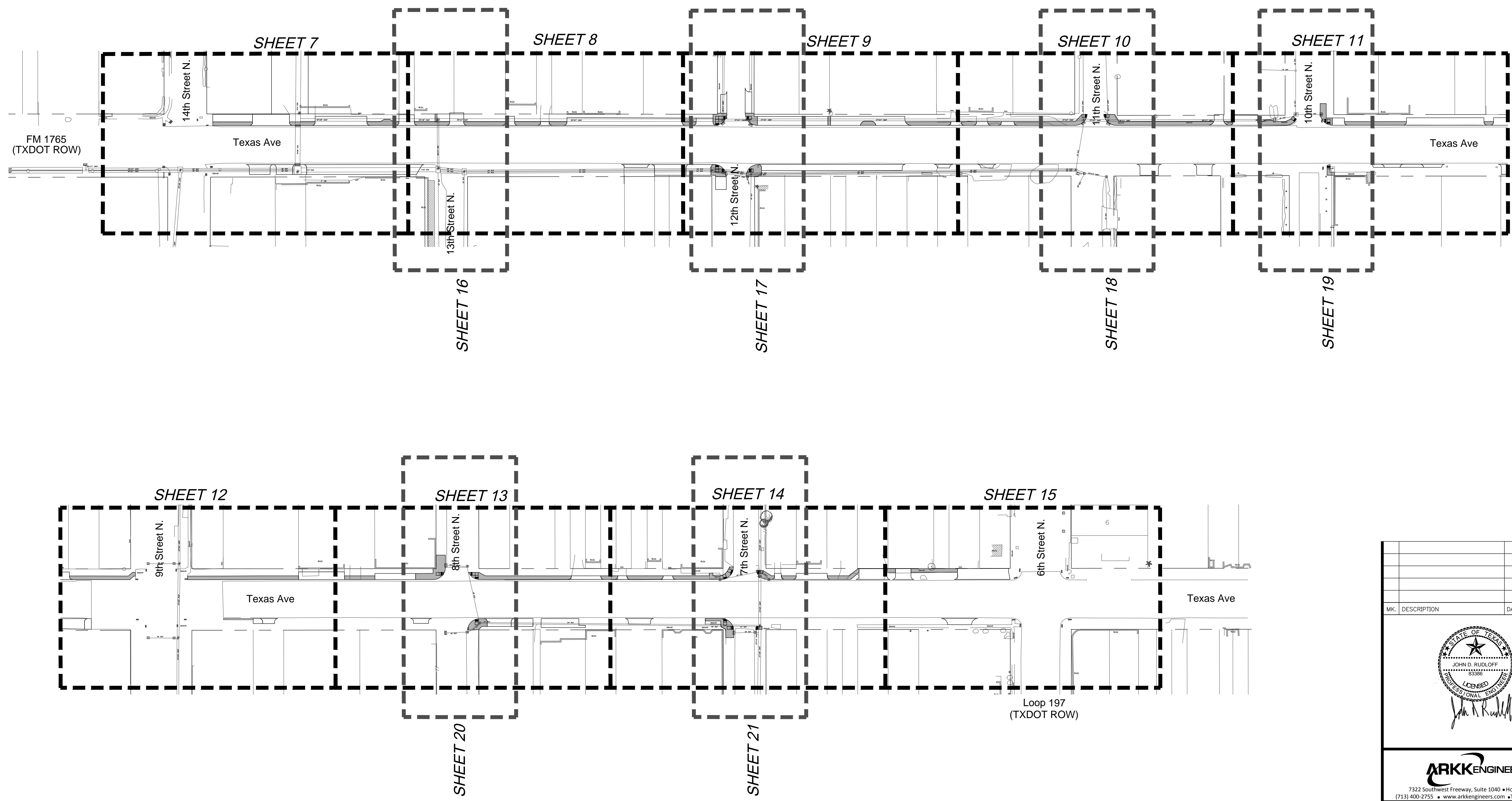
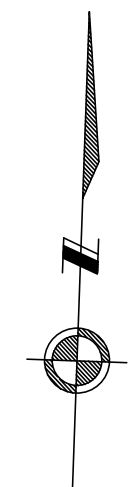
ARKK JOB NO. 18-015



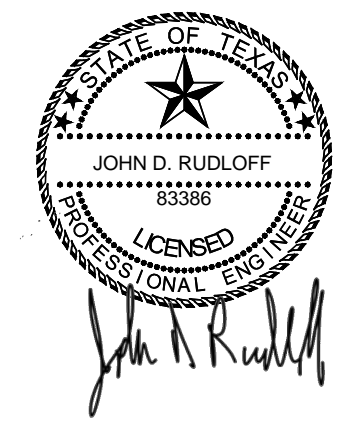
SUBMITTED BY:

John D. Rudloff
JOHN D. RUDLOFF, P.E.
ARKK ENGINEERS, LLC

DATE: 10/14/2019



MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19

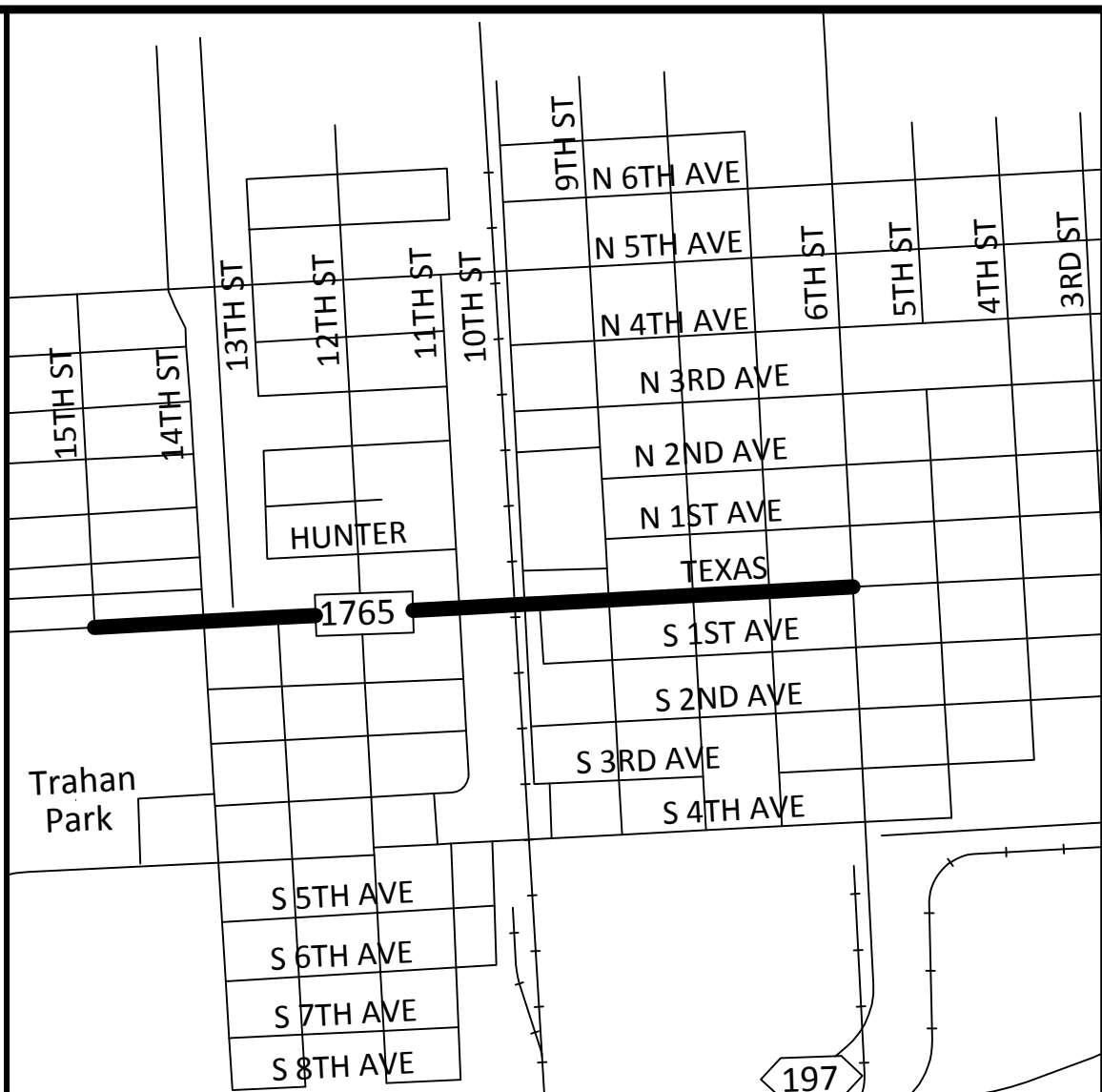
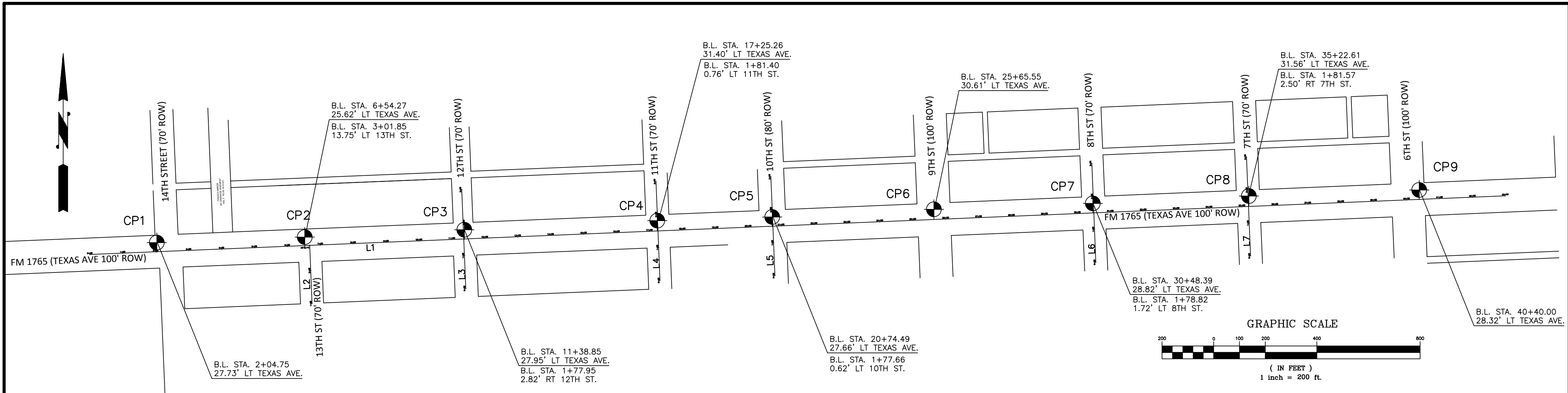
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Galveston County, Texas

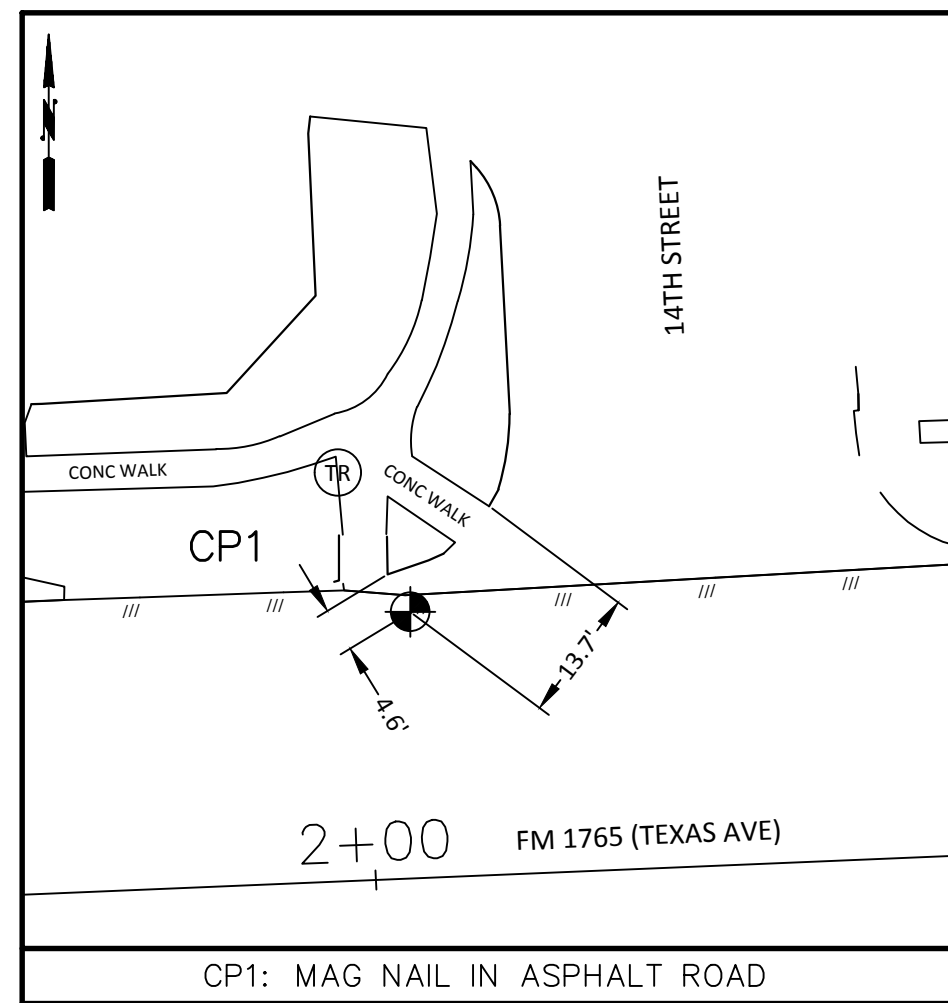
Texas Avenue Reconstruction

Overall Layout Plan

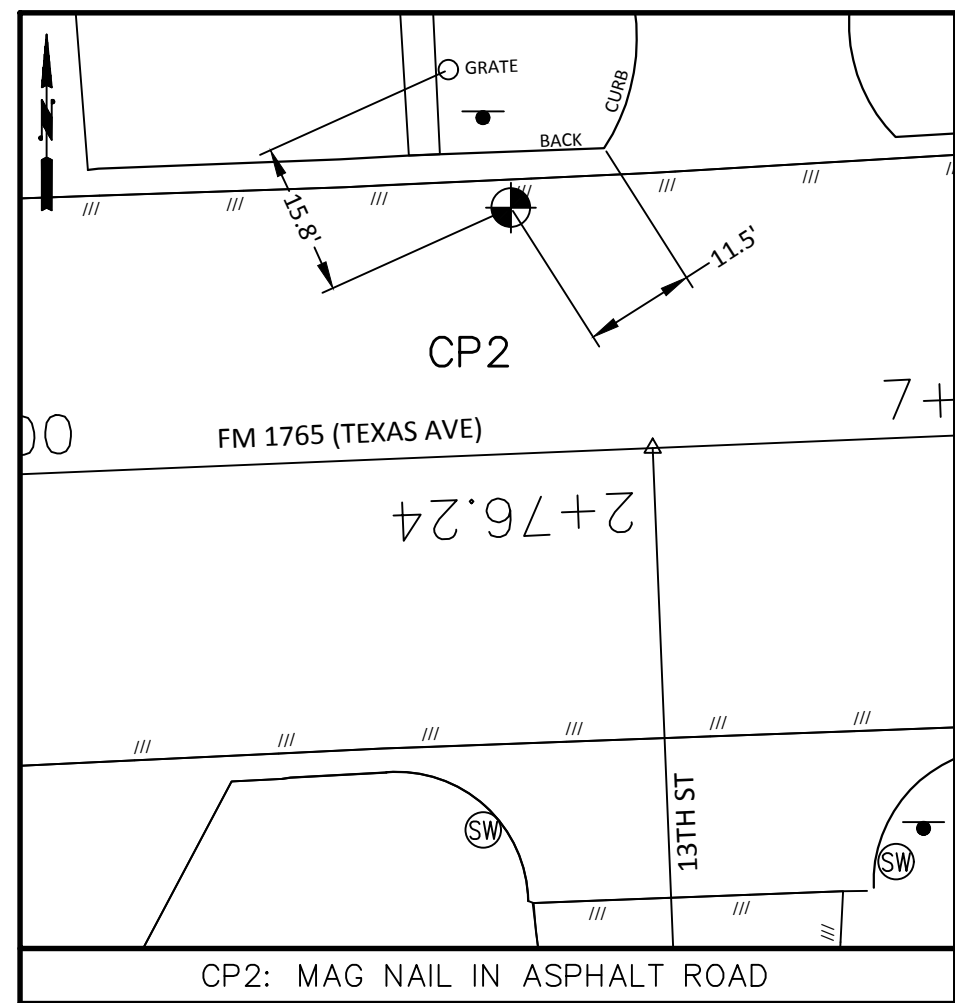
Job No.: 18-015	Scale: HORZ: 1" = 80'	SHEET
Date: September, 2019	VERT:	4
Dwn By: D. Fattig		OF 52
Chkd By: J. Rudloff		



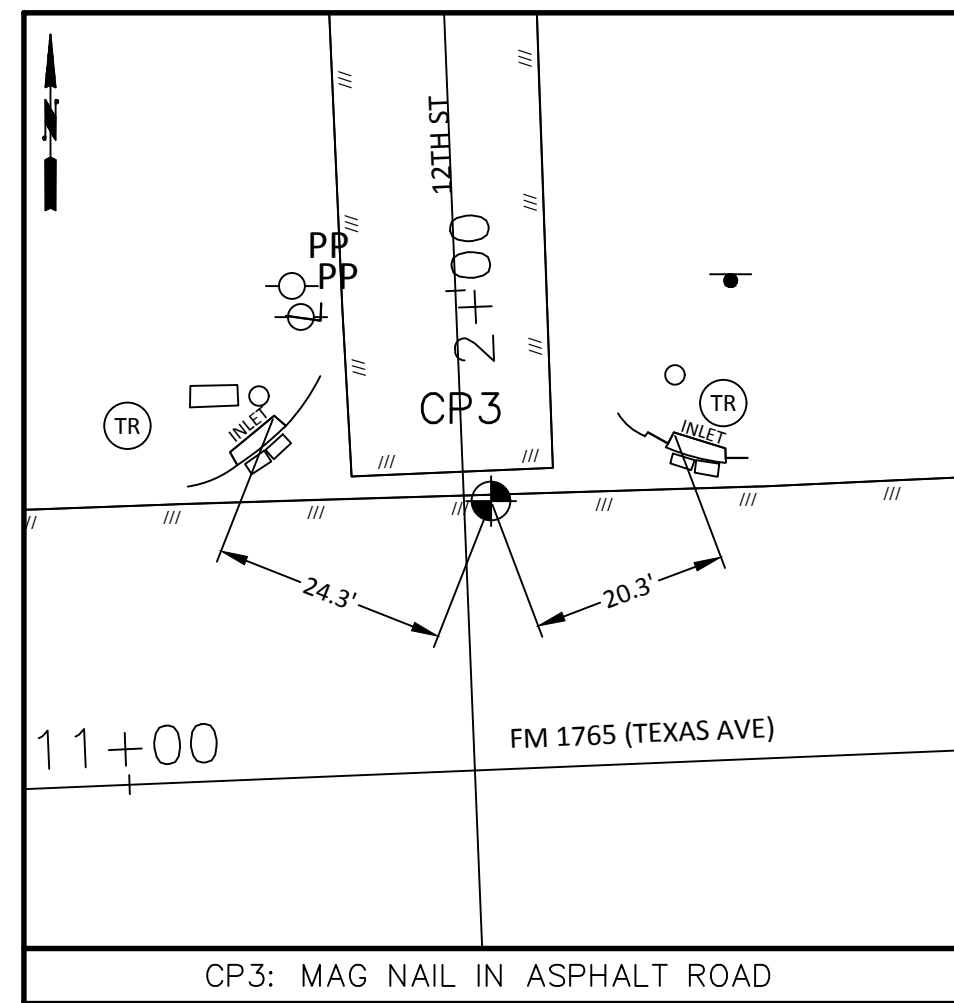
VICINITY MAP N.T.S.



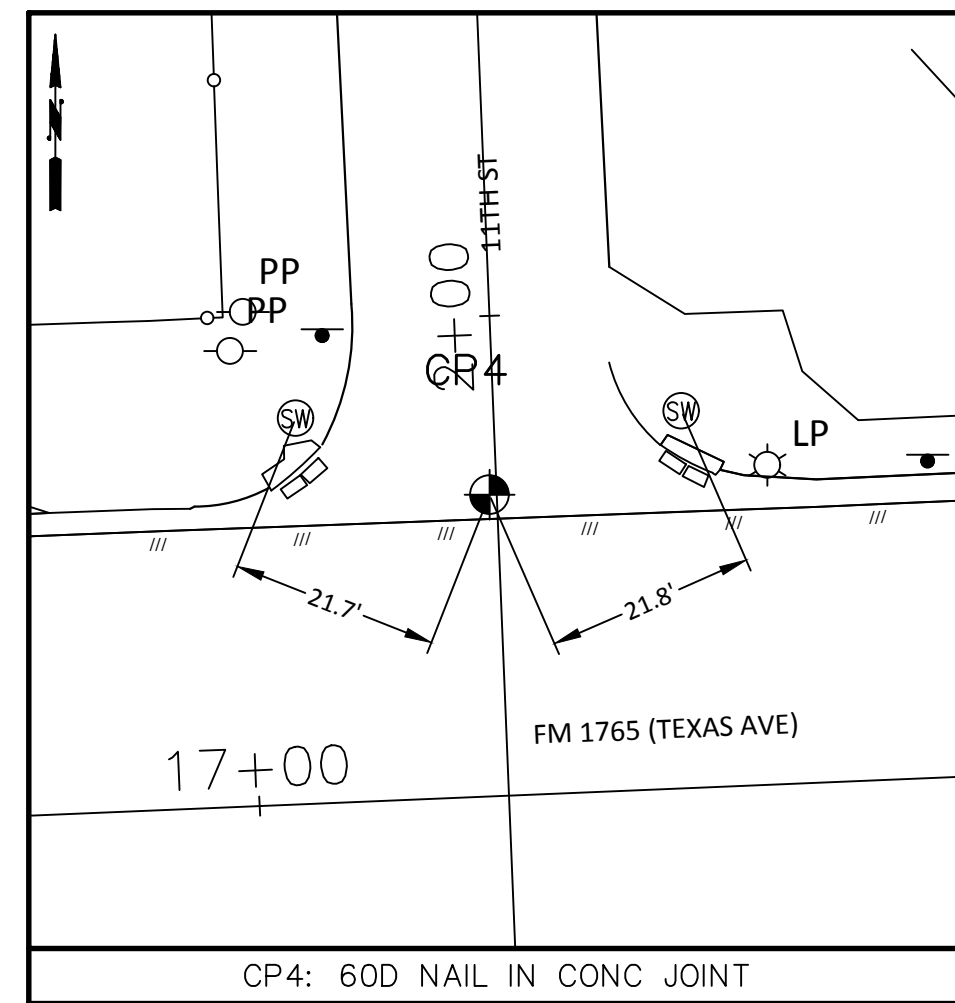
CP1: MAG NAIL IN ASPHALT ROAD



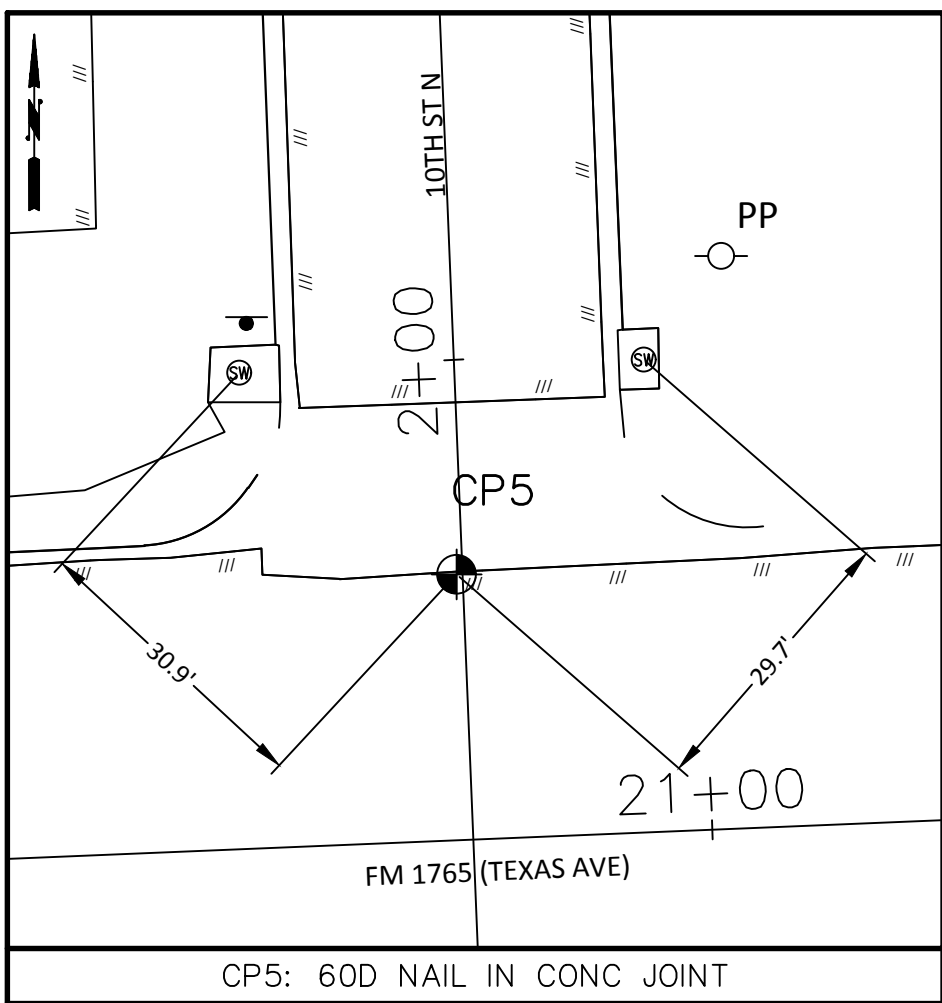
CP2: MAG NAIL IN ASPHALT ROAD



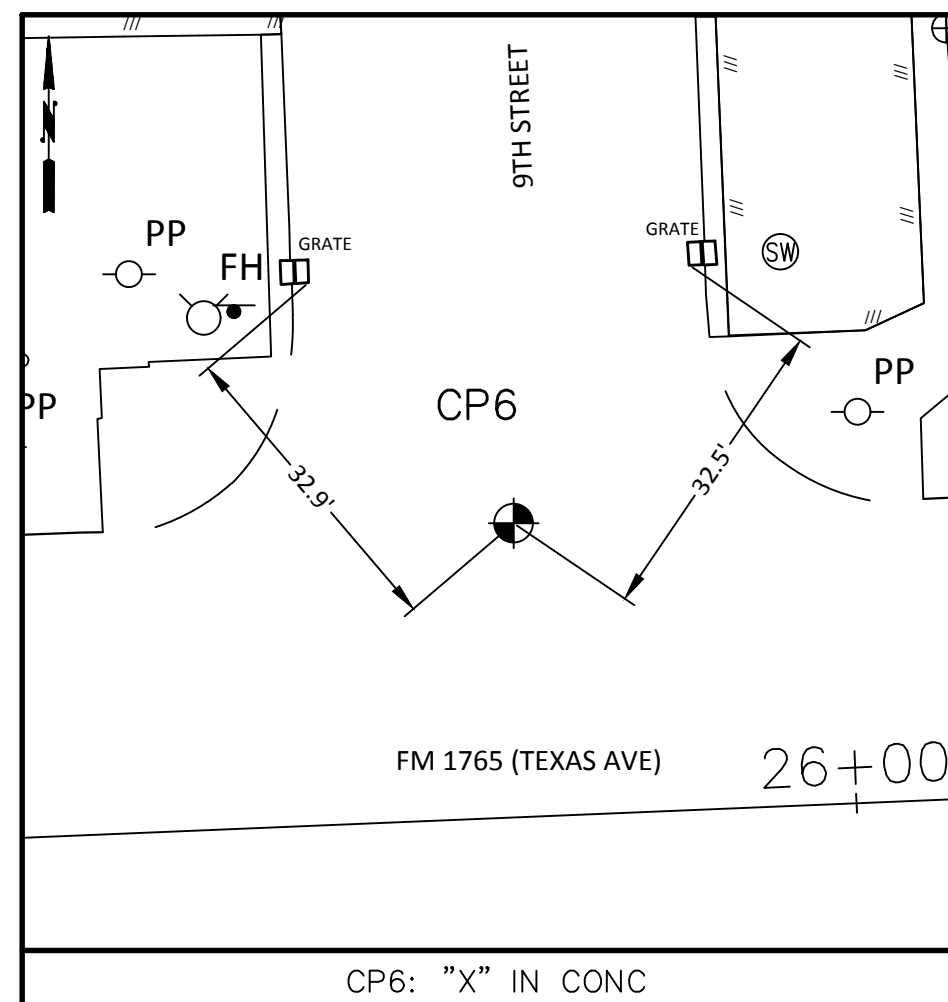
CP3: MAG NAIL IN ASPHALT ROAD



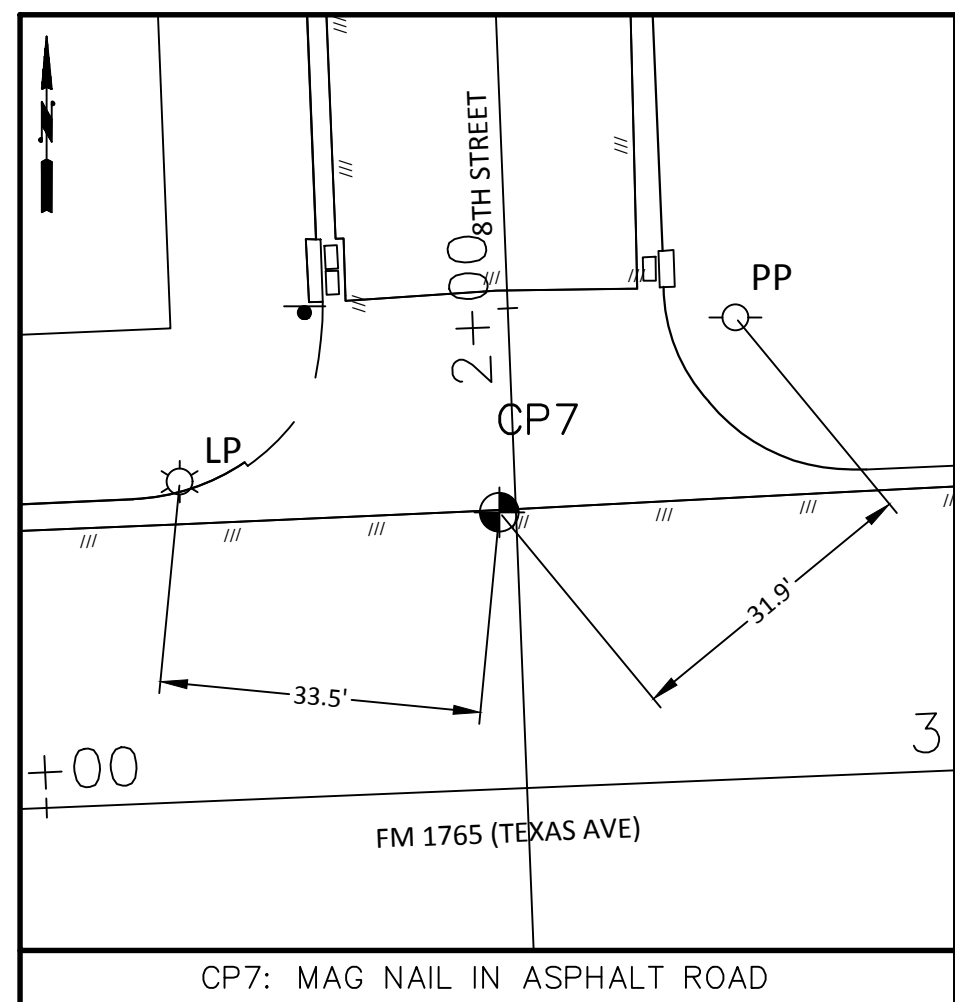
CP4: 60D NAIL IN CONC JOINT



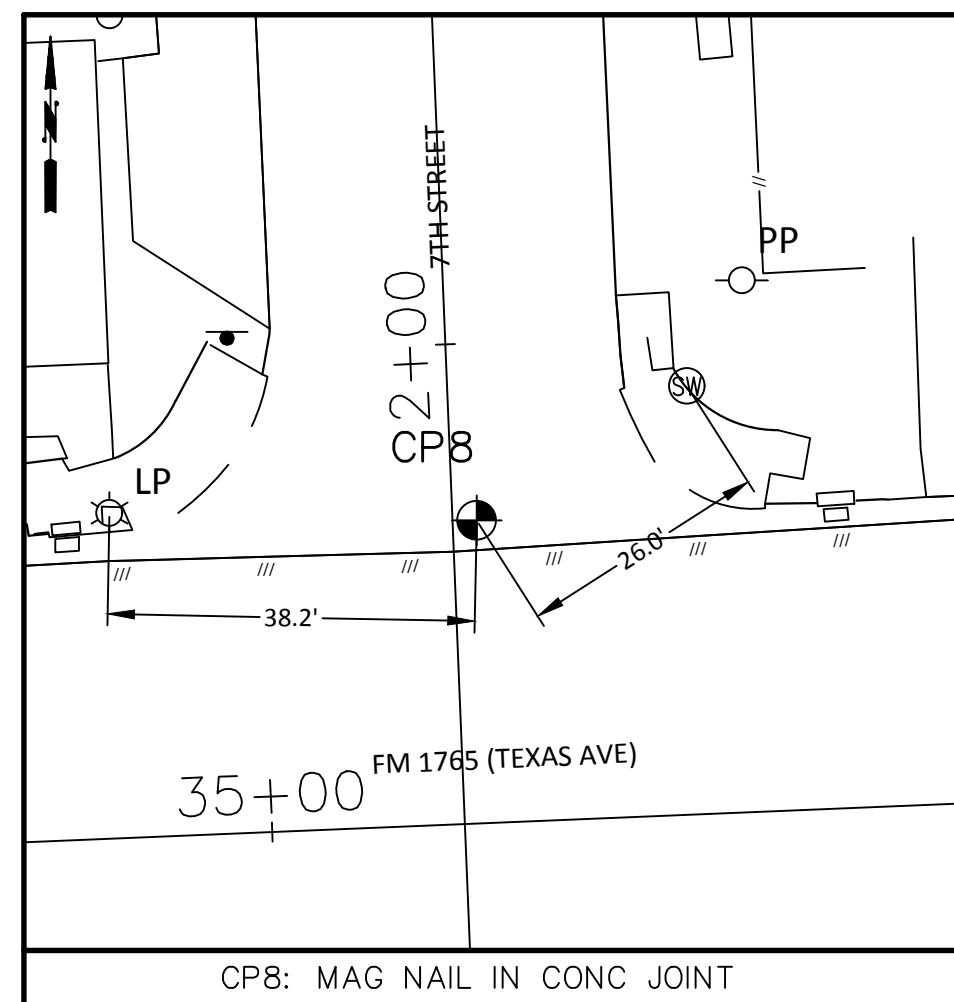
CP5: 60D NAIL IN CONC JOINT



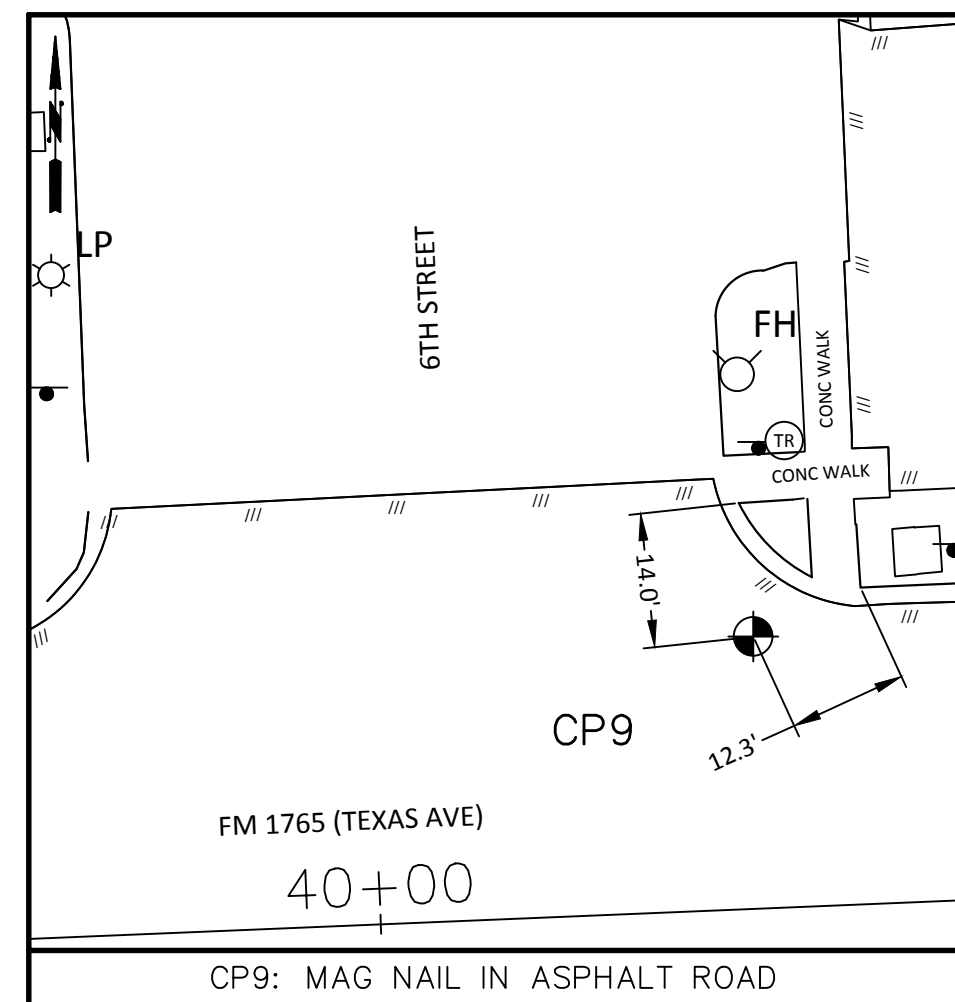
CP6: "X" IN CONC



CP7: MAG NAIL IN ASPHALT ROAD



CP8: MAG NAIL IN CONC JOINT



CP9: MAG NAIL IN ASPHALT ROAD

BENCHMARK
 DATUM: NAVD88 GEOID 12B
 PRIMARY: NGS CONTROL POINT PID A16399 - HGCS058
 RESET ELEV.= 7.82

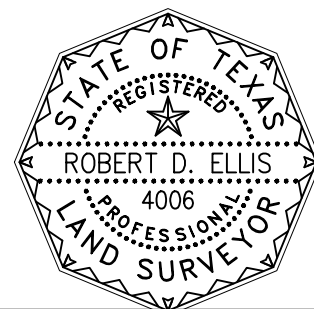
CP#	NORTHING	EASTING	ELEVATION IN FEET	DESCRIPTION
CP1	13709898.50	3269261.52	6.93	MAG NAIL
CP2	13709915.02	3269710.75	6.69	MAG NAIL
CP3	13709937.43	3270194.81	6.11	MAG NAIL
CP4	13709965.18	3270780.57	6.31	60D NAIL
CP5	13709975.92	3271129.65	8.06	60D NAIL
CP6	13709999.22	3271620.17	8.19	"X" IN CONC
CP7	13710017.44	3272102.67	6.84	MAG NAIL
CP8	13710039.84	3272576.37	6.09	MAG NAIL
CP9	13710058.04	3273093.45	6.91	MAG NAIL

DESIGN BASELINE DATA PROVIDED BY ARKK ENGINEERS

LINE	LENGTH	BEARING
L1	4300.00	N87°37'29"E
L2	176.21	N2°19'40"W
L3	300.00	N2°19'40"W
L4	300.00	N2°19'40"W
L5	300.00	N2°19'40"W
L6	300.00	N2°19'40"W
L7	300.00	N2°19'40"W

I, the undersigned, a Registered Professional Land Surveyor of the State of Texas, do hereby certify that this survey was made on the ground and is true and correct to the best of my knowledge and belief.

Robert D. Ellis
 Registered Professional
 Land Surveyor No. 4006



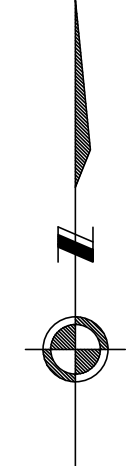
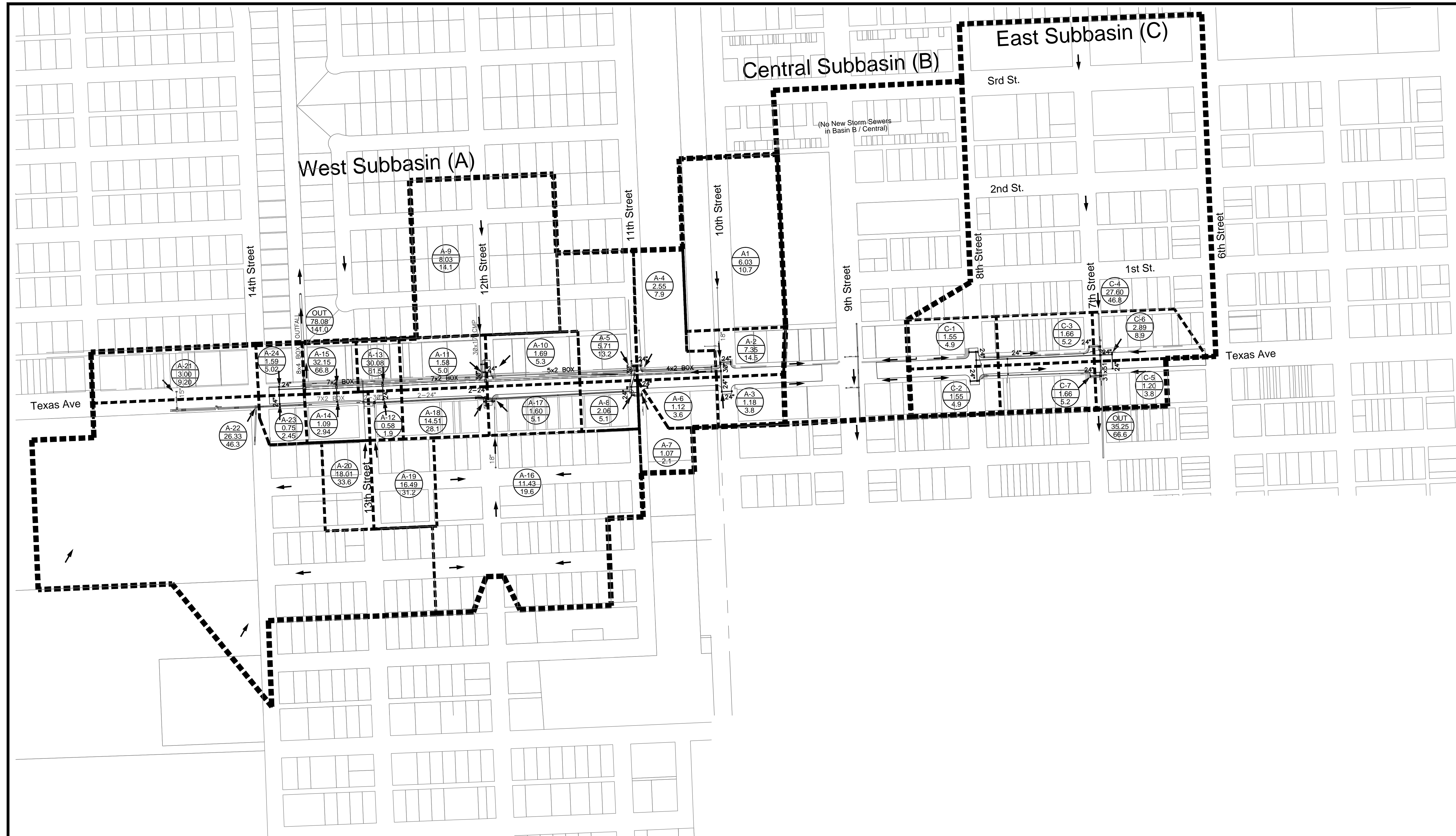
ELLIS SURVEYING SERVICES
 2805 25th Ave. North
 Texas City, Texas 77590
 Tel. : 409-938-8700

SCALE: 1" = 20'
 PHONE: (409)-938-8700

JOB NUMBER
 2675

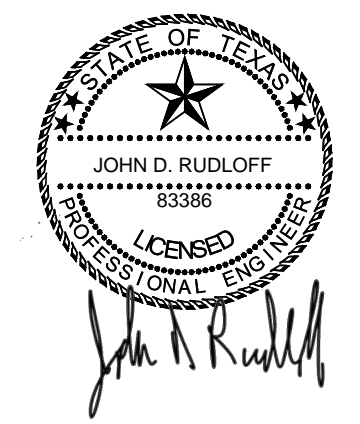
DATE: 2-27-2018
 SHEET 5 OF 52

CONTROL SHEET
F.M. 1765 (TEXAS AVENUE)
FROM 6TH STREET TO 14TH STREET
CITY OF TEXAS CITY
GALVESTON COUNTY, TEXAS



- LEGEND**
- A1
2.17
5.48 Drainage Basin Label
Cumulative Area (acres)
Total 2-year Flow (cfs)
 - Drainage Basin Boundary
 - Drainage Sub-area Boundary
 - Prop. Storm Sewer
 - Exist. Storm Sewer
 - Flow Path

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19

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Galveston County, Texas

Texas Avenue Reconstruction

Drainage Area Map

Job No.: 18-015	Scale: HORZ: 1"=200'	SHEET 6 OF 52
Date: September, 2019	VERT:	
Dwn By: D. Fattig		
Chkd By: J. Rudloff		

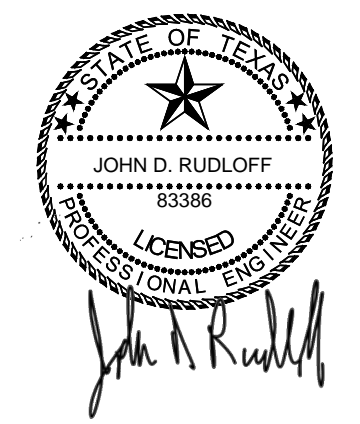
Two Year Storm Analysis

TEXAS AVENUE - GALVESTON COUNTY - 2 YEAR STORM

Basin	Sub - basin	Area (Ac.)	C	C x A	Sum C x A	Sum Areas	Tc (min)	I (in/hr)	Total Runoff, cfs	Pipe Type	Existing Pipe?	Pipe Dia (ft)	No. of Barrels	Span	Rise	Flow Area	P	R	Length	Pipe Slope	Velocity Full	n	Downstream Hydraulic Grade Line, ft	Upstream Hydraulic Grade Line Elevation, ft	Upstream Top of Curb Elevation, ft
A	1	6.03	0.45	2.71	2.71	6.03	28.7	3.95	10.71	round	(Exist)	1.50		n/a	n/a	1.77	4.71	0.38	n/a	n/a	6.06	0.013	6.76	(exist)	out of prj
A	2	1.32	0.75	0.99	3.70	7.35	29.2	3.91	14.47	round		2.50		n/a	n/a	4.91	7.85	0.63	35	1.000%	2.95	0.013	6.72	6.76	8.13
A	3	1.18	0.75	0.89	0.89	1.18	25.3	4.27	3.78	round		2.00		n/a	n/a	3.14	6.28	0.50	80	0.300%	1.20	0.013	6.72	6.74	7.74
A	2+3	0.00	0.75	0.00	4.59	8.53	29.6	3.88	17.78	box		n/a		4.00	2.00	8.00	12.00	0.67	341	0.130%	2.22	0.013	6.50	6.72	8.13
A	4	2.55	0.75	1.91	1.91	2.55	26.8	4.12	7.88	round		2.00		n/a	n/a	3.14	6.28	0.50	24	0.400%	2.51	0.013	6.54	6.57	6.42
A	5	3.16	0.45	1.42	3.33	5.71	28.6	3.96	13.20	RCAP		n/a		36"	23"	4.50	7.85	0.57	34	0.100%	2.93	0.013	6.50	6.54	6.42
A	6	1.12	0.75	0.84	0.84	1.12	25.2	4.28	3.59	round		2.00		n/a	n/a	3.14	6.28	0.50	63	0.200%	1.14	0.013	6.56	6.58	6.73
A	7	1.07	0.45	0.48	0.48	1.07	25.1	4.28	2.06	round		2.00		n/a	n/a	3.14	6.28	0.50	28	0.700%	0.66	0.013	6.58	6.59	6.95
A	8	0.99	0.75	0.74	1.22	2.06	26.4	4.16	5.09	round		2.00		n/a	n/a	3.14	6.28	0.50	41	0.150%	1.62	0.013	6.56	6.58	6.95
A	6+8	0.00	0.75	0.00	2.06	3.18	27.3	4.08	8.41	round		2.00		n/a	n/a	3.14	6.28	0.50	49	0.160%	2.68	0.013	6.50	6.56	7.03
A	8+5+3	0.00	0.75	0.00	9.99	17.42	31.5	3.72	37.19	box		n/a		5.00	2.00	10.00	14.00	0.71	585	0.050%	3.72	0.013	5.53	6.50	6.42
A	9	8.03	0.45	3.61	3.61	8.03	29.4	3.89	14.05	box		n/a		4.00	2.00	8.00	12.00	0.67	51	0.100%	1.76	0.013	5.56	5.58	6.25
A	10	1.69	0.75	1.27	1.27	1.69	26.0	4.20	5.32	round		2.00		n/a	n/a	3.14	6.28	0.50	21	0.500%	1.69	0.013	5.56	5.58	6.14
A	11	1.58	0.75	1.19	1.19	1.58	25.8	4.21	4.99	round		2.00		n/a	n/a	3.14	6.28	0.50	9	1.110%	1.59	0.013	5.56	5.57	6.14
A	10+11+9	0.00	0.75	0.00	6.07	11.30	30.3	3.82	23.15	box		n/a		4.00	2.00	8.00	12.00	0.67	34	0.100%	2.89	0.013	5.53	5.56	6.14
A	11+8	0.00	0.75	0.00	16.05	28.72	33.1	3.61	58.01	box		n/a		7.00	2.00	14.00	18.00	0.78	404	0.050%	4.14	0.013	4.78	5.53	6.14
A	12	0.58	0.75	0.44	0.44	0.58	24.1	4.39	1.91	round		2.00		n/a	n/a	3.14	6.28	0.50	57	0.700%	0.61	0.013	4.78	4.79	7.17
A	13	0.78	0.75	0.59	17.07	30.08	33.2	3.60	61.52	box		n/a		7.00	2.00	14.00	18.00	0.78	181	0.050%	4.39	0.013	4.41	4.78	7.17
A	14	1.09	0.75	0.82	0.82	1.09	25.2	4.28	3.50	round		2.00		n/a	n/a	3.14	6.28	0.50	57	0.300%	1.11	0.013	4.41	4.42	6.84
A	15	0.98	0.75	0.74	18.63	32.15	33.4	3.59	66.84	box		n/a		7.00	2.00	14.00	18.00	0.78	127	0.050%	4.77	0.013	4.10	4.41	6.84
A	16	11.43	0.45	5.14	5.14	11.43	30.4	3.81	19.62	round		2.00	2	n/a	n/a	6.28	6.28	1.00	21	0.100%	3.12	0.013	5.96	5.98	6.00
A	17	1.60	0.75	1.20	1.20	1.60	25.9	4.21	5.05	round		2.00		n/a	n/a	3.14	6.28	0.50	24	0.400%	1.61	0.013	5.96	5.98	6.14
A	18A	1.48	0.75	1.11	7.45	14.51	31.0	3.76	28.05	round		2.00	2	n/a	n/a	6.28	6.28	1.00	54	0.100%	4.47	0.013	5.88	5.96	6.14
A	18B	0.00	0.75	0.00	7.45	14.51	31.0	3.76	28.05	round	(Exist)	2.00	2	n/a	n/a	6.28	12.56	0.50	398	0.075%	4.47	0.013	4.35	5.88	6.30
A	19	1.98	0.45	0.89	8.34	16.49	31.4	3.74	31.17	round	(Exist)	2.50	2	n/a	n/a	9.81	15.70	0.63	43	0.010%	3.18	0.013	4.29	4.35	7.23
A	20	1.52	0.45	0.68	9.03	18.01	31.6	3.72	33.55	box	(Exist)	n/a		7.00	2.00	14.00	18.00	0.78	230	0.170%	2.40	0.013	4.15	4.29	7.70
A	21a	3.00	0.75	2.25	2.25	3.00	27.1	4.09	9.20	round	(Exist)	1.25		n/a	n/a	1.23	3.93	0.31	70	0.100%	7.50	0.013	4.79	6.21	out of prj
A	21b	0.00	0.75	0.00	2.25	3.00	27.1	4.09	9.20	CMAF	(Exist)	n/a	2	42"	29"	13.00	9.42	1.38	310	0.060%	0.71	0.024	4.76	4.79	out of prj
A	22	23.33	0.45	10.50	12.75	26.33	32.8	3.63	46.31	round	(Exist)	2.50	2	n/a	n/a	9.81	15.70	0.63	192	0.060%	4.72	0.013	4.15	4.76	7.10
A	22+20	0.00	0.75	0.00	21.78	44.34	34.5	3.52	76.59	BOX	(Exist)	n/a		8.00	3.00	24.00	22.00	1.09	67	0.300%	3.19	0.013	4.10	4.15	7.28
A	23	0.75	0.75	0.56	0.56	0.75	24.5	4.35	2.45	round		2.00		n/a	n/a	3.14	6.28	0.50	57	0.200%	0.78	0.013	4.15	4.16	6.98
A	24	0.84	0.75	0.63	1.19	1.59	25.9	4.21	5.02	round		2.00		n/a	n/a	3.14	6.28	0.50	99	0.170%	1.60	0.013	4.10	4.15	6.98
A	24+22+15	0.00	0.75	0.00	41.60	78.08	36.5	3.39	140.95	BOX	(Exist)	n/a		8.00	4.00	32.00	24.00	1.33	n/a	0.300%	4.40	0.013	(Pipe Soffit)	4.10	7.28

Basin	Sub - basin	Area (Ac.)	C	Cx A	Sum Cx A	Sum Areas	Tc (min)	I (in/hr)	Total Runoff, cfs	Pipe Type	Existing Pipe?	Pipe Dia (ft)	No. of Barrels	Span	Rise	Flow Area	P	R	Length	Pipe Slope	Velocity Full	n	Downstream Hydraulic Grade Line, ft	Upstream Hydraulic Grade Line Elevation, ft	Upstream Top of Curb Elevation, ft
C	1	1.55	0.75	1.16	1.16	1.55	25.8	4.22	4.90	round		2.00		n/a	n/a	3.14	6.28	0.50	33	0.100%	1.56	0.013	6.32	6.33	6.89
C	2	1.55	0.75	1.16	1.16	1.55	25.8	4.22	4.90	round		2.00		n/a	n/a	3.14	6.28	0.50	82	0.100%	1.56	0.013	6.32	6.35	6.89
C	1+2	0.00	0.00	0.00	2.33	3.10	27.2	4.08	9.49	round		2.00		n/a	n/a	3.14	6.28	0.50	487	0.100%	3.02	0.013	5.46	6.32	6.97
C	3	1.66	0.75	1.25	1.25	1.66	25.9	4.20	5.23	round		2.00		n/a	n/a	3.14	6.28	0.50	43	3.140%	1.67	0.013	5.55	5.57	6.26
C	4	25.94	0.45	11.67	12.92	27.60	32.9	3.62	46.80	RCAP		n/a		51"	31"	8.90	10.99	0.81	33	0.090%	5.26	0.013	5.46	5.55	6.26
C	5	1.20	0.75	0.90	0.90	1.20	25.3	4.26	3.84	RCAP		n/a		29"	18"	2.90	6.28	0.462	56	0.200%	1.32	0.013	5.55	5.57	5.78
C	6	1.69	0.75	1.27	2.17	2.89	27.1	4.10	8.88	RCAP		n/a		29"	18"	2.90	6.28	0.462	46	0.090%	3.06	0.013	5.46	5.55	5.78
C	6+4+2	0.00	0.00	0.00	17.41	33.59	33.6	3.58	62.31	RCAP		n/a		51"	31"	8.90	10.99	0.81	82	0.110%	7.00	0.013	5.05	5.46	6.41
C	7	1.66	0.75	1.25	1.25	1.66	25.9	4.20	5.23	round		2.00		n/a	n/a	3.14	6.28	0.50	42	3.210%	1.67	0.013	5.05	5.07	6.14
C	7+6	0.00	0.00	0.00	18.66	35.25	33.7	3.57	66.57	CMAF	(Exist)	n/a		49"	33"	8.90	10.99	0.81	336	0.208%	7.48	0.024	(Pipe Soffit)	5.05	6.14

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19

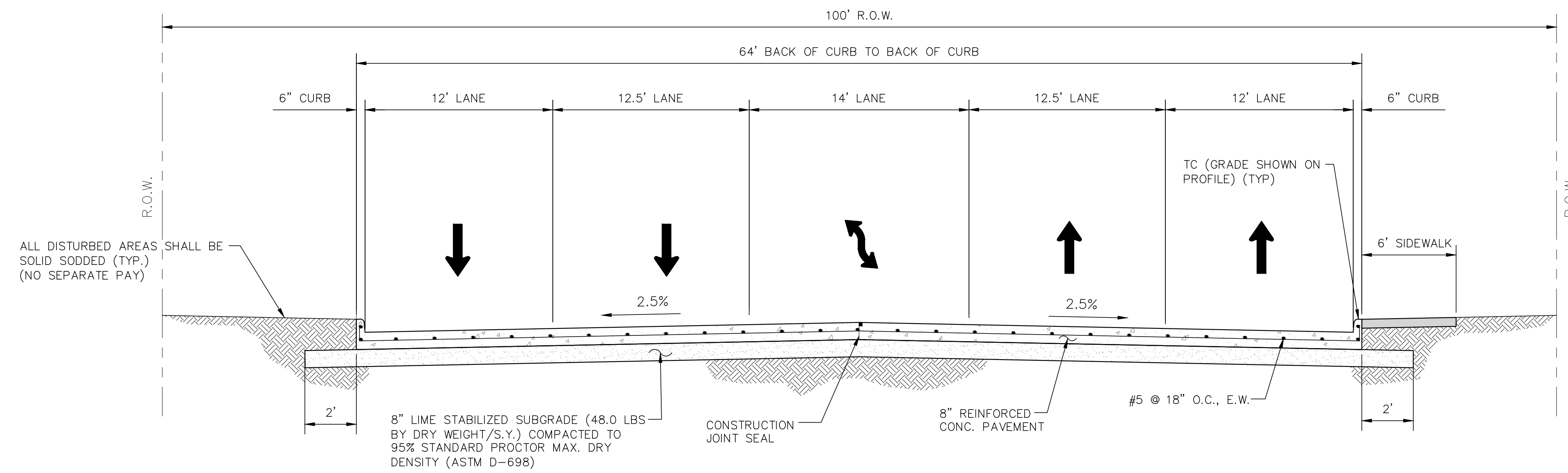
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Galveston County, Texas

Texas Avenue Reconstruction

Drainage Calculations

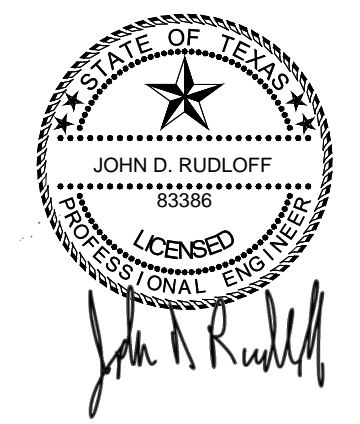
Job No.: 18-015	Scale: n/a	SHEET 6a OF 52
Date: September, 2019	HORZ: n/a	
Dwn By: D. Fattig	VERT:	
Chkd By: J. Rudloff		



PROPOSED TYPICAL PAVEMENT SECTION

Scale: 1"=5'

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19



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Galveston County, Texas

Texas Avenue Reconstruction

Typical Section

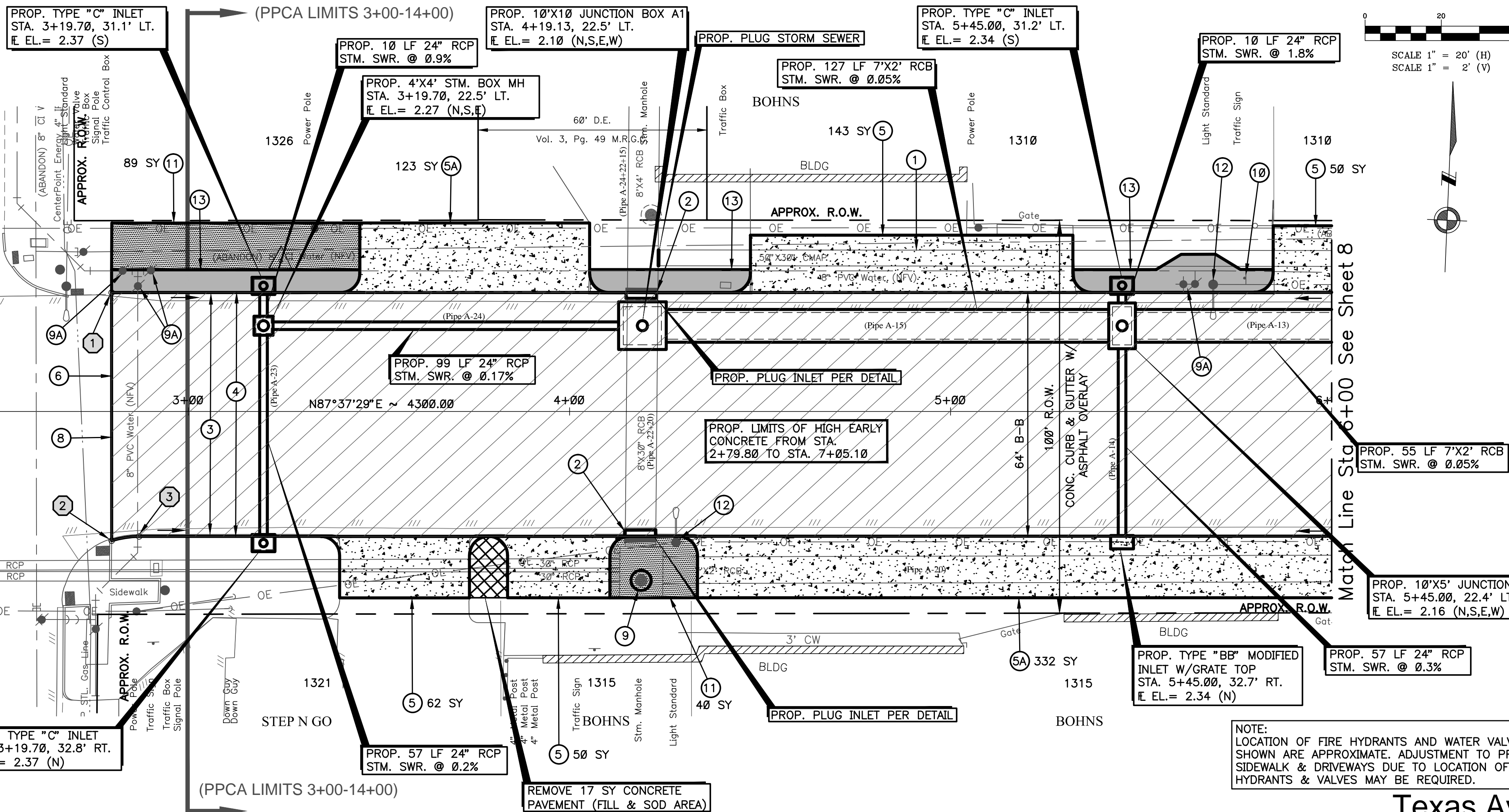
Job No.: 18-015	Scale: 1"=5'	SHEET
Date: September, 2019	HORIZ:	
Dwn By: D. Fattig	VERT:	6b
Chkd By: J. Rudloff		

OF 52

PT. NO	NORTHING	EASTING	ELEVATION	DESCRIPTION
CP 1	13709898.50	3269261.52	6.93	MAG NAIL

14th St. S.
(70' ROW)
(Asphalt Pavement)

TEXACO GAS STATION
1402



BENCHMARK:
SEE SURVEY/BASELINE CONTROL MAPS FOR BENCHMARK REFERENCES/ BASELINE DATA. (SHEET 5)

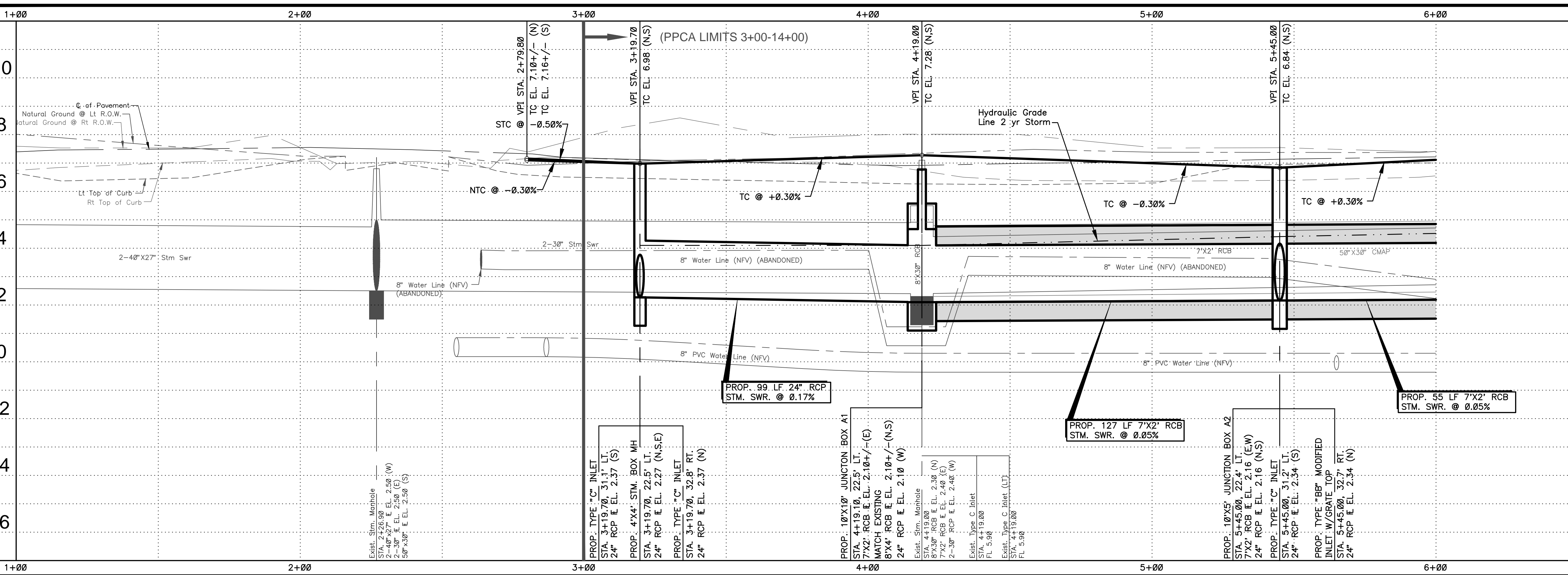
PAVING & DRAINAGE LEGEND:

- REMOVE EXIST. STM. SWR./CULVERT
- REMOVE EXIST. INLET/MANHOLE
- REMOVE AND DISPOSE OF EXISTING ASPH./CONC. PAVEMENT AND BASE COURSE.
- PROP. 8" THICK CONCRETE PAVEMENT AND 8" SUBGRADE (SUBGRADE TO EXTEND 2' OUTSIDE CURB)
- PROP. REMOVE AND REPLACE WITH 6" CONCRETE DRIVEWAY
- PROP. REMOVE AND REPLACE WITH 8" CONCRETE DRIVEWAY
- PROP. CONCRETE PAVING HEADER AT EXIST. CONCRETE ROAD
- PROP. CONCRETE PAVING HEADER AT ASPHALT ROAD
- PROP. SAW CUT. (NO SEPARATE PAY)
- ADJUST MANHOLES COVERS TO GRADE
- ADJUST FIRE HYDRANT & VALVE BOXES TO GRADE
- REMOVE/RELOCATE EXISTING SIGN (NO SEPARATE PAY)
- PROP. 4" THICK CONCRETE PAVEMENT
- PROTECT & BRACE LIGHT/POWER POLES AS NECESSARY (NO SEPARATE PAY)
- PROP. 6" - 4" THICK CONCRETE SIDEWALK
- PROP. CURB RAMP PER ADA REQUIREMENTS
- REMOVE TRAFFIC SIGNAL BOX

LEGEND:

- PROP. CONCRETE DRIVEWAY
- PROP. 4" CONCRETE SIDEWALK
- PROP. 4" CONCRETE PAVEMENT
- PROP. ASPHALT PAVEMENT
- PROP. REMOVE PAVEMENT
- PROP. LIMITS OF HIGH EARLY CONCRETE

NOTE:
LOCATION OF FIRE HYDRANTS AND WATER VALVES SHOWN ARE APPROXIMATE. ADJUSTMENT TO PROPOSED SIDEWALK & DRIVEWAYS DUE TO LOCATION OF FIRE HYDRANTS & VALVES MAY BE REQUIRED.



#	STATION	OFFSET
1	PT 2+79.80	31.20' LT.
2	PT 2+79.80	33.90' RT.
3	PT 2+87.00	32.80' RT.

MK.	DESCRIPTION	DATE	DWN.	CHK.

STATE OF TEXAS
JOHN D. RUDLOFF
83386
LICENSED PROFESSIONAL ENGINEER

9-13-19

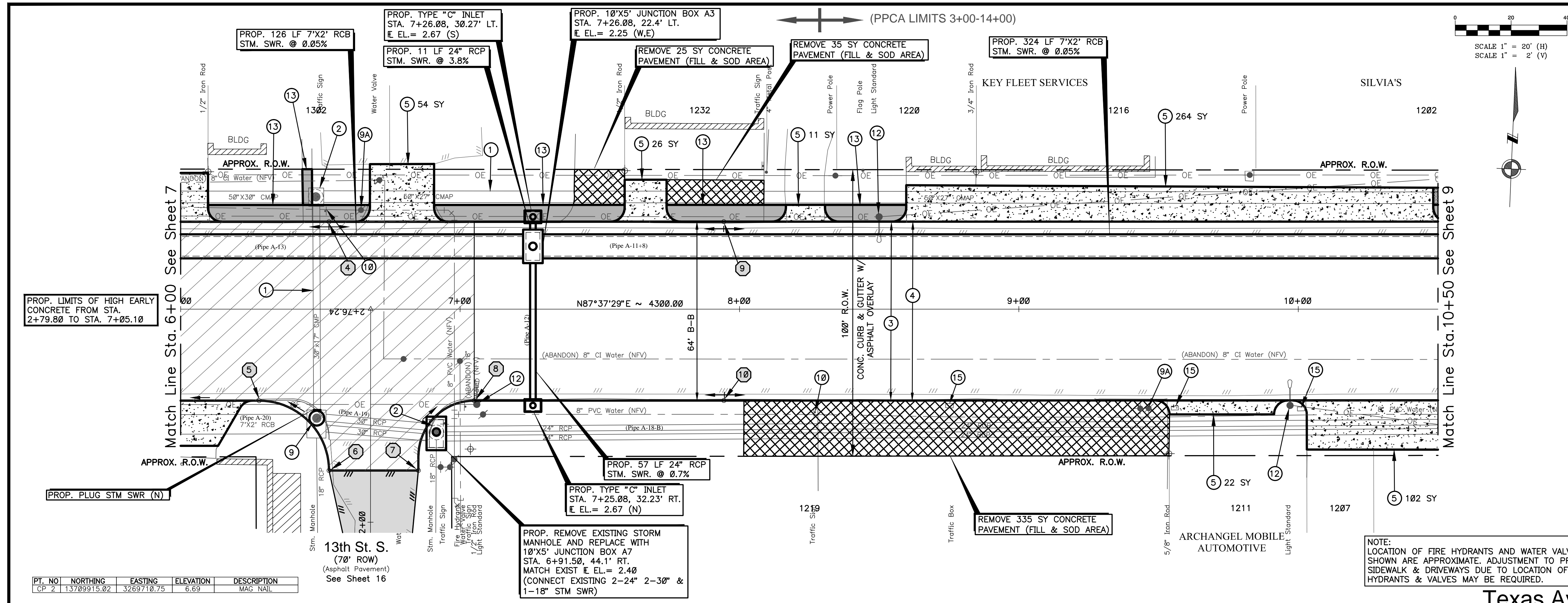
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Galveston County, Texas

Texas Avenue Reconstruction

Texas Ave.
Sta. 1+00 to Sta. 6+00

Job No.: 18-015	Scale: HORZ: 1" = 20' VERT: 1" = 2'	SHEET 7
Date: September, 2019		OF 52
Dwn By: D. Fattig		
Chkd By: J. Rudloff		



BENCHMARK:
SEE SURVEY/BASELINE CONTROL MAPS FOR BENCHMARK REFERENCES/ BASELINE DATA. (SHEET 5)

PAVING & DRAINAGE LEGEND:

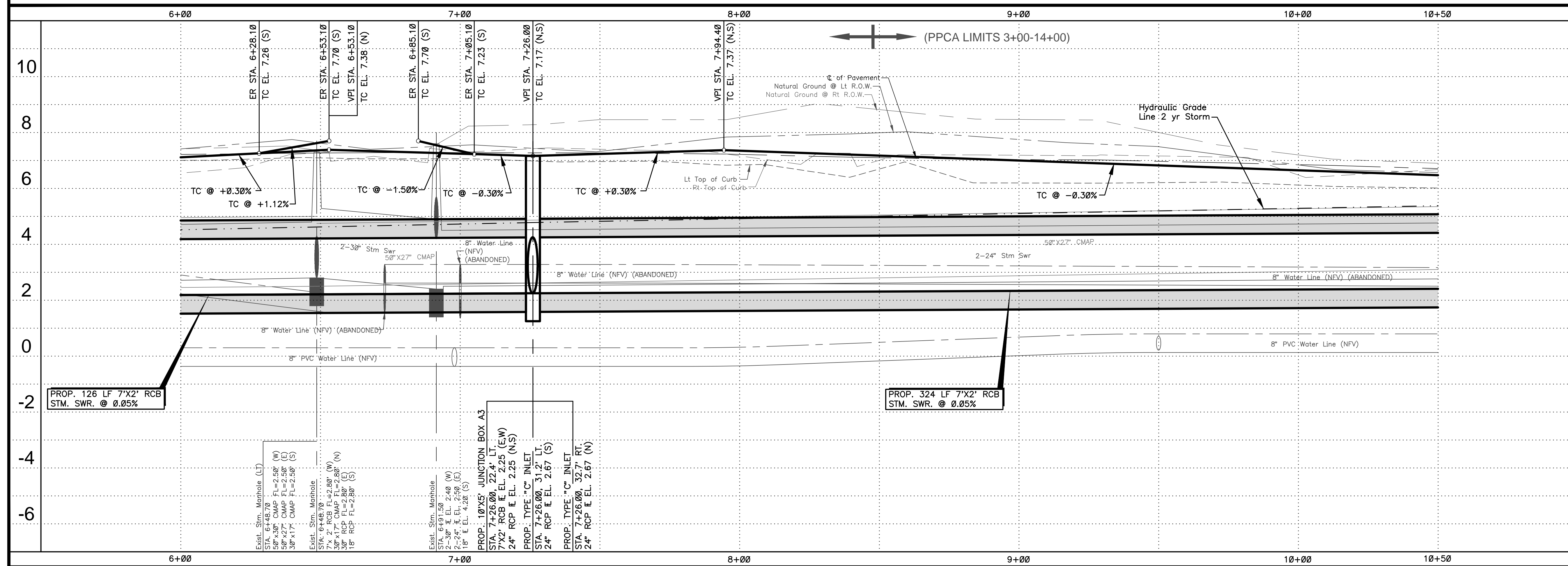
- REMOVE EXIST. STM. SWR./CULVERT
- REMOVE EXIST. INLET/MANHOLE
- REMOVE AND DISPOSE OF EXISTING ASPH./CONC. PAVEMENT AND BASE COURSE.
- PROP. 8" THICK CONCRETE PAVEMENT AND 8" SUBGRADE (SUBGRADE TO EXTEND 2' OUTSIDE CURB)
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- PROP. REMOVE AND REPLACE WITH 8" CONCRETE DRIVEWAY
- PROP. CONCRETE PAVING HEADER AT EXIST. CONCRETE ROAD
- PROP. CONCRETE PAVING HEADER AT ASPHALT ROAD
- PROP. SAW CUT. (NO SEPARATE PAY)
- ADJUST MANHOLES COVERS TO GRADE
- ADJUST FIRE HYDRANT & VALVE BOXES TO GRADE
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- PROP. 6" - 4" THICK CONCRETE SIDEWALK
- PROP. CURB RAMP PER ADA REQUIREMENTS
- REMOVE TRAFFIC SIGNAL BOX

LEGEND:

- PROP. CONCRETE DRIVEWAY
- PROP. 4" CONCRETE SIDEWALK
- PROP. 4" CONCRETE PAVEMENT
- PROP. ASPHALT PAVEMENT
- PROP. REMOVE PAVEMENT
- PROP. LIMITS OF HIGH EARLY CONCRETE

#	STATION	OFFSET
4	PT 6+53.10	31.20' LT.
5	PT 6+28.10	32.70' RT.
6	PT 6+53.10	57.70' RT.
7	PT 6+85.10	57.70' RT.
8	PT 7+05.10	32.70' RT.
9	PT 7+94.40	31.20' LT.
10	PT 7+94.40	32.70' RT.

NOTE: LOCATION OF FIRE HYDRANTS AND WATER VALVES SHOWN ARE APPROXIMATE. ADJUSTMENT TO PROPOSED SIDEWALK & DRIVEWAYS DUE TO LOCATION OF FIRE HYDRANTS & VALVES MAY BE REQUIRED.



MK.	DESCRIPTION	DATE	DWN.	CHK.

9-13-19

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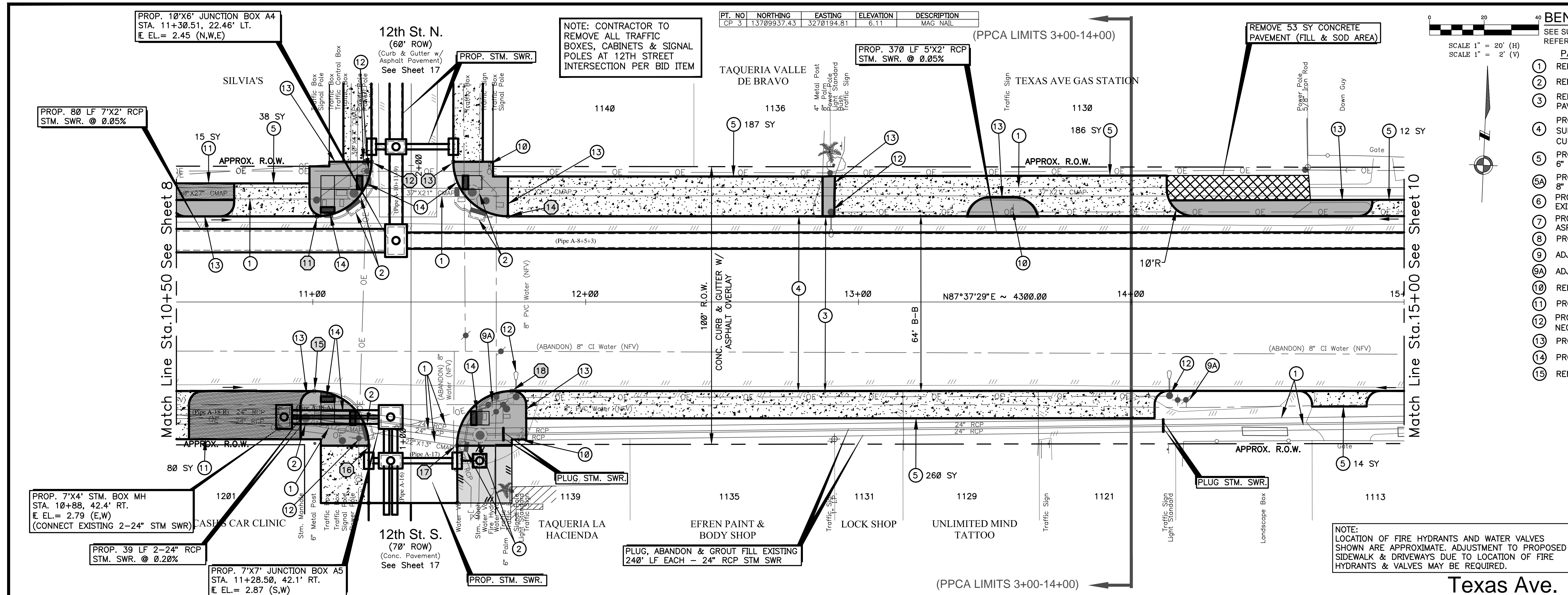
Galveston County, Texas

Texas Avenue Reconstruction

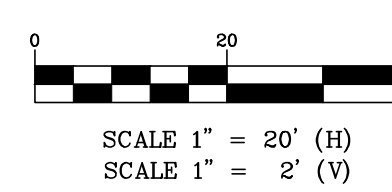
Texas Ave.
Sta. 6+00 to Sta. 10+50

Job No.: 18-015	Scale:	SHEET
Date: September, 2019	HORIZ: 1" = 20'	
Dwn By: D. Fattig	VERT: 1" = 2'	8
Chk By: J. Rudloff		

OF 52



PT. NO	NORTHING	EASTING	ELEVATION	DESCRIPTION
CP 3	1370937.43	3270194.81	6.11	MAG NAIL



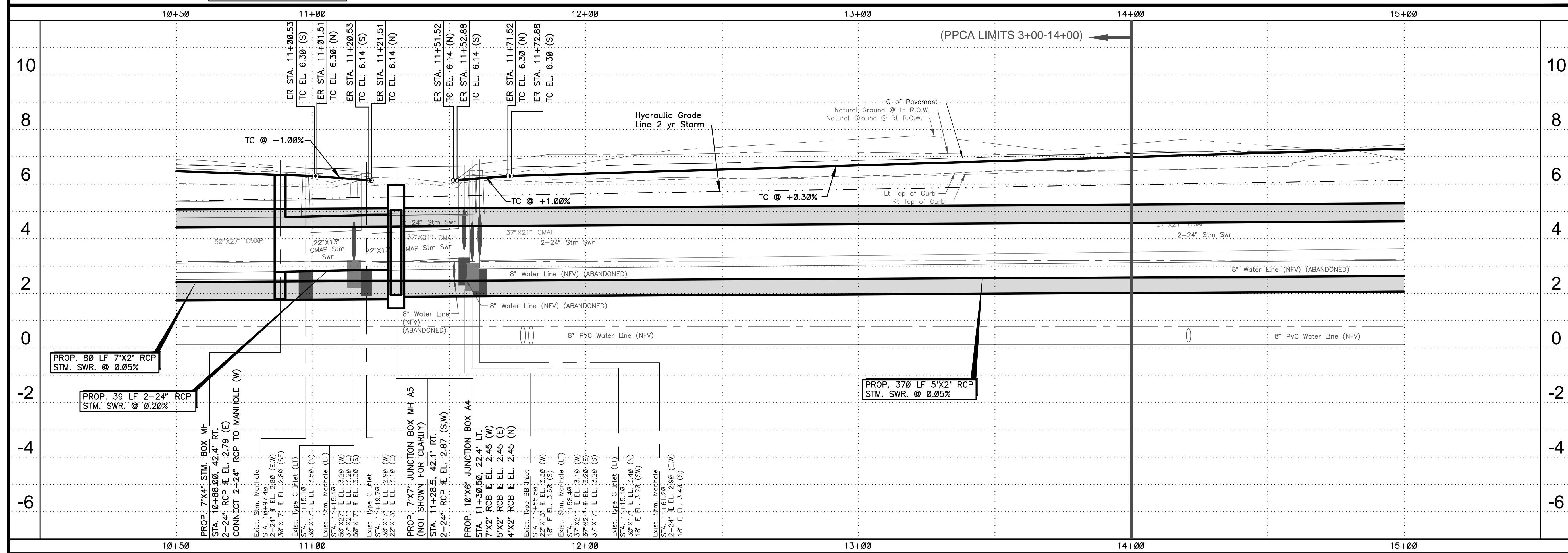
BENCHMARK:
SEE SURVEY/BASELINE CONTROL MAPS FOR BENCHMARK REFERENCES/ BASELINE DATA. (SHEET 5)

- PAVING & DRAINAGE LEGEND:**
- 1 REMOVE EXIST. STM. SWR./CULVERT
 - 2 REMOVE EXIST. INLET/MANHOLE
 - 3 REMOVE AND DISPOSE OF EXISTING ASPH./CONC. PAVEMENT AND BASE COURSE.
 - 4 PROP. 8" THICK CONCRETE PAVEMENT AND 8" SUBGRADE (SUBGRADE TO EXTEND 2' OUTSIDE CURB)
 - 5 PROP. REMOVE AND REPLACE WITH 6" CONCRETE DRIVEWAY
 - 5A PROP. REMOVE AND REPLACE WITH 8" CONCRETE DRIVEWAY
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 - 7 PROP. CONCRETE PAVING HEADER AT ASPHALT ROAD
 - 8 PROP. SAW CUT. (NO SEPARATE PAY)
 - 9 ADJUST MANHOLES COVERS TO GRADE
 - 9A ADJUST FIRE HYDRANT & VALVE BOXES TO GRADE
 - 10 REMOVE/RELOCATE EXISTING SIGN (NO SEPARATE PAY)
 - 11 PROP. 4" THICK CONCRETE PAVEMENT
 - 12 PROTECT & BRACE LIGHT/POWER POLES AS NECESSARY (NO SEPARATE PAY)
 - 13 PROP. 6" - 4" THICK CONCRETE SIDEWALK
 - 14 PROP. CURB RAMP PER ADA REQUIREMENTS
 - 15 REMOVE TRAFFIC SIGNAL BOX

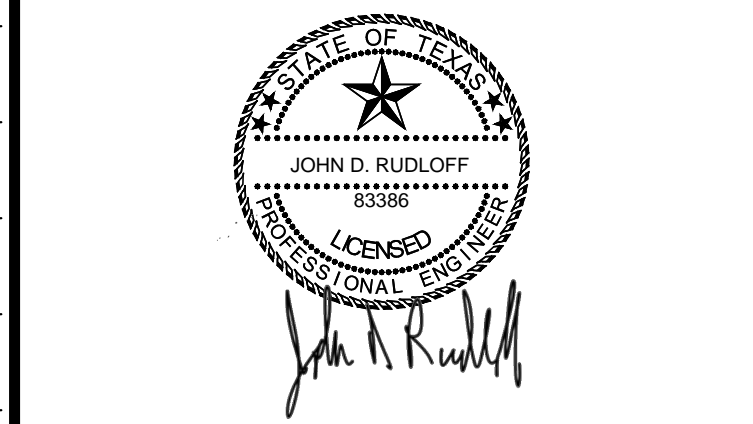
- PROP. CONCRETE DRIVEWAY
- PROP. 4" CONCRETE SIDEWALK
- PROP. 4" CONCRETE PAVEMENT
- PROP. ASPHALT PAVEMENT
- PROP. REMOVE PAVEMENT
- PROP. LIMITS OF HIGH EARLY CONCRETE

#	STATION	OFFSET
11	PT 11+01.50	31.30' LT.
12	PT 11+21.50	51.30' LT.
13	PT 11+51.50	51.30' LT.
14	PT 11+71.50	31.30' LT.
15	PT 11+00.50	32.60' RT.
16	PT 11+20.50	52.60' RT.
17	PT 11+52.90	52.60' RT.
18	PT 11+72.90	32.60' RT.

NOTE: LOCATION OF FIRE HYDRANTS AND WATER VALVES SHOWN ARE APPROXIMATE. ADJUSTMENT TO PROPOSED SIDEWALK & DRIVEWAYS DUE TO LOCATION OF FIRE HYDRANTS & VALVES MAY BE REQUIRED.



MK.	DESCRIPTION	DATE	DWN.	CHK.



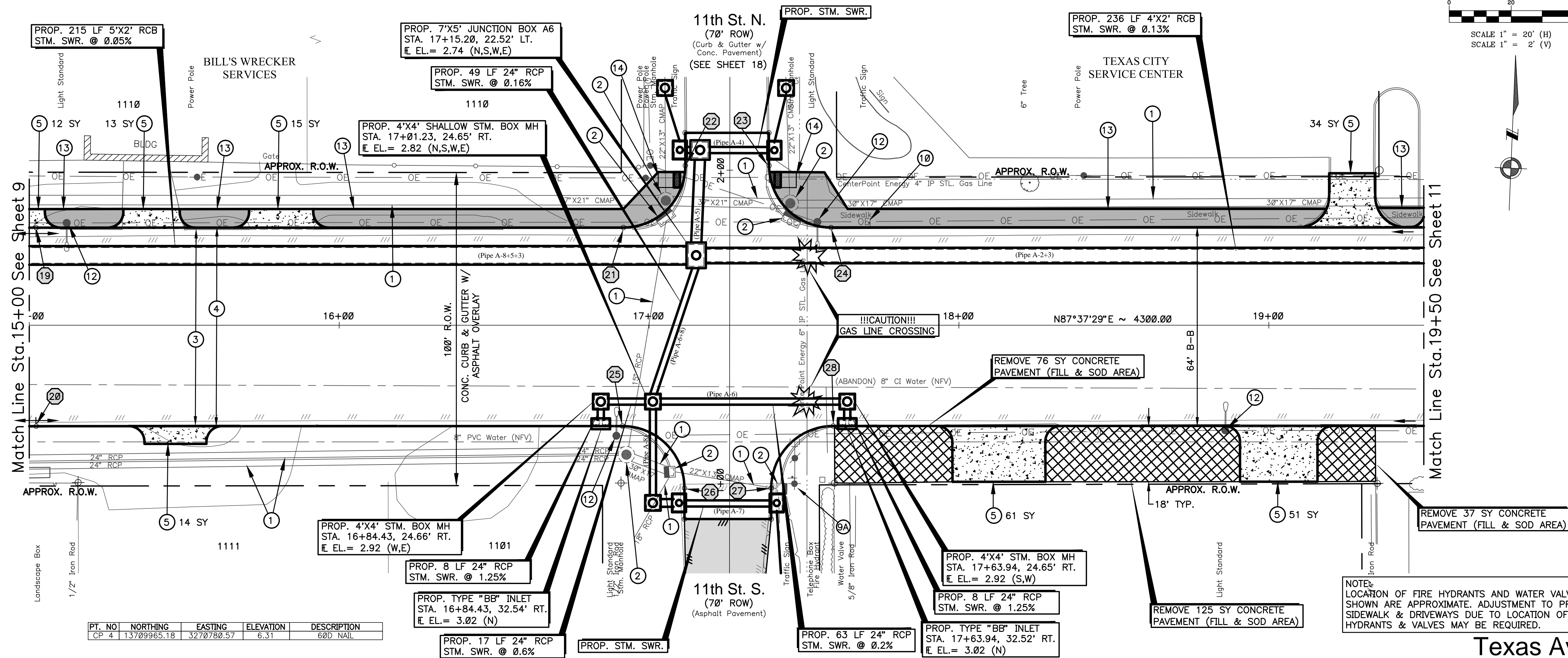
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Galveston County, Texas

Texas Avenue Reconstruction

Texas Ave.
Sta. 10+50 to Sta. 15+00

Job No.: 18-015 Scale: SHEET
Date: September, 2019 HORZ: 1" = 20' 9
Dwn By: D. Fattig VERT: 1" = 2' OF 52
Chk By: J. Rudloff



PT. NO	NORTHING	EASTING	ELEVATION	DESCRIPTION
CP 4	13709965.18	3270780.57	6.31	600' NAIL

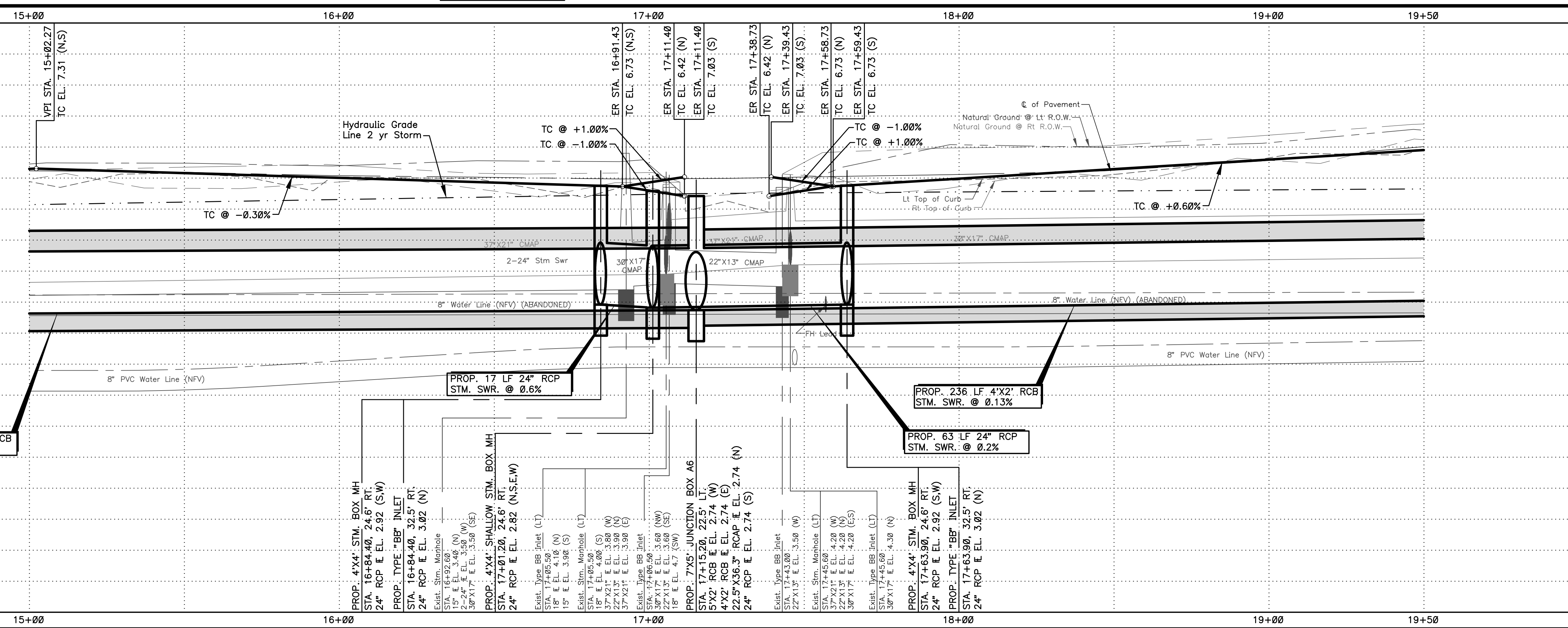
BENCHMARK:
SEE SURVEY/BASELINE CONTROL MAPS FOR BENCHMARK REFERENCES/ BASELINE DATA. (SHEET 5)

- PAVING & DRAINAGE LEGEND:**
- REMOVE EXIST. STM. SWR./CULVERT
 - REMOVE EXIST. INLET/MANHOLE
 - REMOVE AND DISPOSE OF EXISTING ASPH./CONC. PAVEMENT AND BASE COURSE.
 - PROP. 8" THICK CONCRETE PAVEMENT AND 8" SUBGRADE (SUBGRADE TO EXTEND 2' OUTSIDE CURB)
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 - PROP. CONCRETE PAVING HEADER AT ASPHALT ROAD
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 - PROTECT & BRACE LIGHT/POWER POLES AS NECESSARY (NO SEPARATE PAY)
 - PROP. 6" - 4" THICK CONCRETE SIDEWALK
 - PROP. CURB RAMP PER ADA REQUIREMENTS
 - REMOVE TRAFFIC SIGNAL BOX

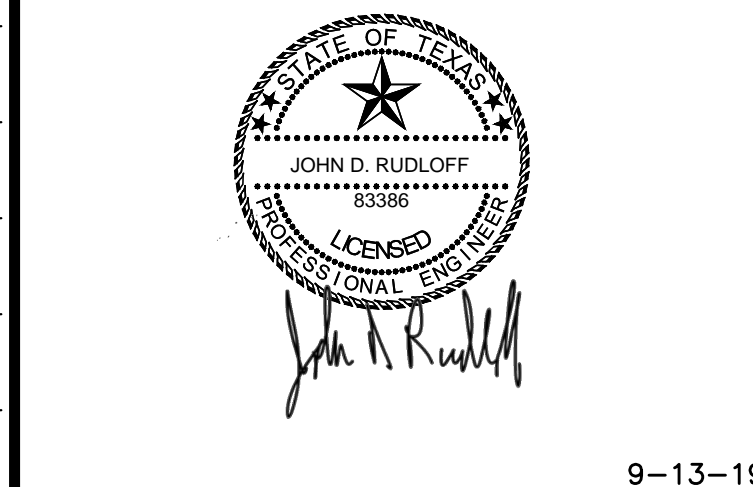
- PROP. CONCRETE DRIVEWAY
- PROP. 4" CONCRETE SIDEWALK
- PROP. 4" CONCRETE PAVEMENT
- PROP. ASPHALT PAVEMENT
- PROP. REMOVE PAVEMENT
- PROP. LIMITS OF HIGH EARLY CONCRETE

#	STATION	OFFSET
19	PT 15+02.20	31.48' LT.
20	PT 15+02.20	32.50' RT.
21	PT 16+91.70	31.50' LT.
22	PT 17+11.70	51.50' LT.
23	PT 17+38.70	51.50' LT.
24	PT 17+58.70	31.50' LT.
25	PT 16+91.40	32.50' RT.
26	PT 17+11.40	52.50' RT.
27	PT 17+39.40	52.50' RT.
28	PT 17+59.40	32.50' RT.

NOTES:
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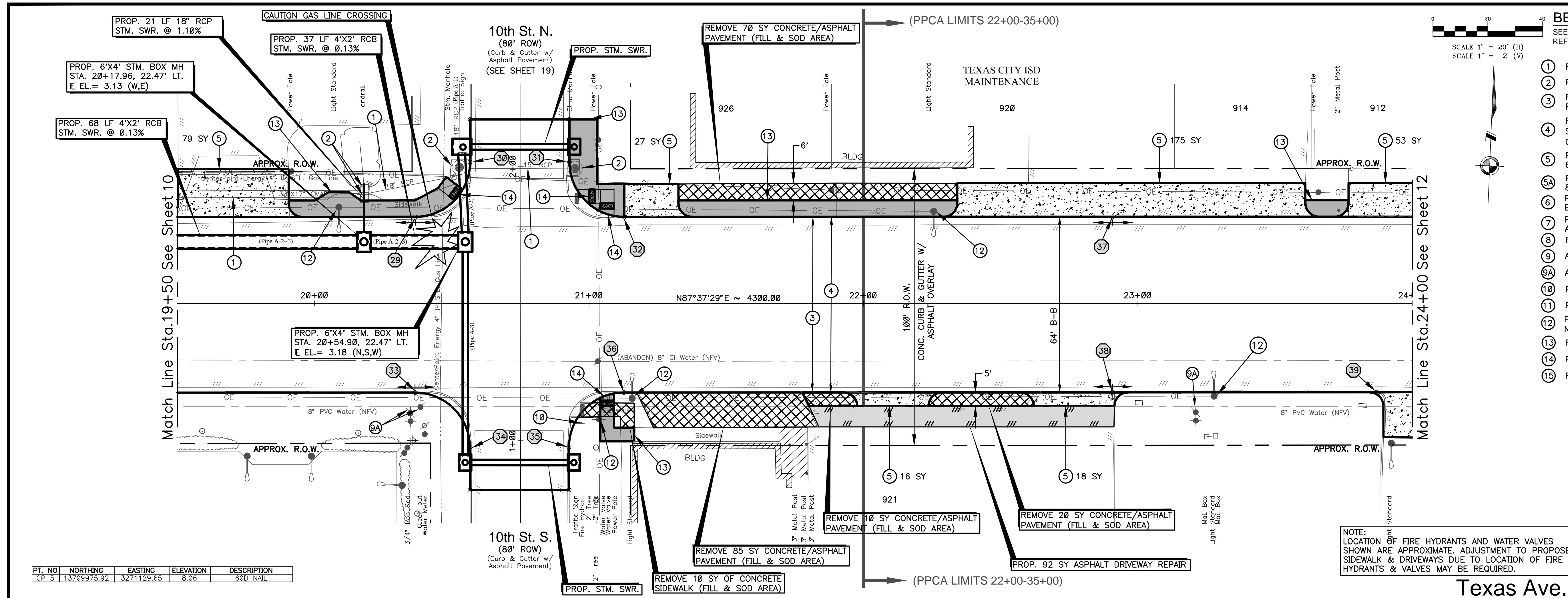
MK.	DESCRIPTION	DATE	DWN.	CHK.



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Galveston County, Texas
Texas Avenue Reconstruction
Texas Ave.
Sta. 15+00 to Sta. 19+50

Job No.: 18-015	Scale: HORIZ: 1" = 20'	SHEET 10 OF 52
Date: September, 2019	VERT: 1" = 2'	
Dwn By: D. Fattig	Chkd By: J. Rudloff	



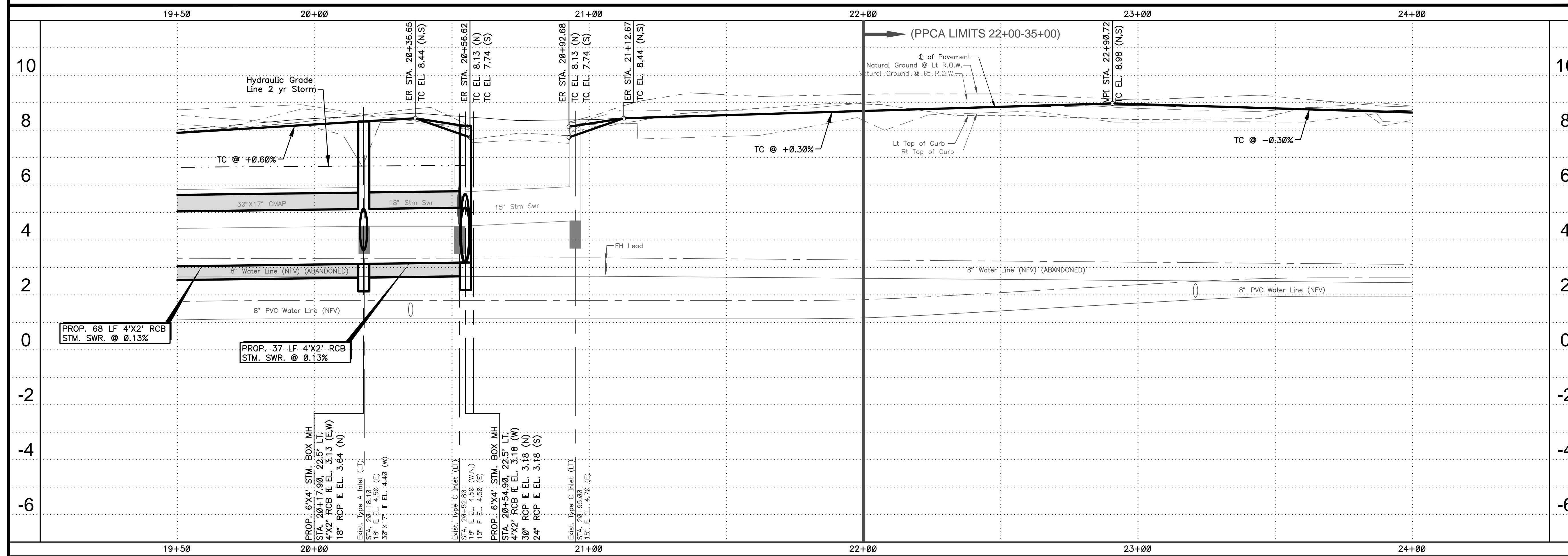
- BENCHMARK:**
SEE SURVEY/BASELINE CONTROL MAPS FOR BENCHMARK REFERENCES/ BASELINE DATA. (SHEET 5)
- PAVING & DRAINAGE LEGEND:**
- 1 REMOVE EXIST. STM. SWR./CULVERT
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 - 15 REMOVE TRAFFIC SIGNAL BOX

- PROP. CONCRETE DRIVEWAY
- PROP. 4" CONCRETE SIDEWALK
- PROP. 4" CONCRETE PAVEMENT
- PROP. ASPHALT PAVEMENT
- PROP. REMOVE PAVEMENT
- PROP. LIMITS OF HIGH EARLY CONCRETE

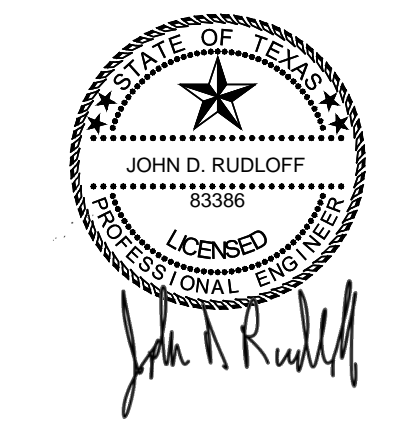
#	STATION	OFFSET
29	PT 20+36.60	31.50' LT.
30	PT 20+56.60	51.50' LT.
31	PT 20+92.80	51.50' LT.
32	PT 21+12.80	31.50' LT.
33	PT 20+36.60	32.40' RT.
34	PT 20+56.60	52.40' RT.
35	PT 20+92.60	52.40' RT.
36	PT 21+12.60	32.40' RT.
37	PT 22+90.70	31.50' LT.
38	PT 22+90.70	32.40' RT.
39	PT 23+86.90	32.40' RT.

NOTE:
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PT. NO	NORTHING	EASTING	ELEVATION	DESCRIPTION
CP 5	13709975.92	3271129.65	8.06	600 NAIL



MK.	DESCRIPTION	DATE	DWN.	CHK.



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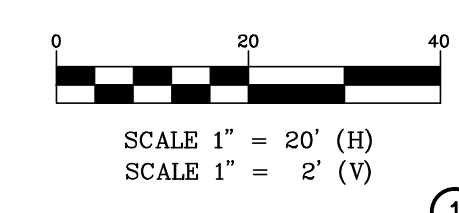
Galveston County, Texas

Texas Avenue Reconstruction

Texas Ave.
Sta. 19+50 to Sta. 24+00

Job No.: 18-015	Scale: HORIZ: 1" = 20'	SHEET 11 OF 52
Date: September, 2019	VERT: 1" = 2'	
Dwn By: D. Fattig		
Chkd By: J. Rudloff		

(PPCA LIMITS 22+00-35+00)



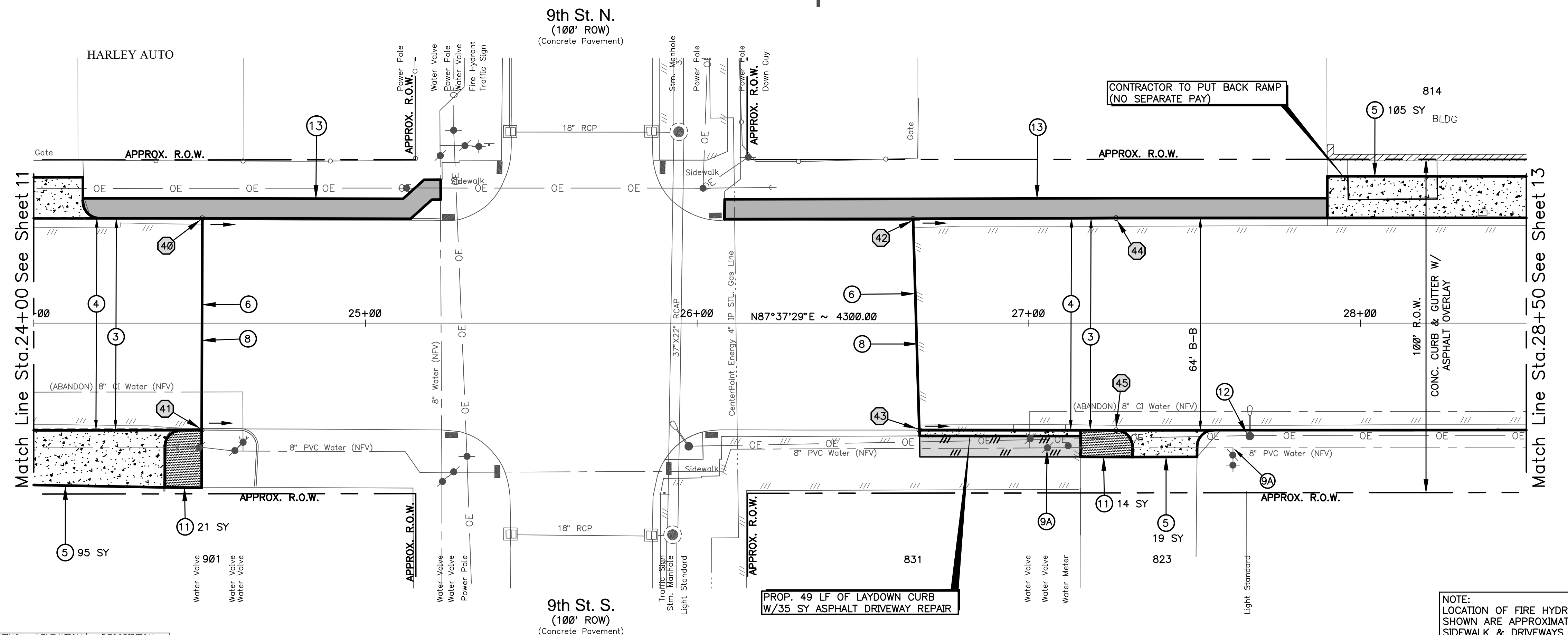
BENCHMARK:
SEE SURVEY/BASELINE CONTROL MAPS FOR BENCHMARK REFERENCES/ BASELINE DATA. (SHEET 5)

- PAVING & DRAINAGE LEGEND:**
- 1 REMOVE EXIST. STM. SWR./CULVERT
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 - 15 REMOVE TRAFFIC SIGNAL BOX

- PROP. CONCRETE DRIVEWAY
- PROP. 4" CONCRETE SIDEWALK
- PROP. 4" CONCRETE PAVEMENT
- PROP. ASPHALT PAVEMENT
- PROP. REMOVE PAVEMENT
- PROP. LIMITS OF HIGH EARLY CONCRETE

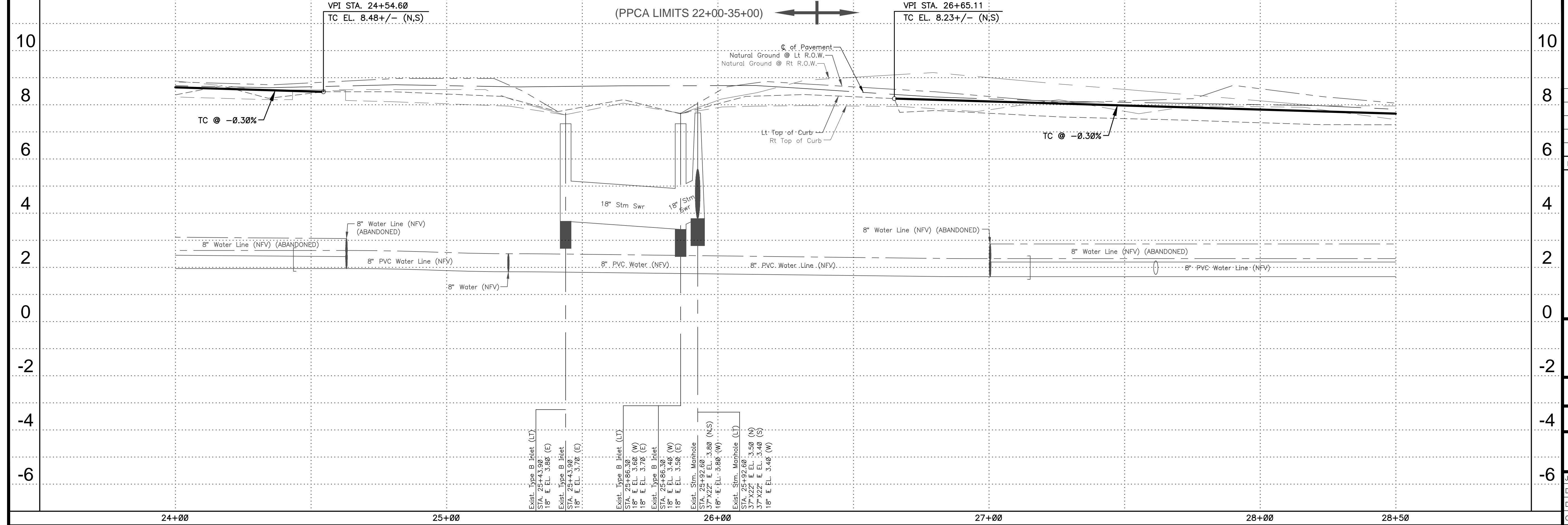
#	STATION	OFFSET
40	PT 24+50.80	31.60' LT.
41	PT 24+50.60	32.20' RT.
42	PT 26+65.10	31.40' LT.
43	PT 26+67.00	32.20' RT.
44	PT 27+26.20	31.60' LT.
45	PT 27+26.20	32.30' RT.

NOTE: LOCATION OF FIRE HYDRANTS AND WATER VALVES SHOWN ARE APPROXIMATE. ADJUSTMENT TO PROPOSED SIDEWALK & DRIVEWAYS DUE TO LOCATION OF FIRE HYDRANTS & VALVES MAY BE REQUIRED.



PT. NO	NORTHING	EASTING	ELEVATION	DESCRIPTION
CP 6	13709999.22	3271620.17	8.19	*X* IN CONC.

24+00 25+00 26+00 27+00 28+00 28+50



MK.	DESCRIPTION	DATE	DWN.	CHK.

9-13-19

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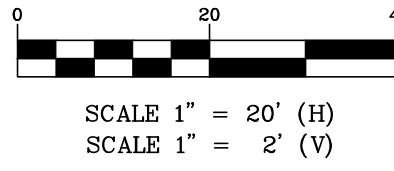
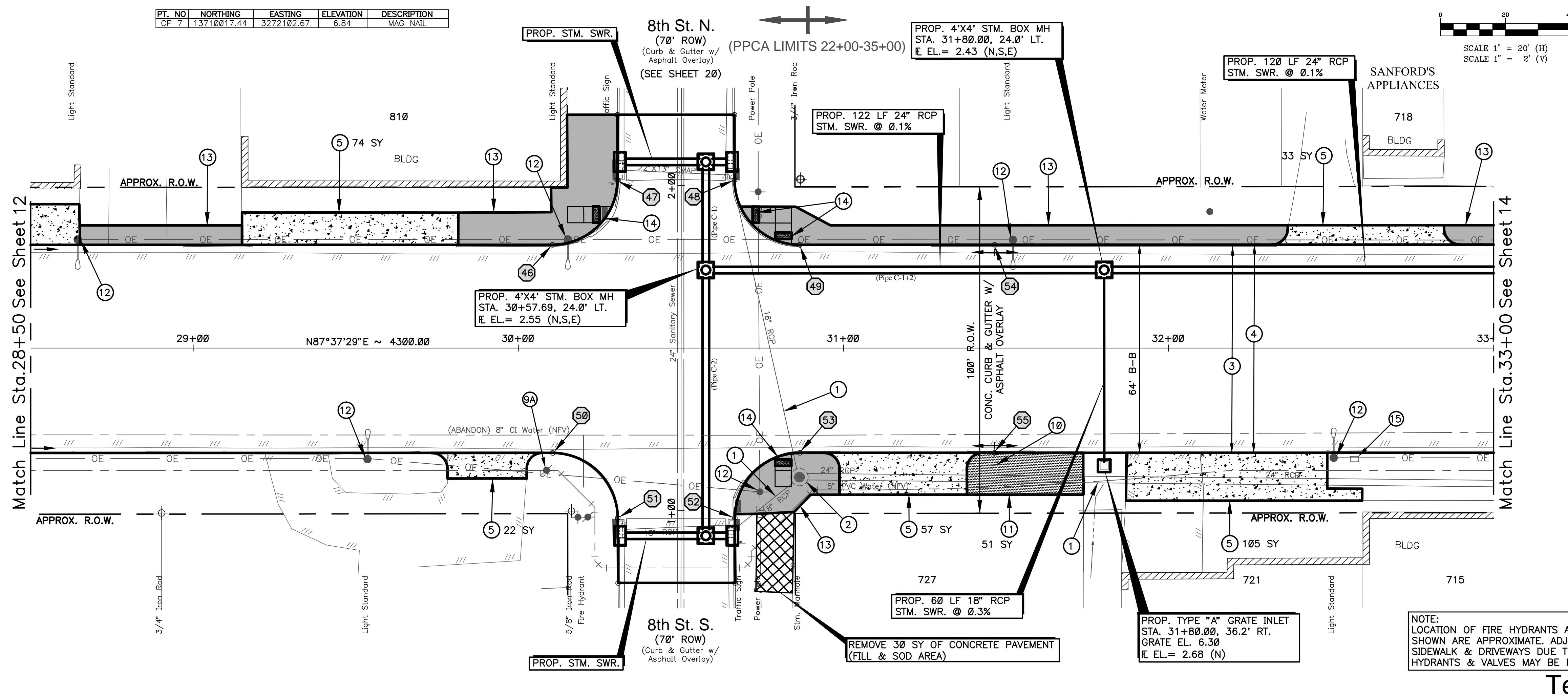
Galveston County, Texas

Texas Avenue Reconstruction

Texas Ave.
Sta. 24+00 to Sta. 28+50

Job No.: 18-015	Scale: HORIZ: 1" = 20'	SHEET 12 OF 52
Date: September, 2019	VERT: 1" = 2'	
Dwn By: D. Fattig		
Chkd By: J. Rudloff		

PT. NO	NORTHING	EASTING	ELEVATION	DESCRIPTION
CP 7	13710017.44	3272102.67	6.84	MAG NAIL



BENCHMARK:
SEE SURVEY/BASELINE CONTROL MAPS FOR BENCHMARK REFERENCES/ BASELINE DATA. (SHEET 5)

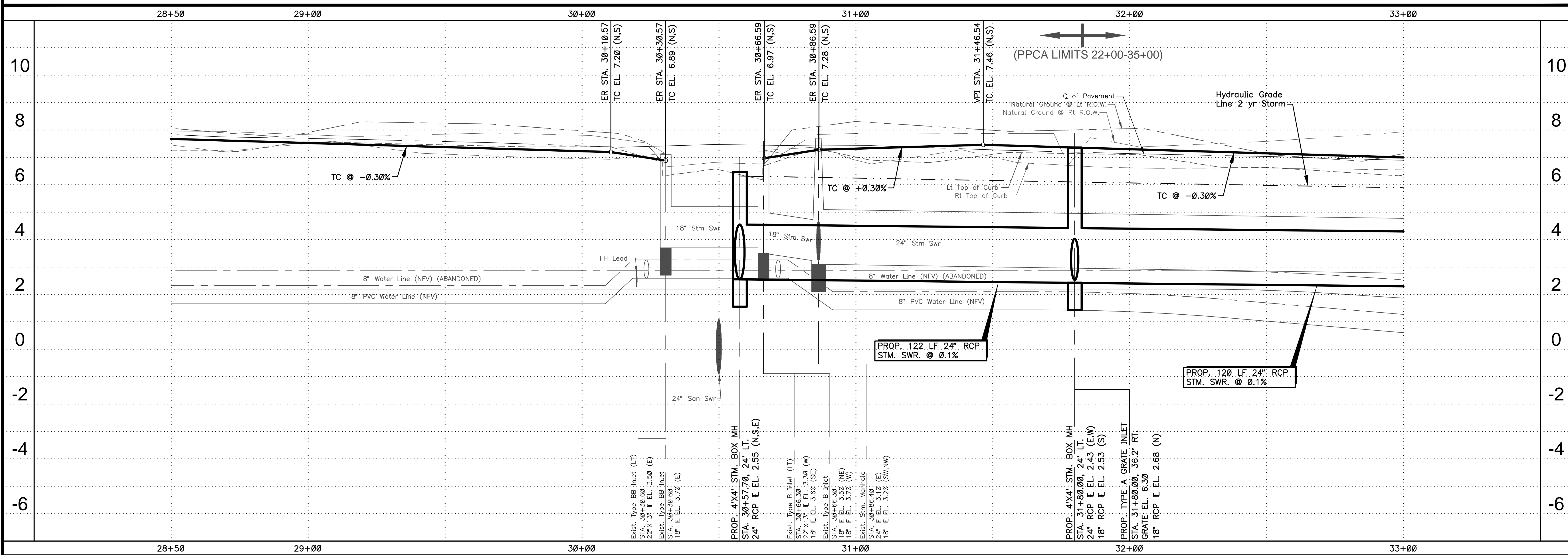
- PAVING & DRAINAGE LEGEND:**
- 1 REMOVE EXIST. STM. SWR./CULVERT
 - 2 REMOVE EXIST. INLET/MANHOLE
 - 3 REMOVE AND DISPOSE OF EXISTING ASPH./CONC. PAVEMENT AND BASE COURSE.
 - 4 PROP. 8" THICK CONCRETE PAVEMENT AND 8" SUBGRADE (SUBGRADE TO EXTEND 2' OUTSIDE CURB)
 - 5 PROP. REMOVE AND REPLACE WITH 6" CONCRETE DRIVEWAY
 - 5A PROP. REMOVE AND REPLACE WITH 8" CONCRETE DRIVEWAY
 - 6 PROP. CONCRETE PAVING HEADER AT EXIST. CONCRETE ROAD
 - 7 PROP. CONCRETE PAVING HEADER AT ASPHALT ROAD
 - 8 PROP. SAW CUT. (NO SEPARATE PAY)
 - 9 ADJUST MANHOLES COVERS TO GRADE
 - 9A ADJUST FIRE HYDRANT & VALVE BOXES TO GRADE
 - 10 REMOVE/RELOCATE EXISTING SIGN (NO SEPARATE PAY)
 - 11 PROP. 4" THICK CONCRETE PAVEMENT
 - 12 PROTECT & BRACE LIGHT/POWER POLES AS NECESSARY (NO SEPARATE PAY)
 - 13 PROP. 6" - 4" THICK CONCRETE SIDEWALK
 - 14 PROP. CURB RAMP PER ADA REQUIREMENTS
 - 15 REMOVE TRAFFIC SIGNAL BOX

- PROP. CONCRETE DRIVEWAY
- PROP. 4" CONCRETE SIDEWALK
- PROP. 4" CONCRETE PAVEMENT
- PROP. ASPHALT PAVEMENT
- PROP. REMOVE PAVEMENT
- PROP. LIMITS OF HIGH EARLY CONCRETE

#	STATION	OFFSET
46	PT 30+10.50	31.70' LT.
47	PT 30+30.50	51.70' LT.
48	PT 30+66.50	51.70' LT.
49	PT 30+86.50	31.70' LT.
50	PT 30+10.50	32.20' RT.
51	PT 30+30.50	52.20' RT.
52	PT 30+66.60	53.20' RT.
53	PT 30+86.60	32.20' RT.
54	PT 31+46.50	31.70' LT.
55	PT 31+46.50	32.20' RT.

NOTE: LOCATION OF FIRE HYDRANTS AND WATER VALVES SHOWN ARE APPROXIMATE. ADJUSTMENT TO PROPOSED SIDEWALK & DRIVEWAYS DUE TO LOCATION OF FIRE HYDRANTS & VALVES MAY BE REQUIRED.

Texas Ave.



MK.	DESCRIPTION	DATE	DWN.	CHK.

9-13-19

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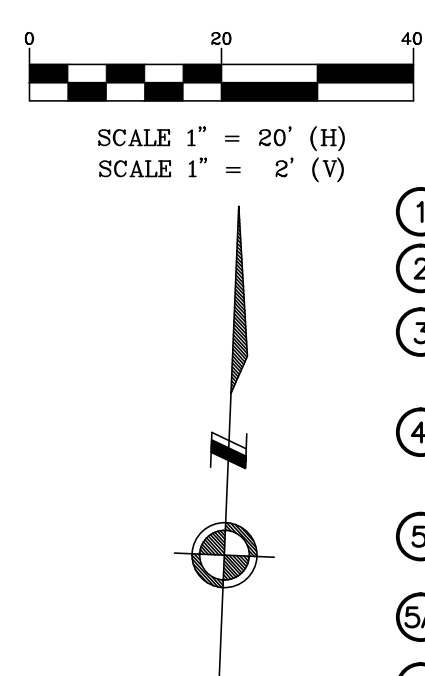
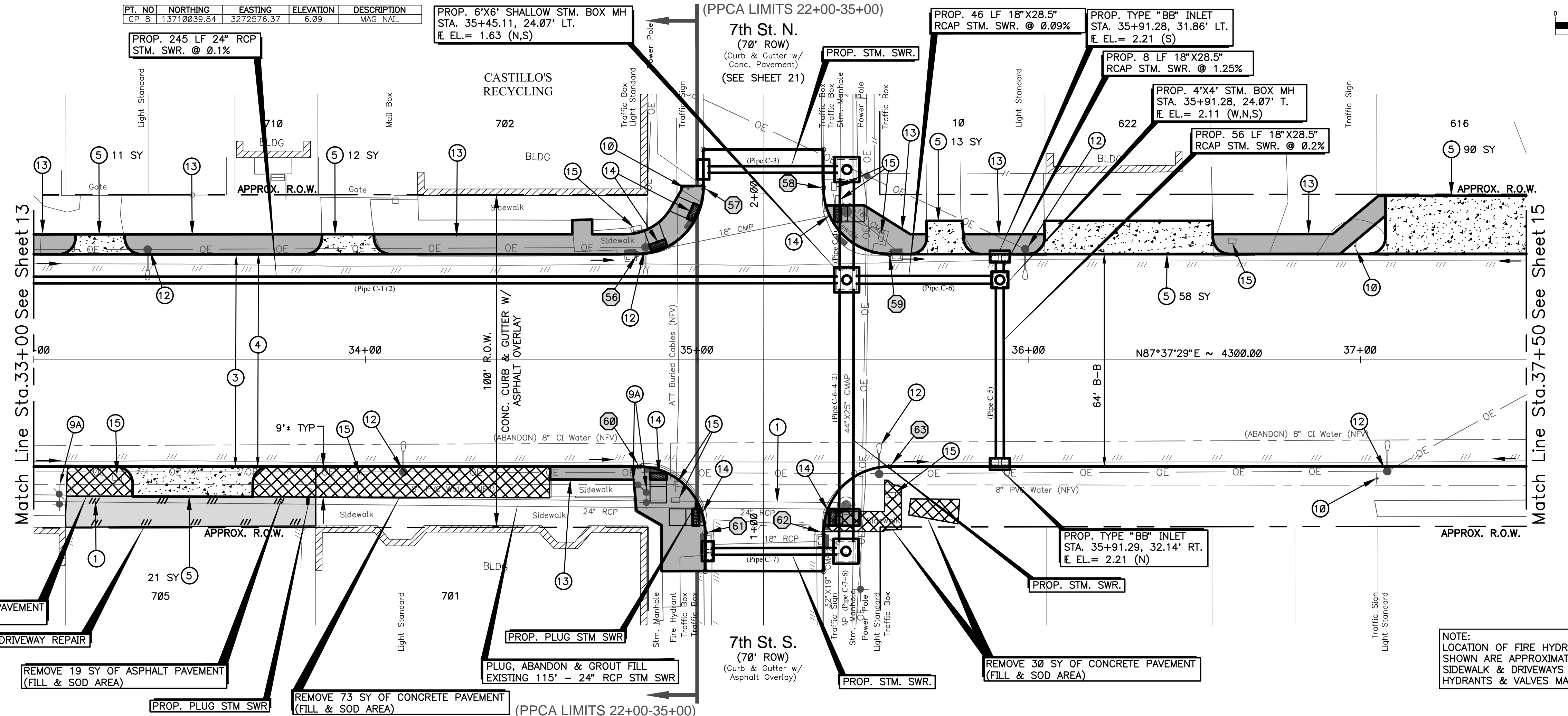
Galveston County, Texas

Texas Avenue Reconstruction
Texas Ave.
Sta. 28+50 to Sta. 33+00

Job No.: 18-015	Scale: HORIZ: 1" = 20'	SHEET 13 OF 52
Date: September, 2019	VERT: 1" = 2'	
Dwn By: D. Fattig		
Chkd By: J. Rudloff		

PT. NO	NORTHING	EASTING	ELEVATION	DESCRIPTION
CP 8	13710239.84	3272576.37	6.09	MAG NAIL

PROP. 6'X6' SHALLOW STM. BOX MH
STA. 35+45.11, 24.07' LT.
E. EL. = 1.63 (N,S)



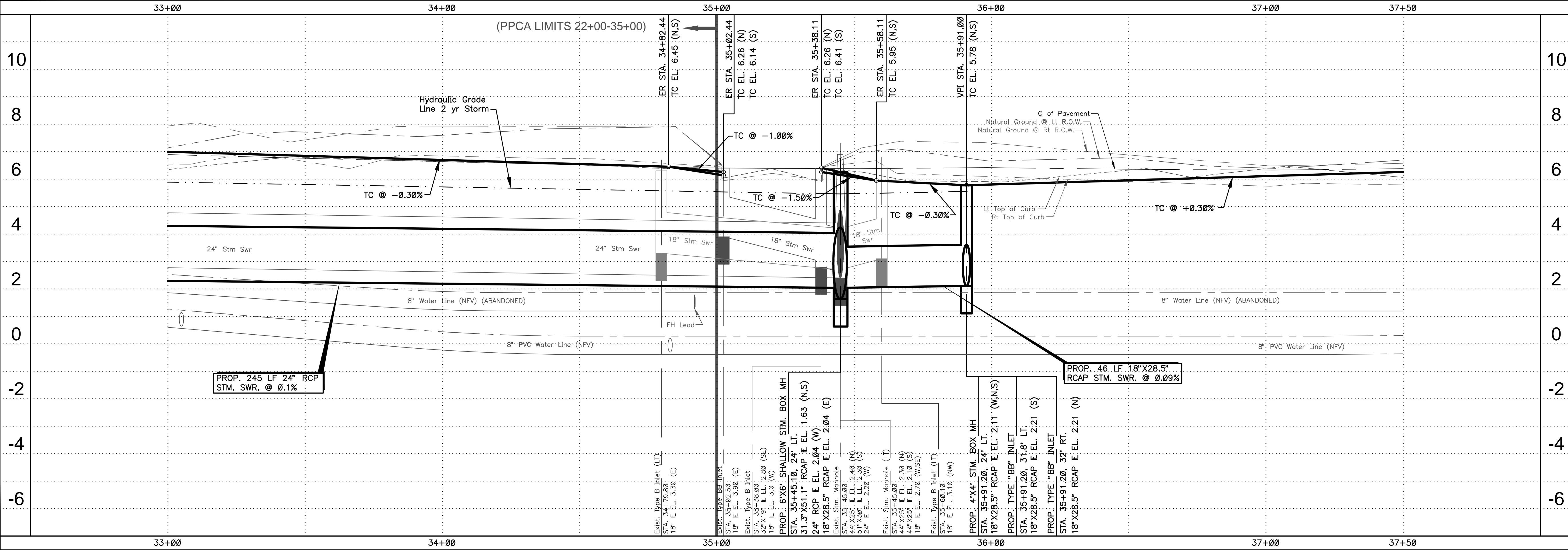
BENCHMARK:
SEE SURVEY/BASELINE CONTROL MAPS FOR BENCHMARK REFERENCES/ BASELINE DATA. (SHEET 5)

- PAVING & DRAINAGE LEGEND:**
- 1 REMOVE EXIST. STM. SWR./CULVERT
 - 2 REMOVE EXIST. INLET/MANHOLE
 - 3 REMOVE AND DISPOSE OF EXISTING ASPH./CONC. PAVEMENT AND BASE COURSE.
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 - 5A PROP. REMOVE AND REPLACE WITH 8" CONCRETE DRIVEWAY
 - 6 PROP. CONCRETE PAVING HEADER AT EXIST. CONCRETE ROAD
 - 7 PROP. CONCRETE PAVING HEADER AT ASPHALT ROAD
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 - 12 PROTECT & BRACE LIGHT/POWER POLES AS NECESSARY (NO SEPARATE PAY)
 - 13 PROP. 6" - 4" THICK CONCRETE SIDEWALK
 - 14 PROP. CURB RAMP PER ADA REQUIREMENTS
 - 15 REMOVE TRAFFIC SIGNAL BOX

- PROP. CONCRETE DRIVEWAY
- PROP. 4" CONCRETE SIDEWALK
- PROP. 4" CONCRETE PAVEMENT
- PROP. ASPHALT PAVEMENT
- PROP. REMOVE PAVEMENT
- PROP. LIMITS OF HIGH EARLY CONCRETE

#	STATION	OFFSET
56	PT 34+81.90	31.80' LT.
57	PT 35+01.90	51.80' LT.
58	PT 35+38.00	51.80' LT.
59	PT 35+58.00	31.80' LT.
60	PT 34+82.40	32.10' RT.
61	PT 35+02.40	52.10' RT.
62	PT 35+38.10	52.10' RT.
63	PT 35+58.10	32.10' RT.

NOTE:
LOCATION OF FIRE HYDRANTS AND WATER VALVES SHOWN ARE APPROXIMATE. ADJUSTMENT TO PROPOSED SIDEWALK & DRIVEWAYS DUE TO LOCATION OF FIRE HYDRANTS & VALVES MAY BE REQUIRED.



MK.	DESCRIPTION	DATE	DWN.	CHK.

9-13-19

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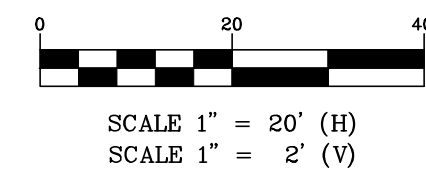
Galveston County, Texas

Texas Avenue Reconstruction

Texas Ave.
Sta. 33+00 to Sta. 37+50

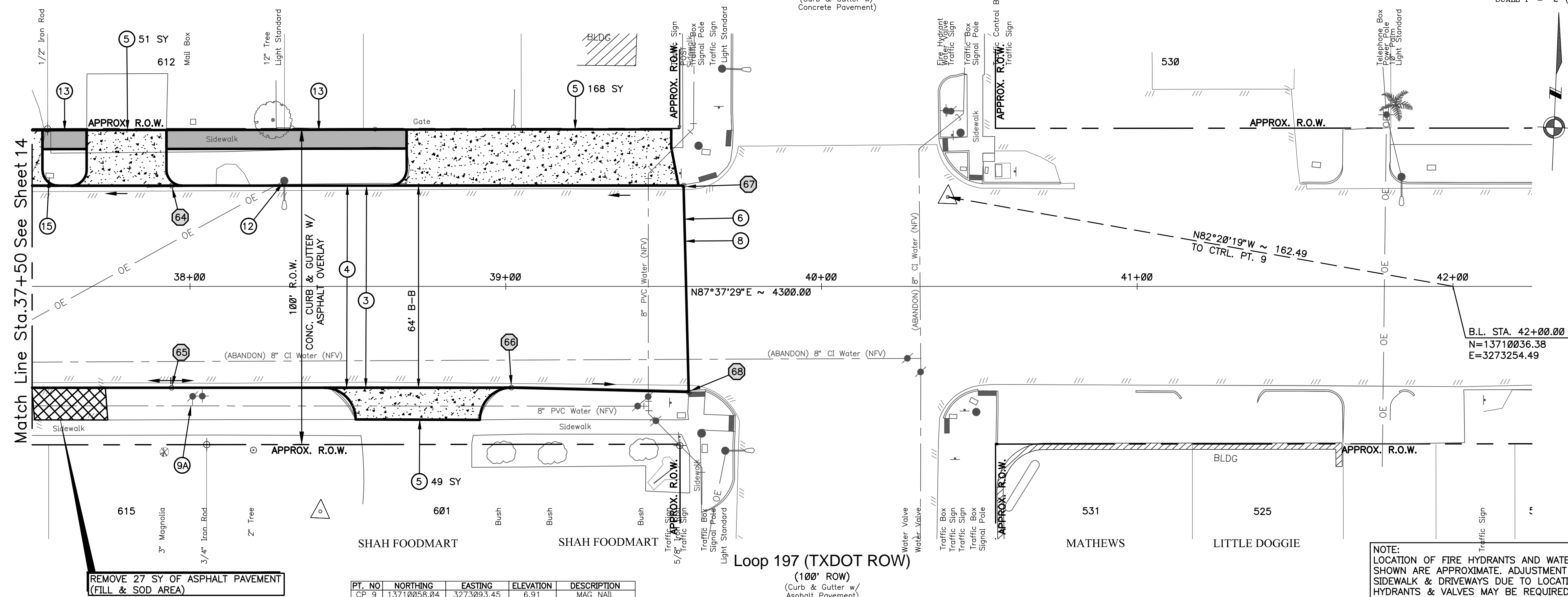
Job No.: 18-015	Scale: HORZ: 1" = 20' VERT: 1" = 2'	SHEET
Date: September, 2019		14
Dwn By: D. Fattig		OF 52
Chkd By: J. Rudloff		

6th St. N. - Loop 197
(100' ROW)
(Curb & Gutter w/
Concrete Pavement)



BENCHMARK:
SEE SURVEY/BASELINE CONTROL MAPS FOR BENCHMARK REFERENCES/ BASELINE DATA. (SHEET 5)

- PAVING & DRAINAGE LEGEND:**
- 1 REMOVE EXIST. STM. SWR./CULVERT
 - 2 REMOVE EXIST. INLET/MANHOLE
 - 3 REMOVE AND DISPOSE OF EXISTING ASPH./CONC. PAVEMENT AND BASE COURSE.
 - 4 PROP. 8" THICK CONCRETE PAVEMENT AND 8" SUBGRADE (SUBGRADE TO EXTEND 2' OUTSIDE CURB)
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 - 11 PROP. 4" THICK CONCRETE PAVEMENT
 - 12 PROTECT & BRACE LIGHT/POWER POLES AS NECESSARY (NO SEPARATE PAY)
 - 13 PROP. 6" - 4" THICK CONCRETE SIDEWALK
 - 14 PROP. CURB RAMP PER ADA REQUIREMENTS
 - 15 REMOVE TRAFFIC SIGNAL BOX



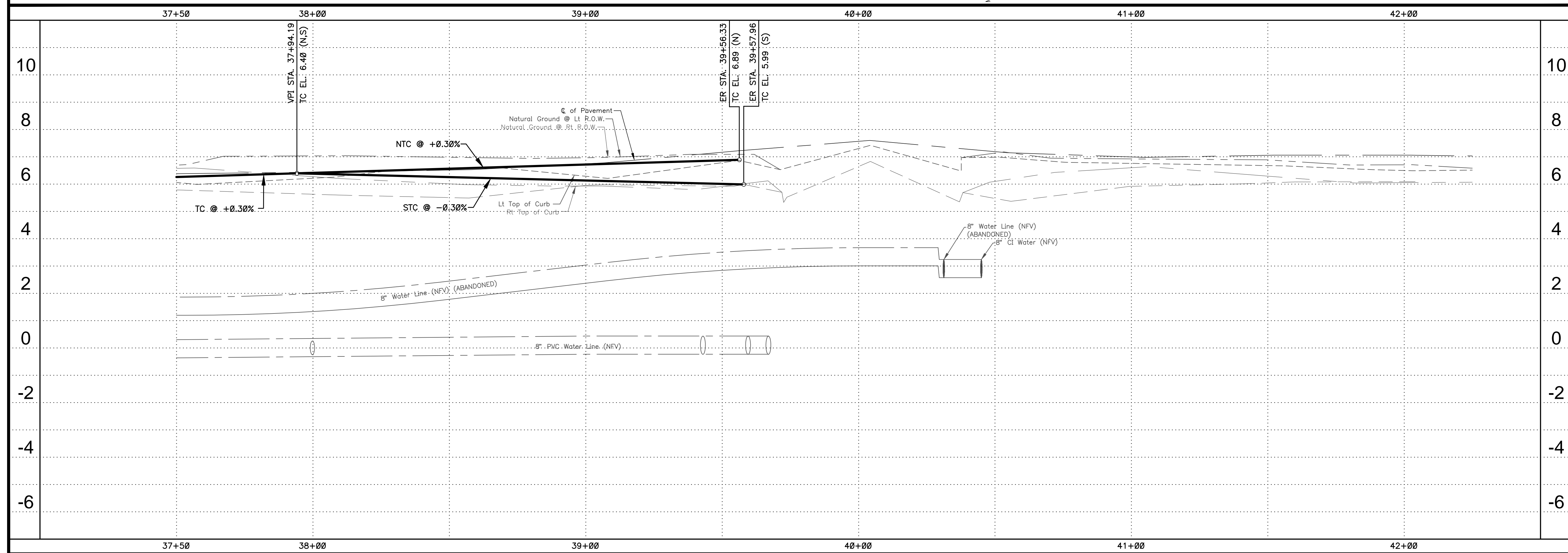
REMOVE 27 SY OF ASPHALT PAVEMENT (FILL & SOD AREA)

PT. NO	NORTHING	EASTING	ELEVATION	DESCRIPTION
CP 9	13710058.04	3273093.45	6.91	MAG NAIL

NOTE:
LOCATION OF FIRE HYDRANTS AND WATER VALVES SHOWN ARE APPROXIMATE. ADJUSTMENT TO PROPOSED SIDEWALK & DRIVEWAYS DUE TO LOCATION OF FIRE HYDRANTS & VALVES MAY BE REQUIRED.

- PROP. CONCRETE DRIVEWAY
- PROP. 4" CONCRETE SIDEWALK
- PROP. 4" CONCRETE PAVEMENT
- PROP. ASPHALT PAVEMENT
- PROP. REMOVE PAVEMENT
- PROP. LIMITS OF HIGH EARLY CONCRETE

#	STATION	OFFSET
64	PT 37+94.20	31.80' LT.
65	PT 37+94.20	32.00' RT.
66	PT 39+01.80	32.00' RT.
67	PT 39+56.30	31.90' LT.
68	PT 39+57.90	33.40' RT.



MK.	DESCRIPTION	DATE	DWN.	CHK.

9-13-19

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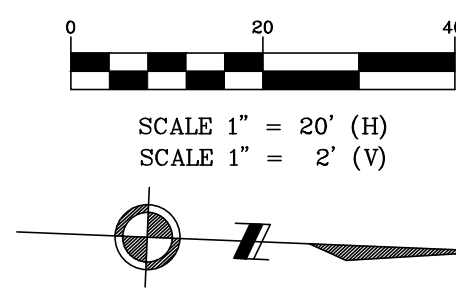
Galveston County, Texas

Texas Avenue Reconstruction

Texas Ave.
Sta. 37+50 to End

Job No.: 18-015	Scale: HORIZ: 1" = 20'	SHEET 15 OF 52
Date: September, 2019	VERT: 1" = 2'	
Dwn By: D. Fattig		
Chkd By: J. Rudloff		

(PPCS LIMITS 3+00-14+00)



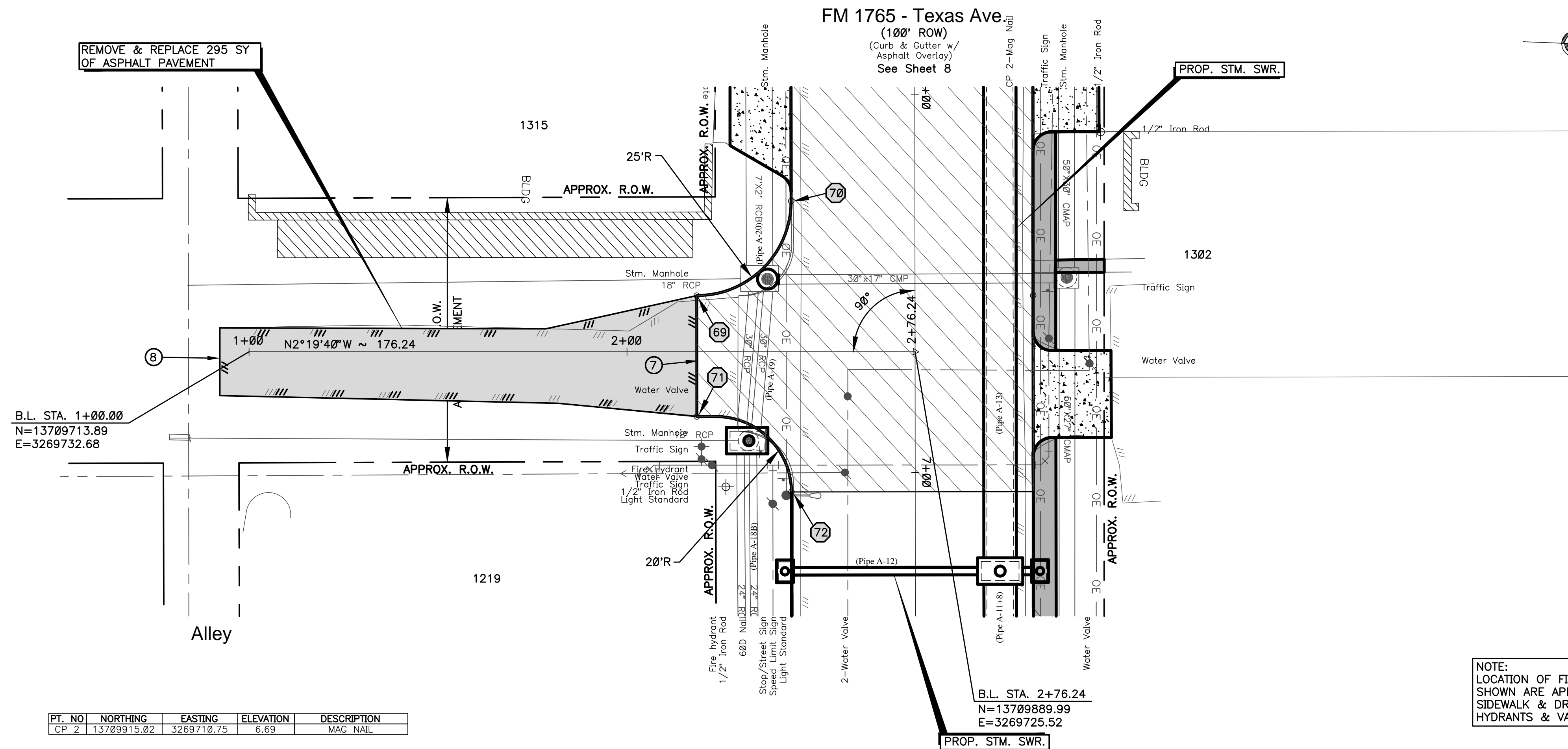
BENCHMARK:
SEE SURVEY/BASELINE CONTROL MAPS FOR BENCHMARK REFERENCES/ BASELINE DATA. (SHEET 5)

- PAVING & DRAINAGE LEGEND:**
- 1 REMOVE EXIST. STM. SWR./CULVERT
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 - 13 PROP. 6" - 4" THICK CONCRETE SIDEWALK
 - 14 PROP. CURB RAMP PER ADA REQUIREMENTS
 - 15 REMOVE TRAFFIC SIGNAL BOX

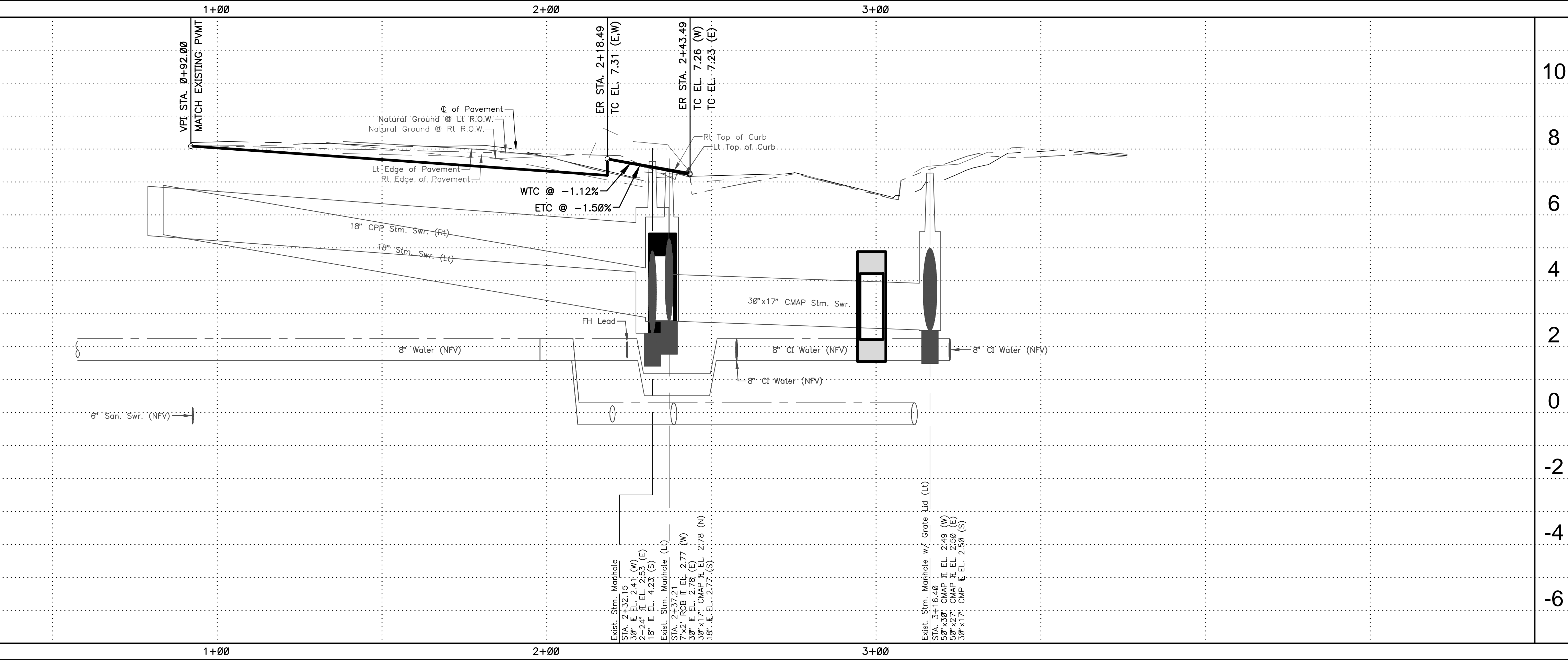
- PROP. CONCRETE DRIVEWAY
- PROP. 4" CONCRETE SIDEWALK
- PROP. 4" CONCRETE PAVEMENT
- PROP. ASPHALT PAVEMENT
- PROP. REMOVE PAVEMENT
- PROP. LIMITS OF HIGH EARLY CONCRETE

#	STATION	OFFSET
69	PT 2+18.50	14.80' LT.
70	PT 2+43.50	39.80' LT.
71	PT 2+18.50	17.10' RT.
72	PT 2+43.50	37.10' RT.

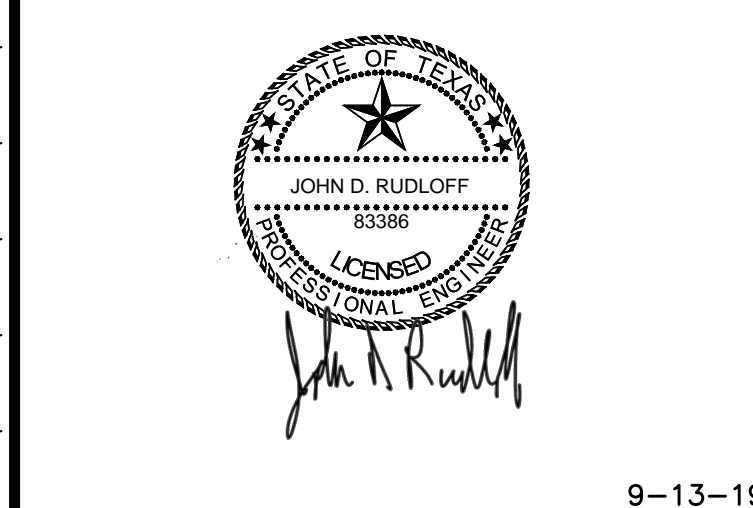
NOTE:
LOCATION OF FIRE HYDRANTS AND WATER VALVES SHOWN ARE APPROXIMATE. ADJUSTMENT TO PROPOSED SIDEWALK & DRIVEWAYS DUE TO LOCATION OF FIRE HYDRANTS & VALVES MAY BE REQUIRED.



PT. NO	NORTHING	EASTING	ELEVATION	DESCRIPTION
CP 2	13709915.02	3269710.75	6.69	MAG NAIL



MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19
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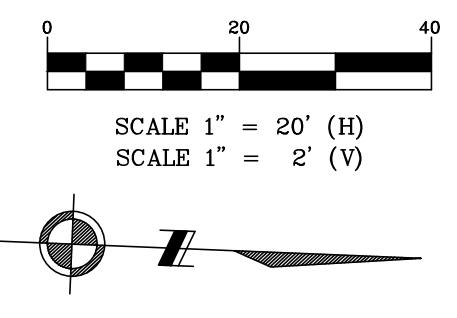
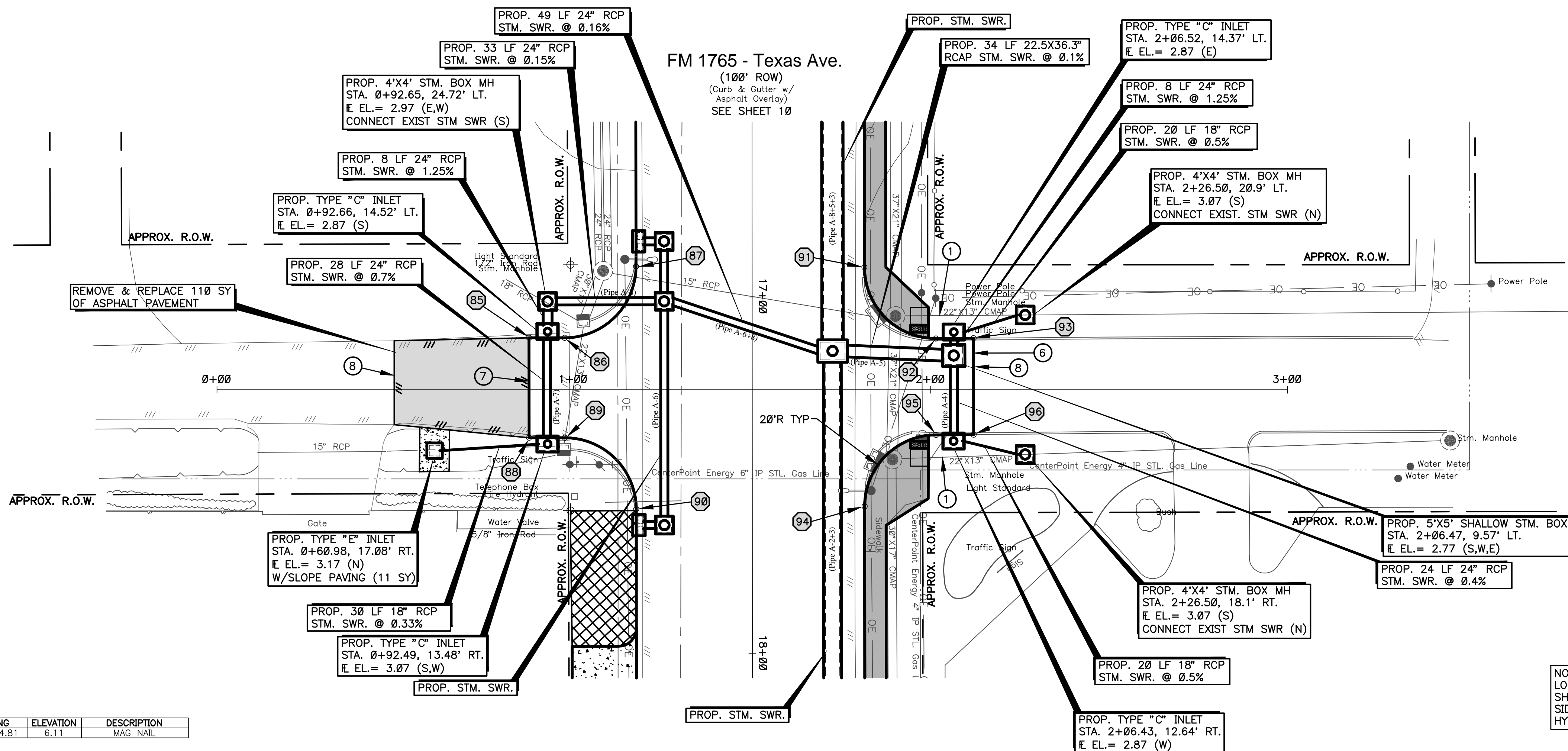
Galveston County, Texas

Texas Avenue Reconstruction

13th Street S.
Sta. 1+00 to End

Job No.: 18-015	Scale:	SHEET
Date: September, 2019	HORIZ: 1" = 20' VERT: 1" = 2'	
Dwn By: D. Fattig		16
Chkd By: J. Rudloff		

OF 52



BENCHMARK:
SEE SURVEY/BASELINE CONTROL MAPS FOR BENCHMARK REFERENCES/ BASELINE DATA. (SHEET 5)

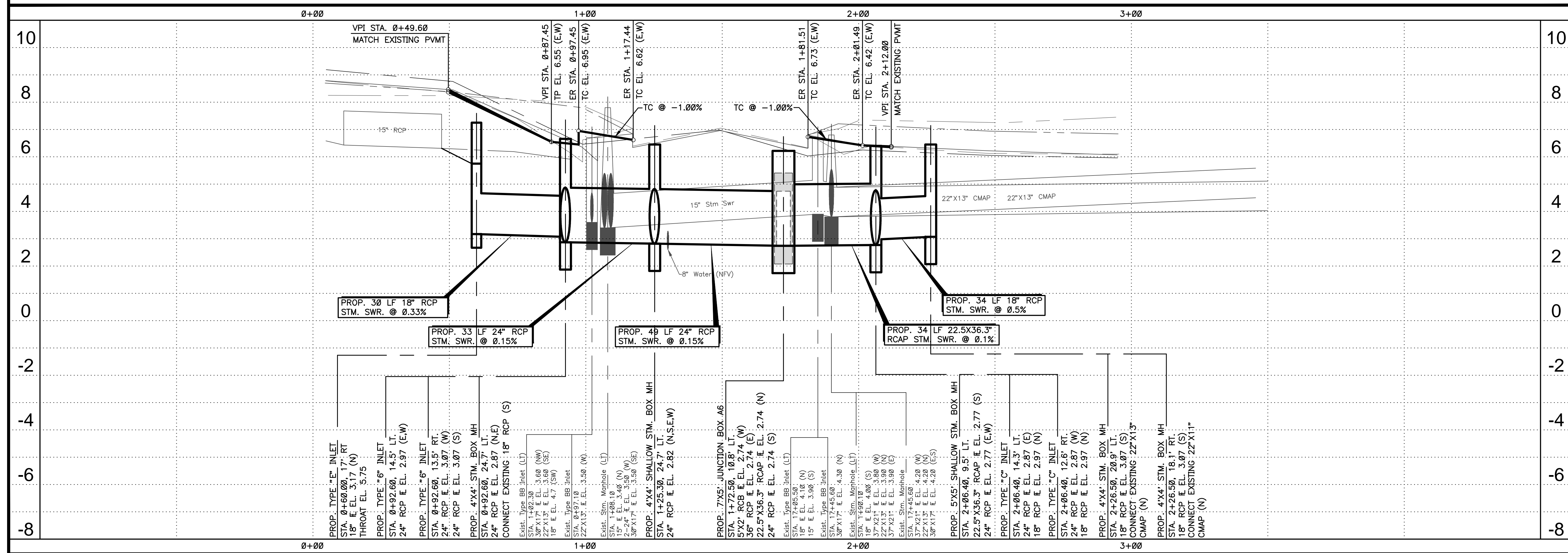
- PAVING & DRAINAGE LEGEND:**
- 1 REMOVE EXIST. STM. SWR./CULVERT
 - 2 REMOVE EXIST. INLET/MANHOLE
 - 3 REMOVE AND DISPOSE OF EXISTING ASPH./CONC. PAVEMENT AND BASE COURSE.
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 - 5A PROP. REMOVE AND REPLACE WITH 8" CONCRETE DRIVEWAY
 - 6 PROP. CONCRETE PAVING HEADER AT EXIST. CONCRETE ROAD
 - 7 PROP. CONCRETE PAVING HEADER AT ASPHALT ROAD
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 - 11 PROP. 4" THICK CONCRETE PAVEMENT
 - 12 PROTECT & BRACE LIGHT/POWER POLES AS NECESSARY (NO SEPARATE PAY)
 - 13 PROP. 6" - 4" THICK CONCRETE SIDEWALK
 - 14 PROP. CURB RAMP PER ADA REQUIREMENTS
 - 15 REMOVE TRAFFIC SIGNAL BOX

#	STATION	OFFSET
85	PT 0+87.40	14.50' LT.
86	PT 0+97.40	14.50' LT.
87	PT 1+17.40	34.50' LT.
88	PT 0+87.40	13.50' RT.
89	PT 0+97.50	13.50' RT.
90	PT 1+17.50	33.40' RT.
91	PT 1+81.40	34.30' LT.
92	PT 2+01.40	14.30' LT.
93	PT 2+12.00	14.40' LT.
94	PT 1+81.50	32.70' RT.
95	PT 2+01.50	12.70' RT.
96	PT 2+12.00	12.60' RT.

- PROP. CONCRETE DRIVEWAY
- PROP. 4" CONCRETE SIDEWALK
- PROP. 4" CONCRETE PAVEMENT
- PROP. ASPHALT PAVEMENT
- PROP. REMOVE PAVEMENT
- PROP. LIMITS OF HIGH EARLY CONCRETE

NOTE: LOCATION OF FIRE HYDRANTS AND WATER VALVES SHOWN ARE APPROXIMATE. ADJUSTMENT TO PROPOSED SIDEWALK & DRIVEWAYS DUE TO LOCATION OF FIRE HYDRANTS & VALVES MAY BE REQUIRED.

PT. NO	NORTHING	EASTING	ELEVATION	DESCRIPTION
CP 3	13709937.43	3270194.81	6.11	MAG NAIL



MK.	DESCRIPTION	DATE	DWN.	CHK.

9-13-19

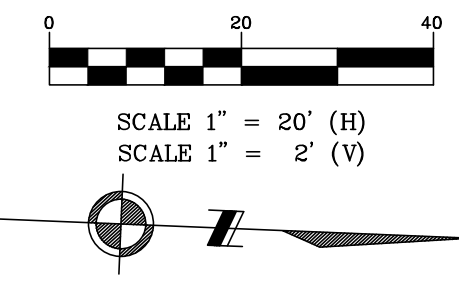
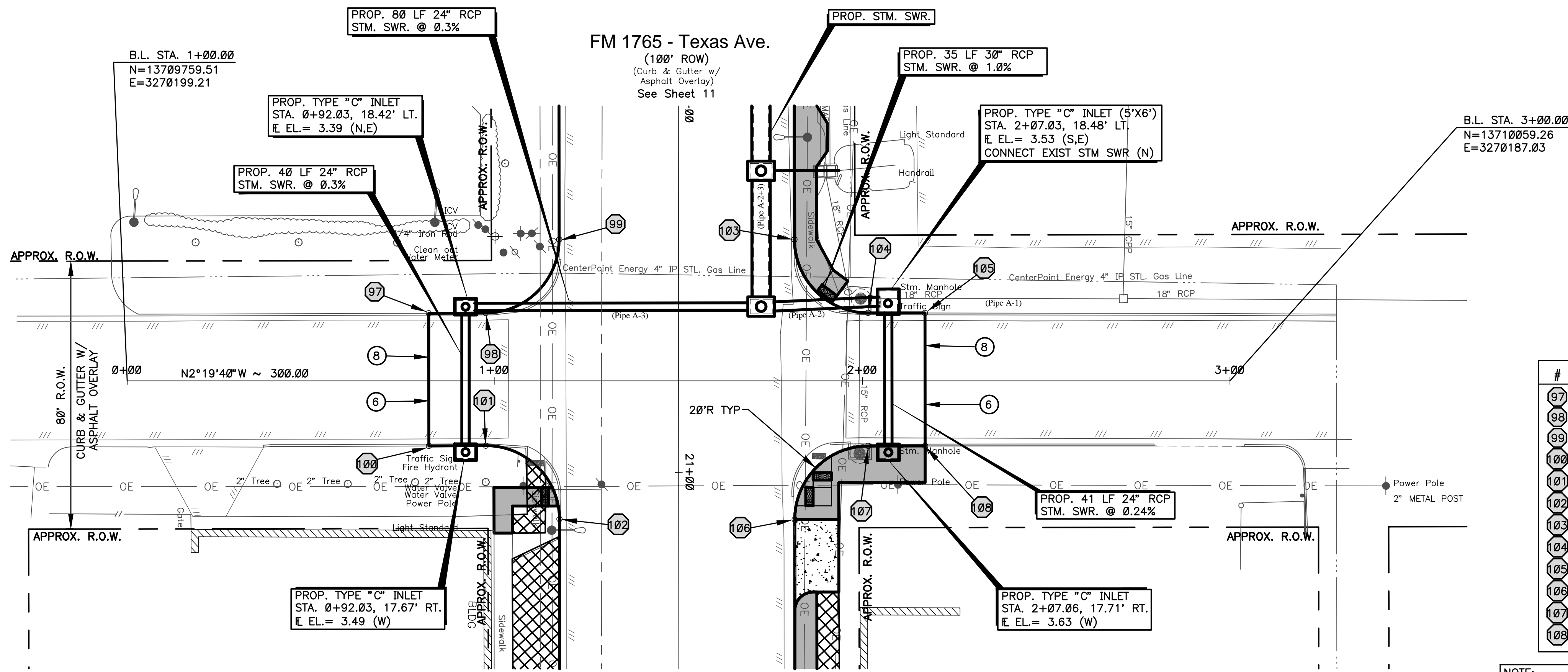
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Galveston County, Texas

Texas Avenue Reconstruction

11th Street
Sta. 0+00 to End

Job No.: 18-015	Scale: HORIZ: 1" = 20'	SHEET 18
Date: September, 2019	VERT: 1" = 2'	
Dwn By: D. Fattig		OF 52
Chkd By: J. Rudloff		

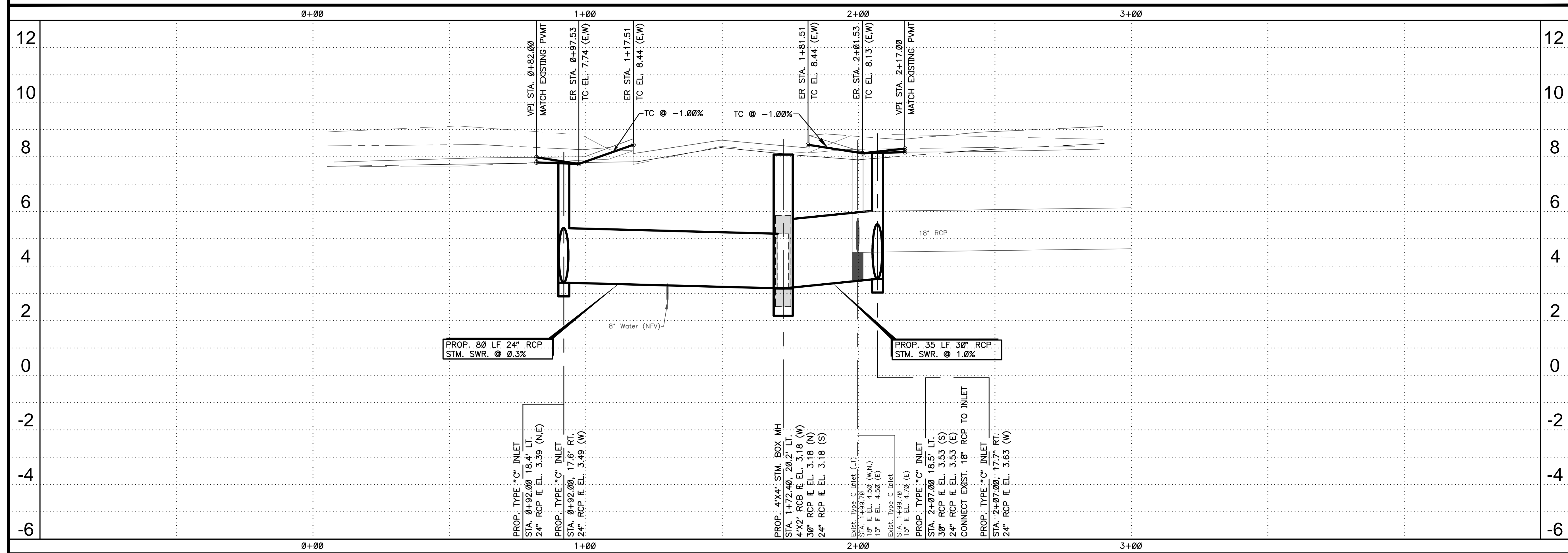


- BENCHMARK:**
SEE SURVEY/BASELINE CONTROL MAPS FOR BENCHMARK REFERENCES/ BASELINE DATA. (SHEET 5)
- PAVING & DRAINAGE LEGEND:**
- 1 REMOVE EXIST. STM. SWR./CULVERT
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 - 12 PROTECT & BRACE LIGHT/POWER POLES AS NECESSARY (NO SEPARATE PAY)
 - 13 PROP. 6" - 4" THICK CONCRETE SIDEWALK
 - 14 PROP. CURB RAMP PER ADA REQUIREMENTS
 - 15 REMOVE TRAFFIC SIGNAL BOX

#	STATION	OFFSET
97	PT 0+82.00	18.40' LT.
98	PT 0+97.50	18.40' LT.
99	PT 1+17.50	38.40' LT.
100	PT 0+82.00	17.70' RT.
101	PT 0+97.50	17.60' RT.
102	PT 1+17.50	37.60' RT.
103	PT 1+81.50	38.50' LT.
104	PT 2+01.50	18.50' LT.
105	PT 2+17.00	18.40' LT.
106	PT 1+81.60	37.70' RT.
107	PT 2+01.50	17.70' RT.
108	PT 2+17.00	17.70' RT.

NOTE:
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PT. NO	NORTHING	EASTING	ELEVATION	DESCRIPTION
CP 3	13709937.43	3270194.81	6.11	MAG NAIL



MK.	DESCRIPTION	DATE	DWN.	CHK.

9-13-19

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Galveston County, Texas

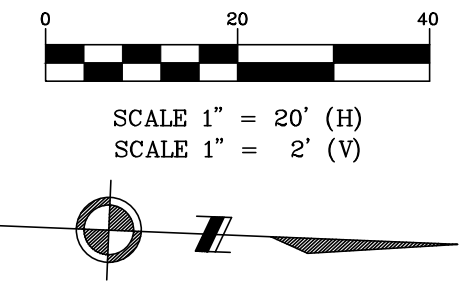
Texas Avenue Reconstruction

10th Street
Sta. 0+00 to End

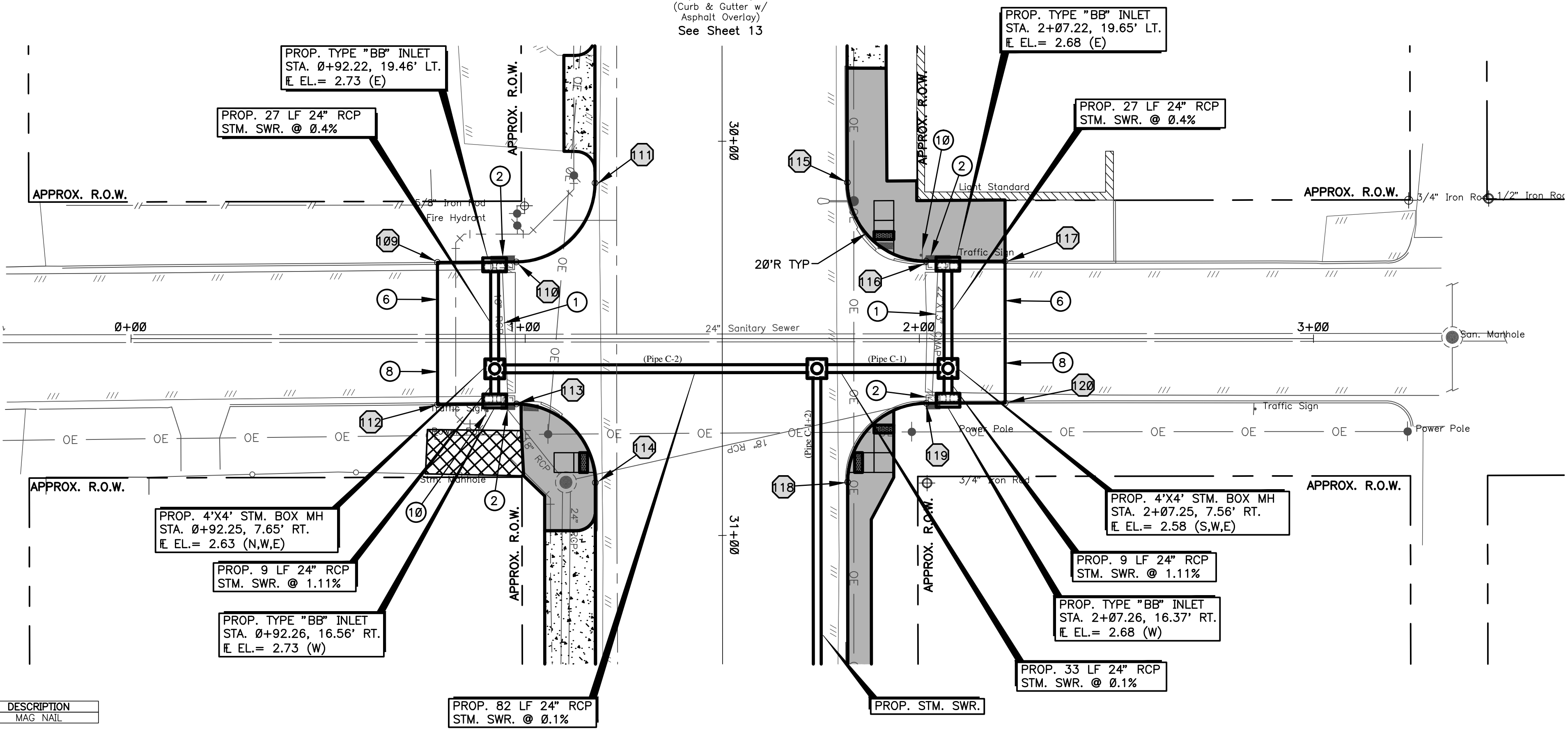
Job No.: 18-015	Scale:	SHEET
Date: September, 2019	HORIZ: 1" = 20'	
Dwn By: D. Fattig	VERT: 1" = 2'	19
Chkd By: J. Rudloff		

OF 52

FM 1765 - Texas Ave.
(100' ROW)
(Curb & Gutter w/
Asphalt Overlay)
See Sheet 13



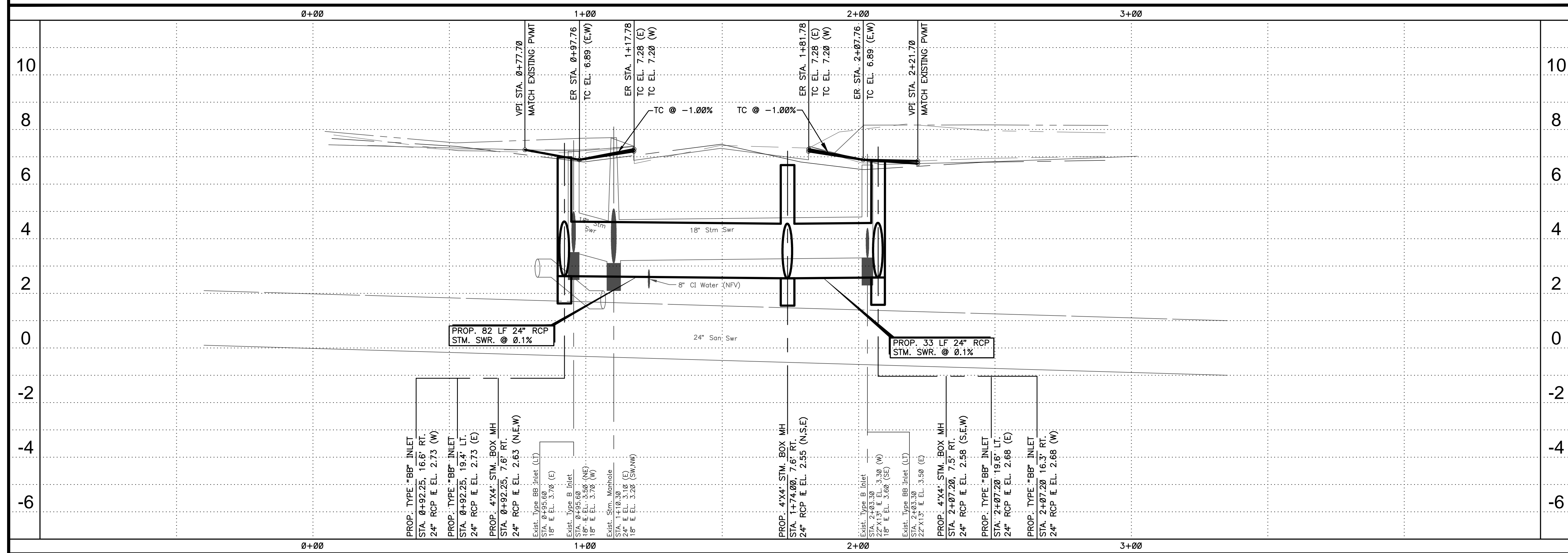
- BENCHMARK:**
SEE SURVEY/BASELINE CONTROL MAPS FOR BENCHMARK REFERENCES/ BASELINE DATA. (SHEET 5)
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- 1 REMOVE EXIST. STM. SWR./CULVERT
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 - 13 PROP. 6" - 4" THICK CONCRETE SIDEWALK
 - 14 PROP. CURB RAMP PER ADA REQUIREMENTS
 - 15 REMOVE TRAFFIC SIGNAL BOX



#	STATION	OFFSET
109	PT 0+77.70	19.30' LT.
110	PT 0+97.70	19.50' LT.
111	PT 1+17.70	39.50' LT.
112	PT 0+77.70	16.70' RT.
113	PT 0+97.70	16.50' RT.
114	PT 1+17.80	36.50' RT.
115	PT 1+81.70	39.60' LT.
116	PT 2+01.70	19.60' LT.
117	PT 2+21.70	19.60' LT.
118	PT 1+81.80	36.40' RT.
119	PT 2+01.70	16.40' RT.
120	PT 2+21.70	16.30' RT.

NOTE:
LOCATION OF FIRE HYDRANTS AND WATER VALVES SHOWN ARE APPROXIMATE. ADJUSTMENT TO PROPOSED SIDEWALK & DRIVEWAYS DUE TO LOCATION OF FIRE HYDRANTS & VALVES MAY BE REQUIRED.

PT. NO	NORTHING	EASTING	ELEVATION	DESCRIPTION
CP 3	13709937.43	3270194.81	6.11	MAG NAIL



MK.	DESCRIPTION	DATE	DWN.	CHK.

9-13-19

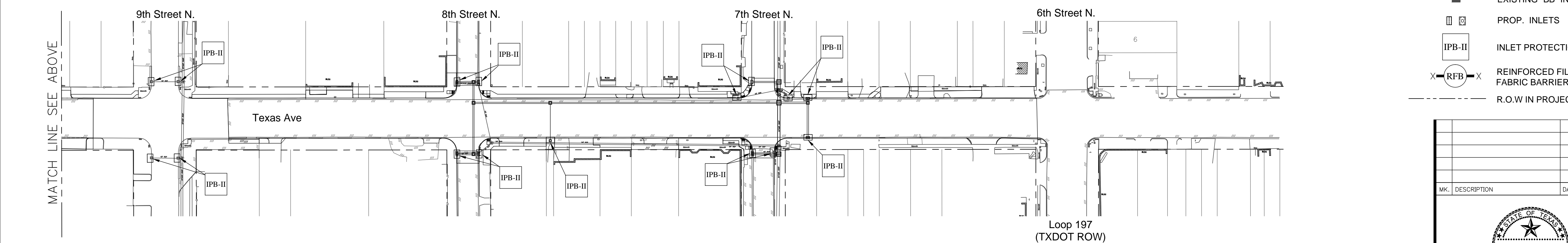
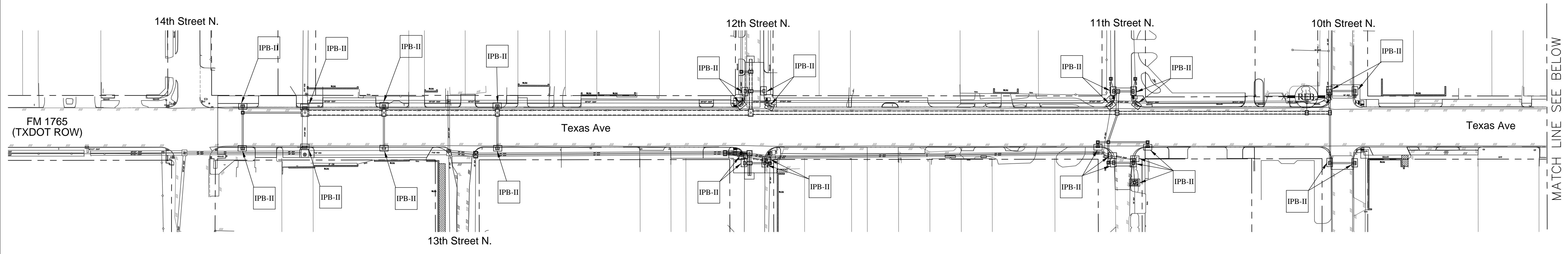
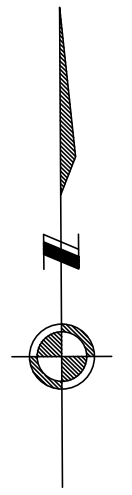
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Galveston County, Texas

Texas Avenue Reconstruction

8th Street
Sta. 0+00 to End

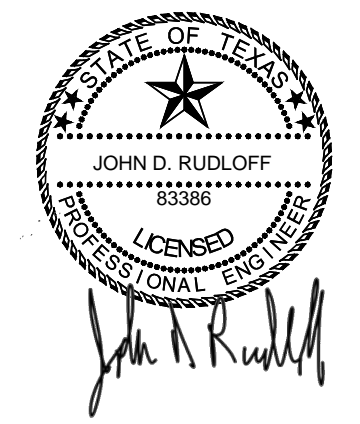
Job No.: 18-015 Scale: SHEET
Date: September, 2019 HORZ: 1" = 20' 20
Dwn By: D. Fattig VERT: 1" = 2' OF 52
Chkd By: J. Rudloff



LEGEND

- EXISTING STORM SEWER
- EXISTING MANHOLE
- EXISTING "A" INLET
- EXISTING "BB" INLET
- PROP. INLETS
- IPB-II INLET PROTECTION BARRIER
- ⊗ RFB ⊗ REINFORCED FILTER FABRIC BARRIER
- - - R.O.W IN PROJECT AREA

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19

EROSION & SEDIMENTATION CONTROL NOTES:

1. PRIOR TO START OF CONSTRUCTION, CONTRACTOR SHALL INSTALL EROSION AND SEDIMENTATION CONTROLS AT LOCATION SHOWN ON PLANS.
2. CONTRACTOR SHALL MAINTAIN, REPAIR AND/OR REPLACE DAMAGED EROSION AND SEDIMENTATION CONTROL SYSTEM THROUGHOUT THE DURATION OF THE CONTRACT. (NO SEPARATE PAY).
3. CONTRACTOR SHALL PROVIDE PROTECTED STORAGE AREAS FOR CHEMICALS, PAINTS, SOLVENTS, FERTILIZERS, AND OTHER POTENTIALLY TOXIC MATERIALS.
4. CONTRACTOR SHALL LOCATE FUEL/MATERIAL STORAGE AREAS AWAY FROM STORM WATER CONVEYANCE SYSTEMS. CONTRACTOR SHALL USE BERMS AROUND FUEL STORAGE AREAS. (NO SEPARATE PAY).
5. CONTRACTOR SHALL ADVISE OWNER IMMEDIATELY, VERBALLY, AND IN WRITING, OF ANY FUEL OR TOXIC MATERIAL SPILLS ONTO THE PROJECT AREA AND THE ACTION TAKEN TO REMEDY THE PROBLEM.
6. CONTRACTOR IS RESPONSIBLE FOR DISPOSING OF HIS FUELS, MATERIALS, AND CONTAMINATED EXCAVATIONS IN A LEGALLY APPROVED MANNER. (NO SEPARATE PAY). NO DISPOSAL SHALL BE PERMITTED ON PROJECT SITE.
7. CONTRACTOR IS RESPONSIBLE FOR COMPLYING WITH ALL APPLICABLE ENVIRONMENTAL LAWS.
8. CONTRACTOR IS RESPONSIBLE FOR PROVIDING ADEQUATELY MAINTAINED SANITARY FACILITIES.
9. AT COMPLETION OF THE CONTRACT, OWNER AND/OR OWNER'S REPRESENTATIVE WITH THE CONTRACTOR SHALL EXAMINE EROSION AND SEDIMENTATION CONTROL SYSTEM BEFORE RELIEVING CONTRACTOR OF HIS MAINTENANCE RESPONSIBILITIES.
10. CONTRACTOR SHALL BE RESPONSIBLE FOR STREET CLEANING, ON A DAILY BASIS, OF ALL MUD AND DIRT DEPOSITED ON THE EXISTING PAVEMENT DUE TO HIS CONSTRUCTION ACTIVITY.
11. INLETS AND MANHOLES THAT ARE NOT COMPLETE AND/OR ARE SUBJECT TO CONVEYING STORM WATER FLOWS ARE TO BE PROTECTED TO PREVENT SEDIMENT FROM ENTERING THE PROPOSED OR EXISTING STORM SEWER SYSTEM.
12. IF PAVING CONTRACTOR REMOVES OR PUNCTURES TIMBER GRATE TO ESTABLISH DRAINAGE, INLET MUST BE SURROUNDED BY INLET FILTER FABRIC AS SHOWN IN DETAILS.
13. FILTER FABRIC TO BE CLEANED OR REPLACED WHEN IT CEASES TO FUNCTION PROPERLY OR AS DIRECTED BY THE ENGINEER.
14. LOCATION OF CONSTRUCTION ACCESS IS APPROXIMATE. EXACT LOCATION SHALL BE BASED ON THE ACTUAL SEQUENCING OF WORK AND LOCATIONS FOR EGRESS OF THE SITE BY THE CONTRACTOR.



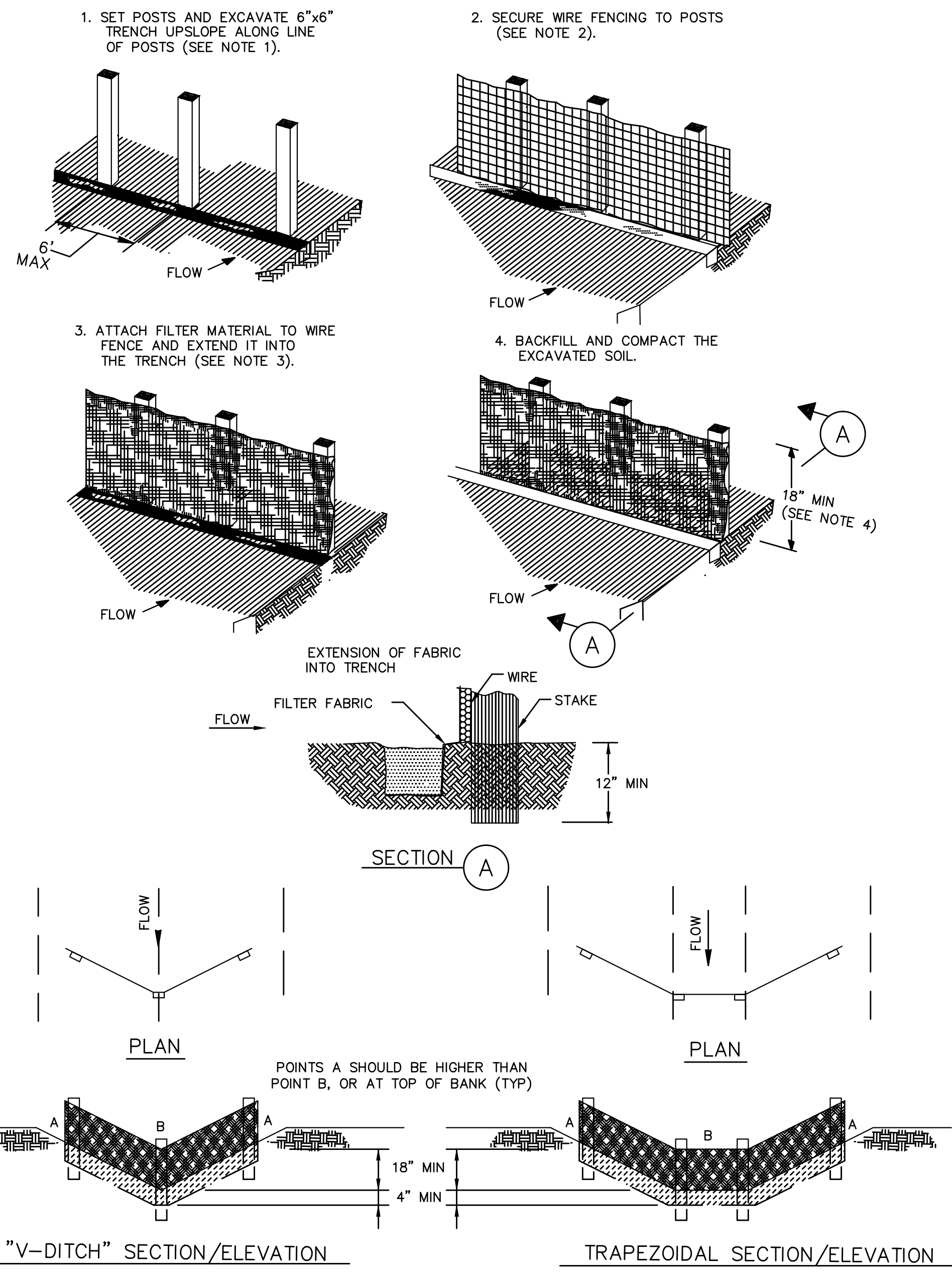
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Galveston County, Texas

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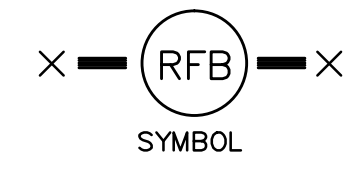
Stormwater Pollution Prevention Plan

Job No.: 18-015	Scale: HORZ: 1" = 80'	SHEET 22 OF 52
Date: September, 2019	VERT:	
Dwn By: D. Fattig		
Chkd By: J. Rudloff		

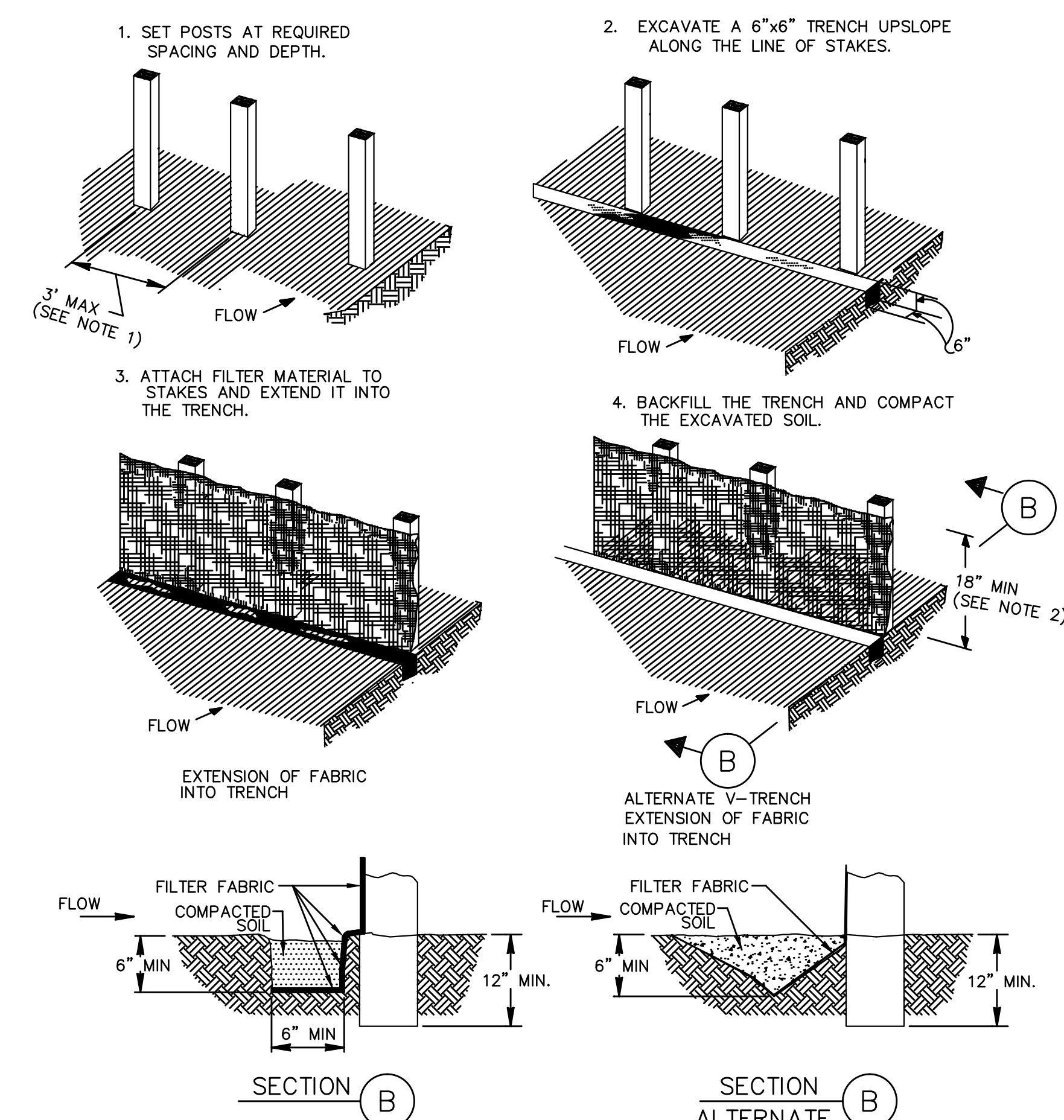


CONSTRUCTION NOTES:

1. SET 2 INCH BY 2 INCH WOODEN STAKES SPACED A MAX OF 6 FEET APART AND EMBEDDED A MIN OF 12 INCHES.
2. WOVEN WIRE FENCE TO BE FASTENED SECURELY TO FENCE POSTS WITH STAPLES.
3. FILTER CLOTH TO BE FASTENED SECURELY TO WOVEN WIRE FENCE, WITH TIES SPACED EVERY 24 INCHES AT TOP AND MIDSECTION.
4. MINIMUM HEIGHT OF FILTER SHOULD BE 18 INCHES AND A MAXIMUM OF 36 INCHES ABOVE NATURAL GROUND.
5. WHEN TWO SECTIONS OF FILTER CLOTH ADJOIN EACH OTHER THEY SHALL BE OVERLAPPED 6 INCHES AT THE POSTS, AND FOLDED.
6. SEE SPECIFICATION FOR FILTER FABRIC BARRIER.

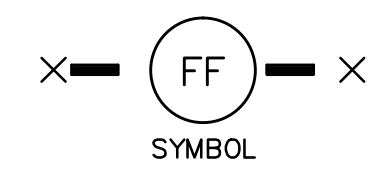


REINFORCED FILTER FABRIC BARRIER

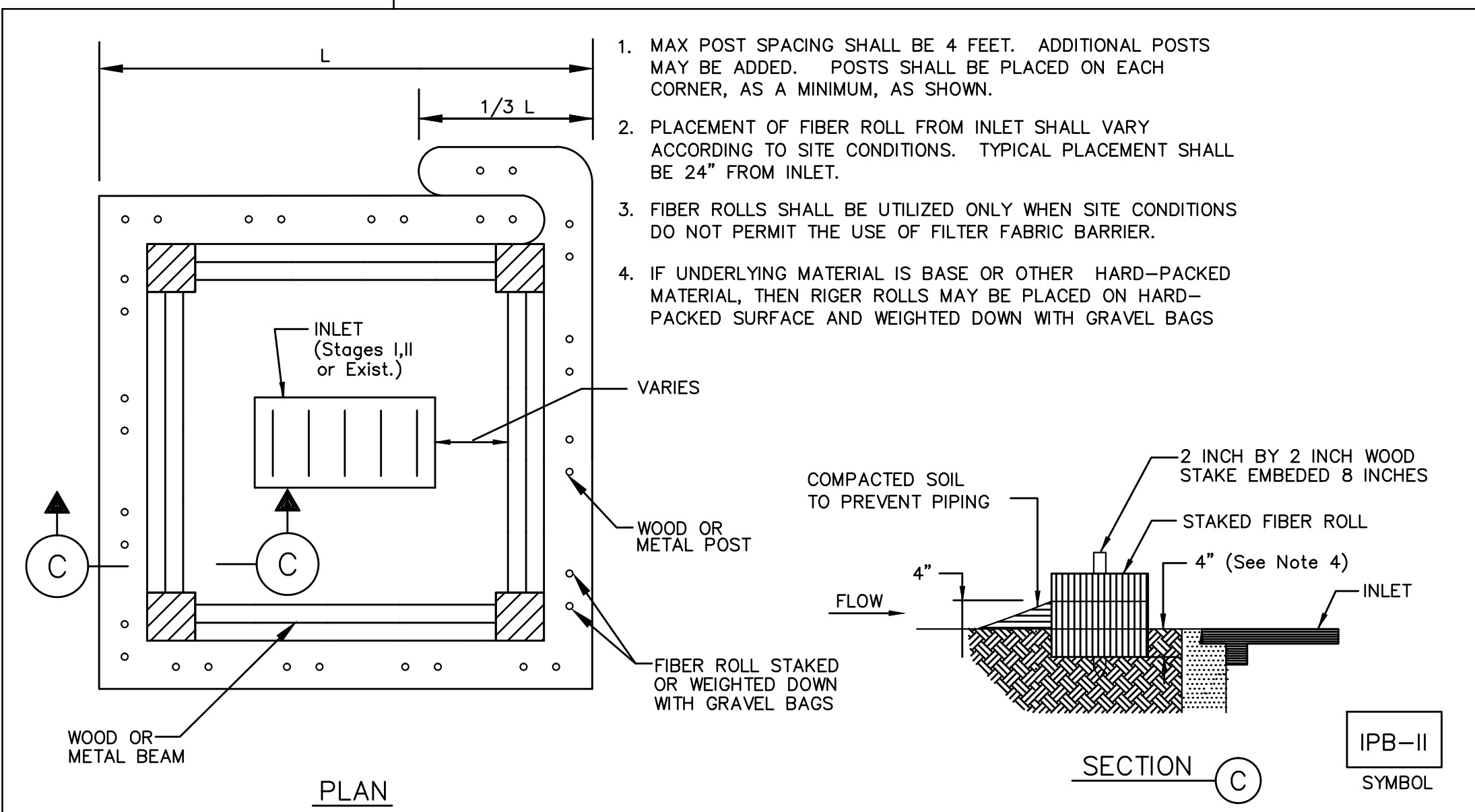


CONSTRUCTION NOTES:

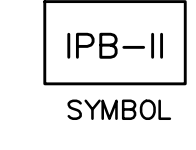
1. 2 INCH THICK BY 2 INCH WOODEN STAKES TO BE SET AT MAX SPACING OF 3 FEET AND EMBEDDED A MIN OF 12 INCHES. IF PREASSEMBLED FENCE WITH SUPPORT NETTING IS USED, SPACING OF POST MAY BE INCREASED TO 6 FEET MAX.
2. ATTACH FILTER FABRIC TO WOODEN STAKES. FILTER FABRIC FENCE SHALL HAVE A MIN HEIGHT OF 18 INCHES AND MAX HEIGHT OF 36 INCHES ABOVE NATURAL GROUND.
3. WHEN TWO SECTIONS OF FILTER CLOTH ADJOIN EACH OTHER THEY SHOULD BE OVERLAPPED 6 INCHES AT THE POSTS, AND FOLDED.
4. SEE SPECIFICATION FOR FILTER FABRIC FENCE.



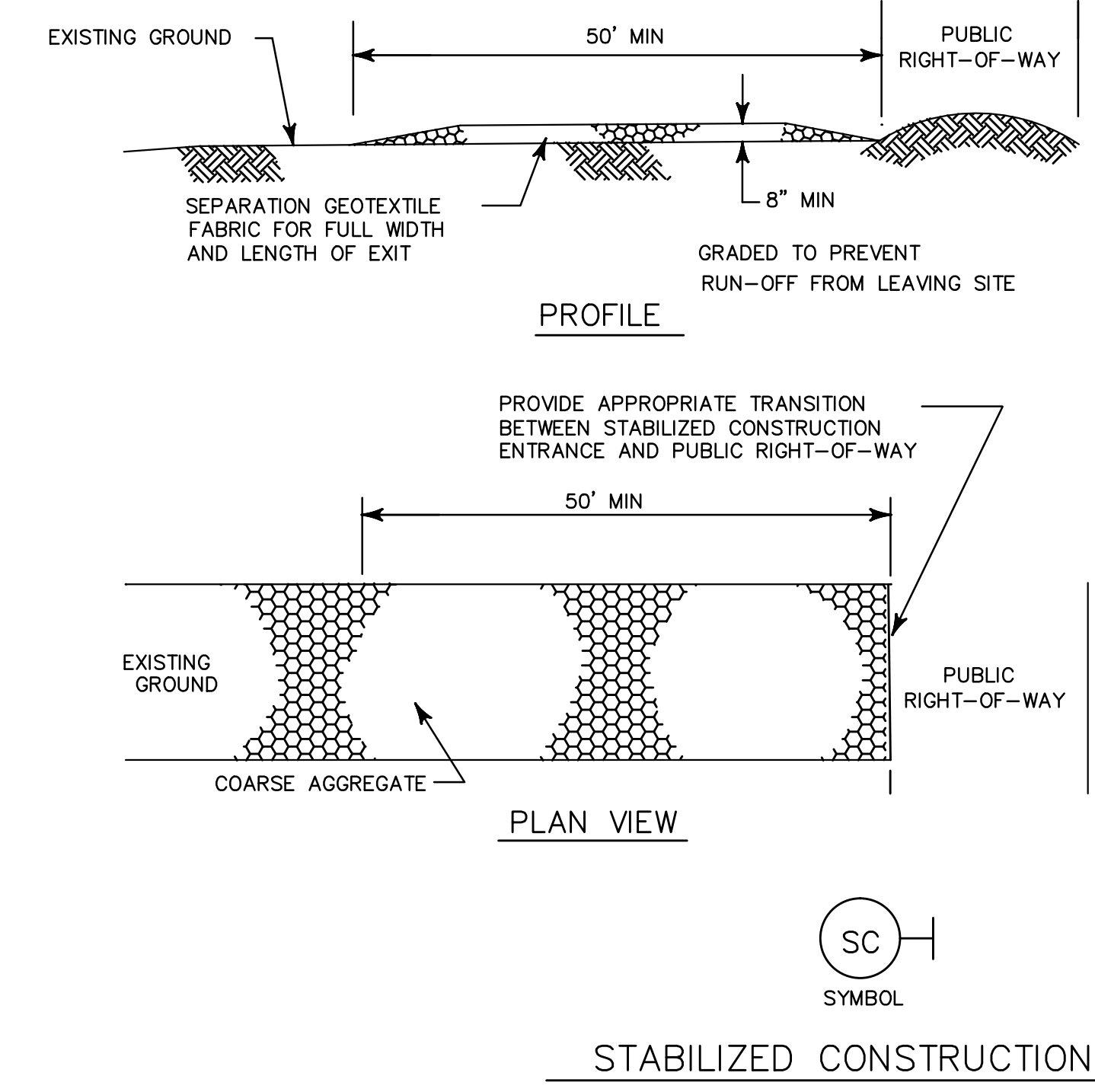
FILTER FABRIC FENCE



FIBER ROLL INLET PROTECTION BARRIER



INLET PROTECTION BARRIER (FOR EXISTING & PROPOSED STAGE II INLETS)



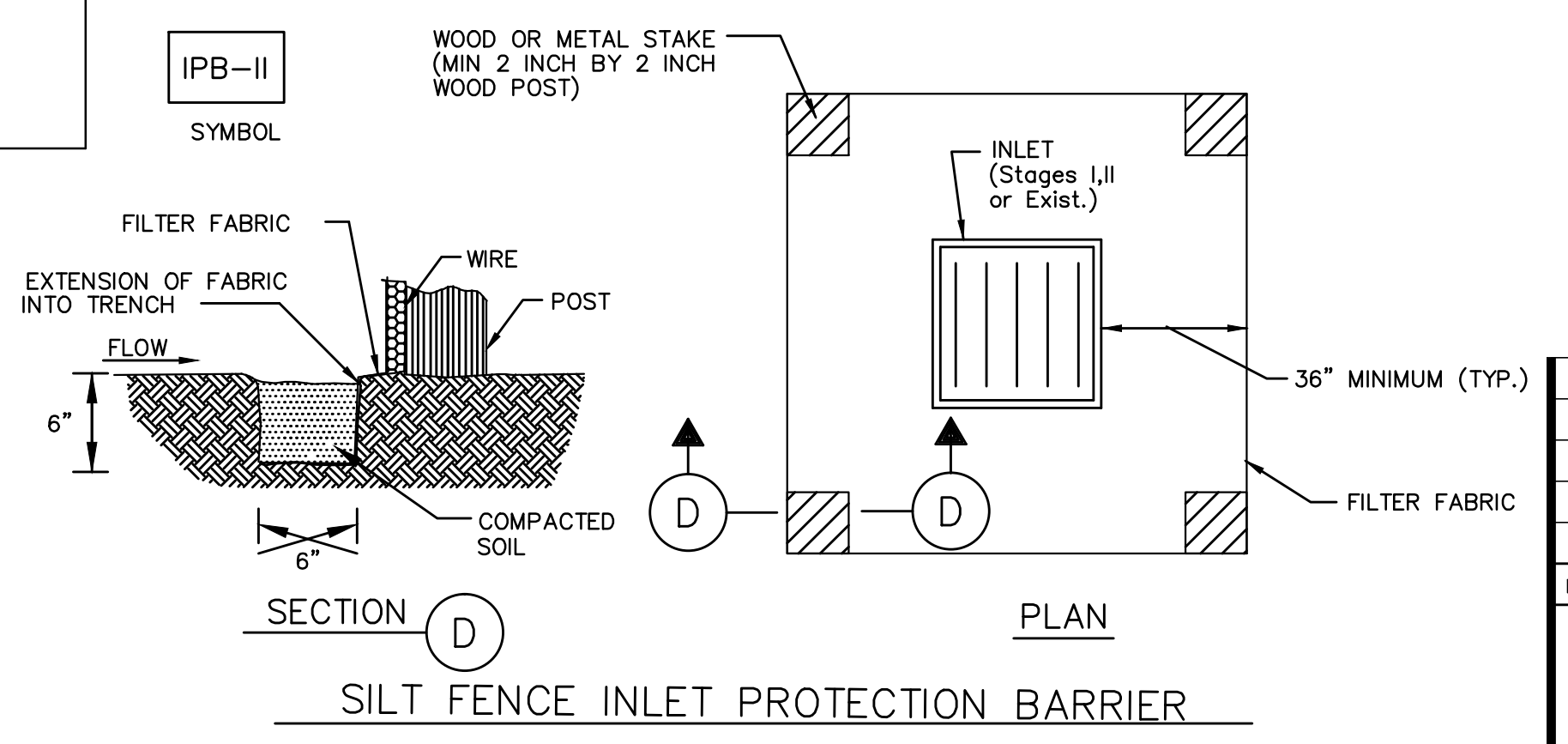
STABILIZED CONSTRUCTION EXIT

CONSTRUCTION NOTES:

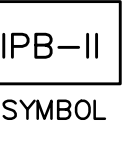
1. LENGTH SHALL BE AS SHOWN ON THE CONSTRUCTION DRAWINGS, BUT NOT LESS THAN 50 FEET.
2. THICKNESS SHALL BE NOT LESS THAN 8 INCHES.
3. WIDTH SHALL BE NOT LESS THAN FULL WIDTH OF ALL POINTS OF INGRESS OR EGRESS.
4. STABILIZATION FOR OTHER AREAS SHALL HAVE THE SAME AGGREGATE THICKNESS AND WIDTH REQUIREMENTS AS THE STABILIZED CONSTRUCTION EXIT, UNLESS OTHERWISE SHOWN ON THE CONSTRUCTION DRAWINGS.
5. STABILIZED AREA MAY BE WIDENED OR LENGTHENED TO ACCOMMODATE A TRUCK WASHING AREA. AN OUTLET SEDIMENT TRAP MUST BE PROVIDED FOR THE TRUCK WASHING AREA.
6. SEE SPECIFICATION FOR STABILIZED CONSTRUCTION EXIT.
7. STABILIZED CONSTRUCTION EXIT SHALL BE MAINTAINED FREE OF SEDIMENT FOR THE DURATION OF THE PROJECT.

CONSTRUCTION NOTE:

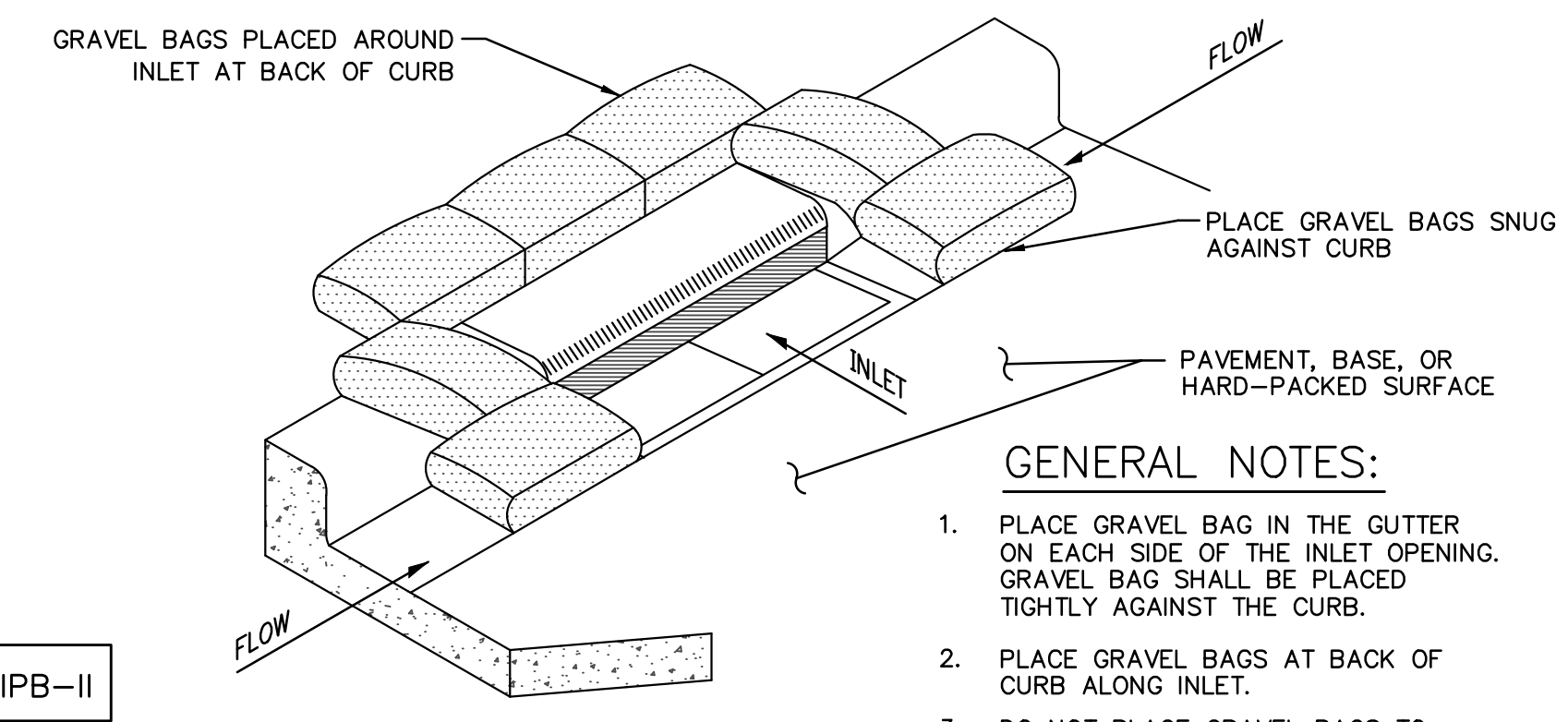
1. MAX. POST SPACING SHALL BE 4 FEET. ADDITIONAL POSTS MAY BE ADDED. POSTS SHALL BE PLACED ON EACH CORNER, AS A MINIMUM, AS SHOWN.
2. PLACEMENT OF FILTER FABRIC BARRIER FROM INLET SHALL VARY ACCORDING TO SITE CONDITIONS. TYPICAL PLACEMENT SHALL BE 36" MINIMUM FROM INLET EDGE.



SILT FENCE INLET PROTECTION BARRIER



INLET PROTECTION BARRIER (FOR EXISTING & PROPOSED STAGE II INLETS)



GENERAL NOTES:

1. PLACE GRAVEL BAG IN THE GUTTER ON EACH SIDE OF THE INLET OPENING. GRAVEL BAG SHALL BE PLACED TIGHTLY AGAINST THE CURB.
2. PLACE GRAVEL BAGS AT BACK OF CURB ALONG INLET.
3. DO NOT PLACE GRAVEL BAGS TO BLOCK THROAT OF INLET, UNLESS DIRECTED BY ENGINEER.

MK.	DESCRIPTION	DATE	DWN.	CHK.

STATE OF TEXAS
 JOHN D. RUDLOFF
 LICENSED PROFESSIONAL ENGINEER
 83386
 John D. Rudloff

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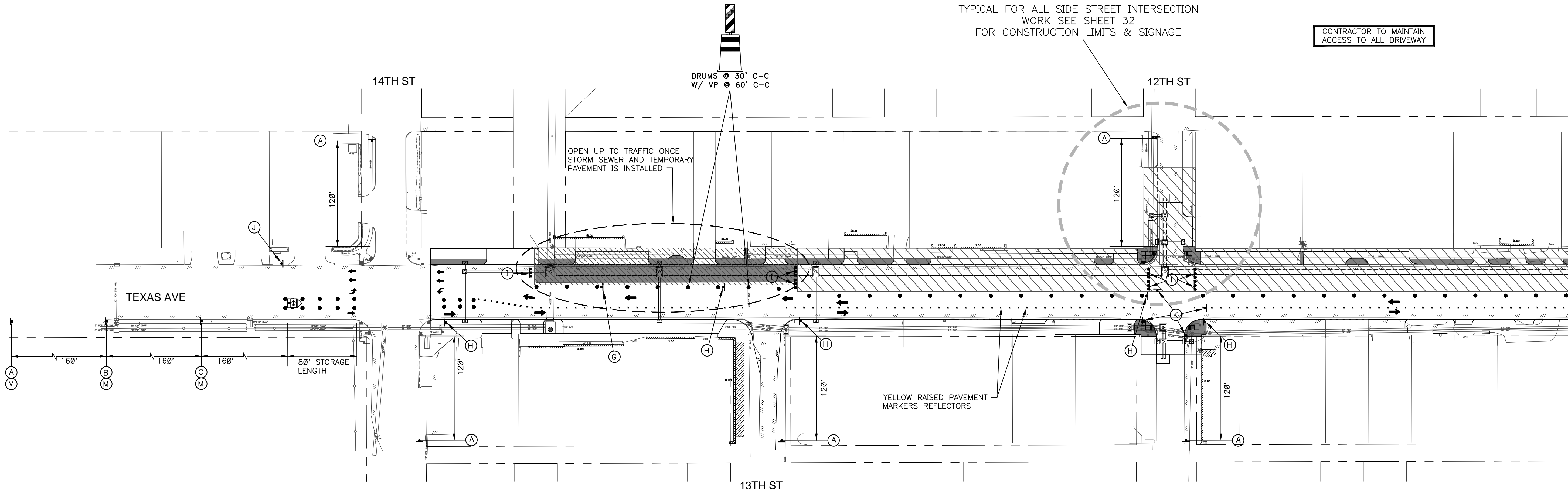
Texas Avenue Reconstruction

SWPPP Details

Job No.: 18-015	Scale: N/A	SHEET
Date: September, 2019	HORZ: N/A	23
Dwn By: D. Fattig	VERT: N/A	OF 52
Chkd By: J Rudloff		

TYPICAL FOR ALL SIDE STREET INTERSECTION
WORK SEE SHEET 32
FOR CONSTRUCTION LIMITS & SIGNAGE

CONTRACTOR TO MAINTAIN
ACCESS TO ALL DRIVEWAY



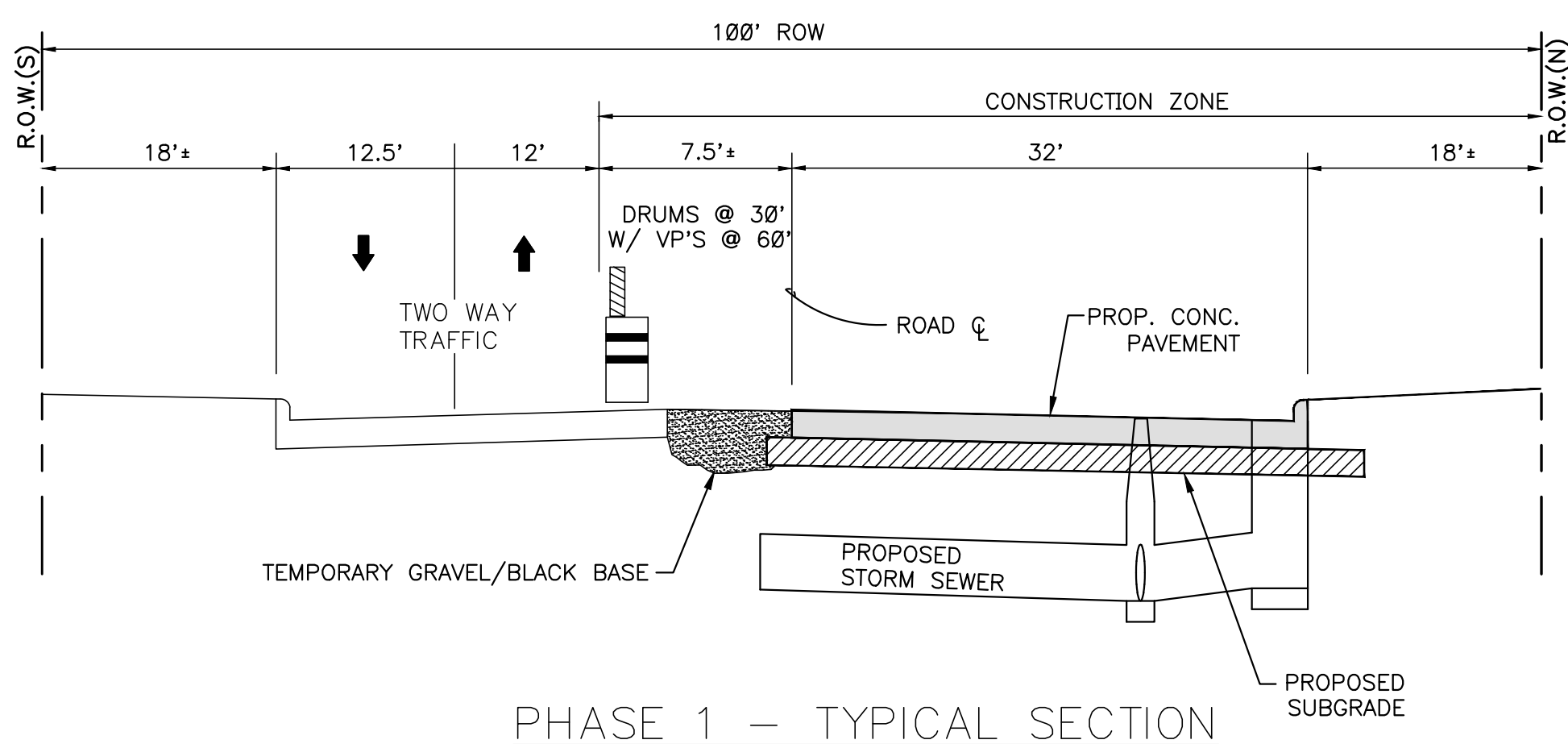
MATCH LINE STA. 16+00 SEE SHEET 25

LEGEND

- PHASE 1 PVMT CONSTRUCTION
- PHASE 1A STORM SEWER CONSTRUCTION ONLY (TEMPORARY BLACK BASE REPAIR)
- PHASE 2 PVMT CONSTRUCTION
- PHASE 3 PVMT CONSTRUCTION
- PHASE 4 PVMT CONSTRUCTION
- TEMPORARY BLACK BASE REPAIR
- COMPLETED CONCRETE PAVEMENT
- TRAFFIC FLOW
- DRUMS
- TRAFFIC SIGNS
- RAISED PAVEMENT MARKERS REFLECTORS
- TRAILER MOUNTED FLASHING ARROW BOARD

PHASE 1/1A PAVEMENT NOTES:

1. CLOSE WESTBOUND LANES FROM 6th STREET TO 13th STREET PLACE TRAFFIC CONTROL SIGNAGE, DETOUR SIGNS, DEVICES AND DRUMS.
2. ONCE INSTALLATION OF STORM SEWER AND TEMPORARY PAVEMENT IN PHASE 1A AREA IS COMPLETE. CONTRACTOR IS TO OPEN UP THIS AREA (PHASE 1A) TO TRAFFIC FLOW WESTBOUND.
3. PLACE TWO-WAY TRAFFIC ON EASTBOUND LANES TO PROVIDE TEMPORARY LOCAL ACCESS.
4. INSTALL STORM SEWER ALONG THE ROADWAY AS INDICATED ON PLANS.
5. BACKFILL STORM SEWER IMMEDIATELY TO MAINTAIN ACCESS TO DRIVEWAYS AND SIDE STREETS. (NO SEPARATE PAY)
6. FOLLOW UP WITH PAVING ON WESTBOUND LANES FROM 13th STREET TO 6th STREET.
7. CONTINUE TO MAINTAIN ACCESS TO DRIVEWAYS. (NO SEPARATE PAY)
8. NO TWO CONSECUTIVE INTERSECTION CAN BE CLOSE AT THE SAME TIME.



TEXAS AVE SPEED LIMIT
WEST OF 14th STREET - 35 MPH
EAST OF 14th STREET - 30 MPH

Posted Speed * S	Formula	Minimum Desirable Taper Lengths **			Suggested Maximum Spacing of Channelizing Devices			Minimum Sign Spacing "x" Distance	Suggested Longitudinal Buffer Space "y"
		10' Offset	11' Offset	12' Offset	On a Taper	On a Tangent	On a Curve		
30	$L = \frac{WS^2}{60}$	150'	165'	180'	30'	60'	120'	90'	
35		205'	225'	245'	35'	70'	160'	120'	
40		265'	295'	320'	40'	80'	240'	155'	
45		450'	495'	540'	45'	90'	320'	195'	
50		500'	550'	600'	50'	100'	400'	240'	
55		550'	605'	660'	55'	110'	500'	295'	
60		600'	660'	720'	60'	120'	600'	350'	
65		650'	715'	780'	65'	130'	700'	410'	
70		700'	770'	840'	70'	140'	800'	475'	
75		750'	825'	900'	75'	150'	900'	540'	

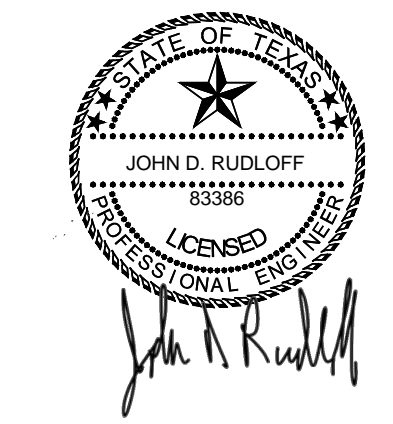
* Conventional Roads Only
** Taper lengths have been rounded off.
L=Length of Taper(F) W=Width of Offset(S) S=Posted Speed(MPH)

SEE SHEET 32 FOR TYPICAL
DETOUR LAYOUT FOR
CONSTRUCTION OF SIDE STREETS

GENERAL NOTES:

1. CONTRACTOR SHALL PROVIDE AND INSTALL ALL TRAFFIC CONTROL DEVICES AS PER THE LATEST REVISION OF THE TEXAS MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES (TXMUTCD).
2. THE TRAFFIC CONTROL PLAN AND DETAILS INCLUDED IN THE PLAN DRAWINGS ARE PROVIDED AS A GUIDE TO THE CONTRACTOR AND ARE THE MINIMUM REQUIREMENTS. CONTRACTOR IS RESPONSIBLE FOR PREPARATION AND SUBMITTAL OF A REVISED TRAFFIC CONTROL PLAN FOR REVIEW AND APPROVAL IF IMPLEMENTED DIFFERENTLY FROM WHAT IS SHOWN ON THE PLAN DRAWINGS.
3. THIS IS A GENERAL LAYOUT. IT IS NOT THE INTENT OF HAVING THE ENTIRE HALF OF ROADWAY REMOVE FROM END TO END AT ONE TIME. THE WORK SHALL BE LIMITED TO TWO BLOCKS AT A TIME.
4. THE CONTRACTOR IS RESPONSIBLE FOR MAINTAINING ACCESS TO ALL BUSINESS DURING CONSTRUCTION. THIS MAY REQUIRE LEAVING SEGMENTS OF EXISTING PAVEMENT AVAILABLE FOR ACCESS WHILE ADJACENT PAVEMENT IS POURED AND CURED.
5. ANY ADJUSTMENTS TO THE TRAFFIC CONTROL PLAN, INCLUDING PROVISION OF ADDITIONAL TRAFFIC CONTROL DEVICES AND SIGNAGE, AS NEEDED TO FACILITATE SMOOTH FLOW OF TRAFFIC AND TO ACCOMMODATE FIELD CONDITIONS SHALL BE CONSIDERED INCIDENTAL TO THE TRAFFIC CONTROL AND REGULATION BID ITEM.
6. CONTRACTOR SHALL MAINTAIN ALL WEATHER ACCESS TO RESIDENTIAL AND COMMERCIAL PROPERTIES ADJACENT TO AND IN THE WORK AREAS AT ALL TIMES.
7. CONTRACTOR IS RESPONSIBLE FOR MAINTAINING POSTAL SERVICE AND TRASH PICKUP SERVICE TO RESIDENTS DURING THE DURATION OF CONSTRUCTION OPERATIONS.

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19

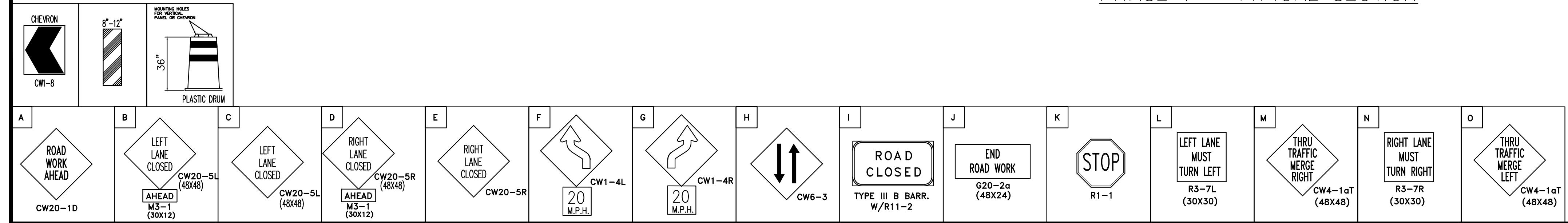
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Galveston County, Texas

Texas Avenue Reconstruction

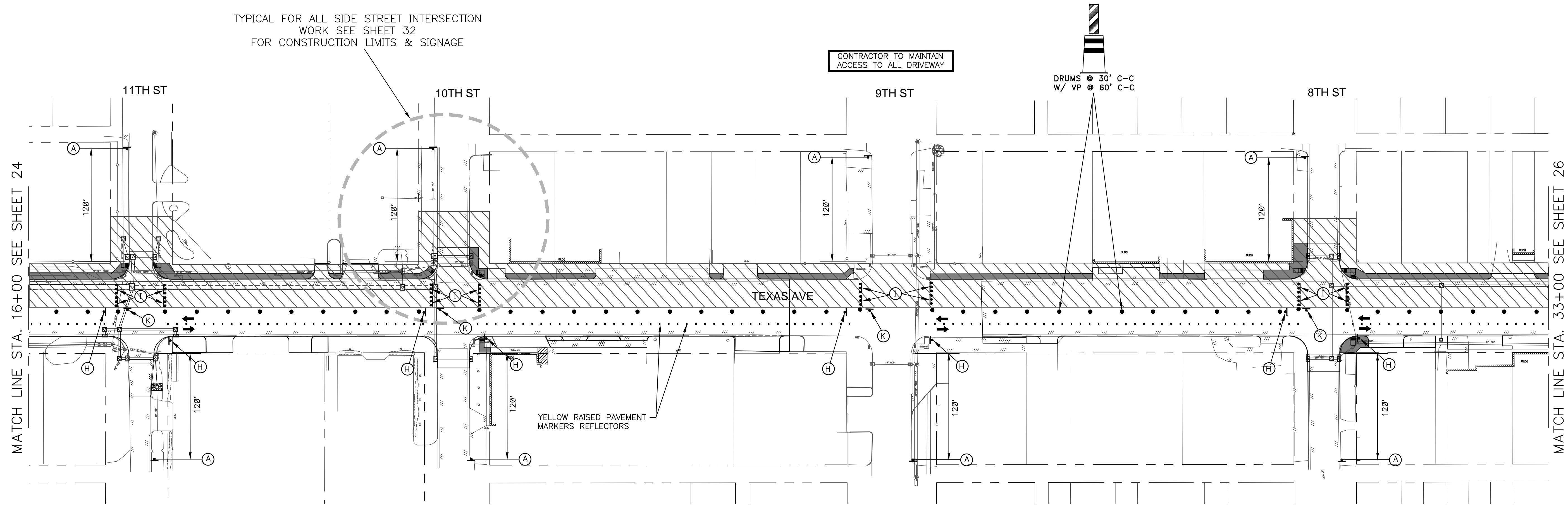
Phase 1 Traffic Layout - 1 of 3

Job No.: 18-015	Scale: 1"=40'	SHEET
Date: September, 2019	HORZ: 1"=40'	24
Dwn By: D. Fattig	VERT:	
Chk By: J Rudloff		OF 52



TYPICAL FOR ALL SIDE STREET INTERSECTION WORK SEE SHEET 32 FOR CONSTRUCTION LIMITS & SIGNAGE

CONTRACTOR TO MAINTAIN ACCESS TO ALL DRIVEWAY



MATCH LINE STA. 16+00 SEE SHEET 24

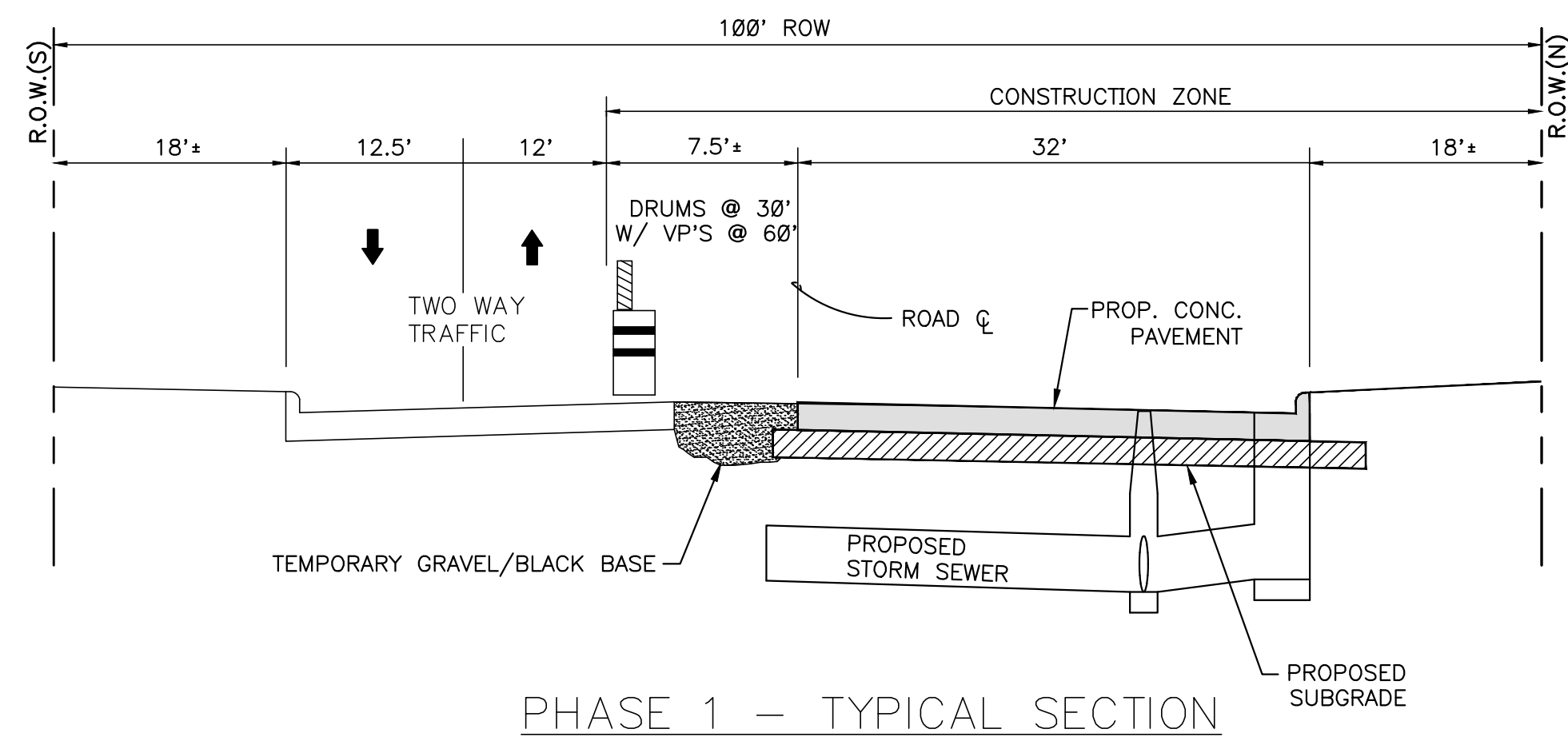
MATCH LINE STA. 33+00 SEE SHEET 26

LEGEND

- PHASE 1 PVMT CONSTRUCTION
- PHASE 1A STORM SEWER CONSTRUCTION ONLY (TEMPORARY BLACK BASE REPAIR)
- PHASE 2 PVMT CONSTRUCTION
- PHASE 3 PVMT CONSTRUCTION
- PHASE 4 PVMT CONSTRUCTION
- TEMPORARY BLACK BASE REPAIR
- COMPLETED CONCRETE PAVEMENT
- TRAFFIC FLOW
- DRUMS
- TRAFFIC SIGNS
- RAISED PAVEMENT MARKERS REFLECTORS
- TRAILER MOUNTED FLASHING ARROW BOARD

PHASE 1 PAVEMENT NOTES:

- CLOSE WESTBOUND LANES FROM 6th STREET TO 13th STREET PLACE TRAFFIC CONTROL SIGNAGE, DETOUR SIGNS, DEVICES AND DRUMS.
- PLACE TWO-WAY TRAFFIC ON EASTBOUND LANES TO PROVIDE TEMPORARY LOCAL ACCESS.
- INSTALL STORM SEWER ALONG THE ROADWAY AS INDICATED ON PLANS.
- BACKFILL STORM SEWER IMMEDIATELY TO MAINTAIN ACCESS TO DRIVEWAYS AND SIDE STREETS. (NO SEPARATE PAY)
- FOLLOW UP WITH PAVING ON WESTBOUND LANES FROM 13th STREET TO 6th STREET.
- CONTINUE TO MAINTAIN ACCESS TO DRIVEWAYS. (NO SEPARATE PAY)
- NO TWO CONSECUTIVE INTERSECTION CAN BE CLOSE AT THE SAME TIME.



TEXAS AVE SPEED LIMIT
WEST OF 14th STREET - 35 MPH
EAST OF 14th STREET - 30 MPH

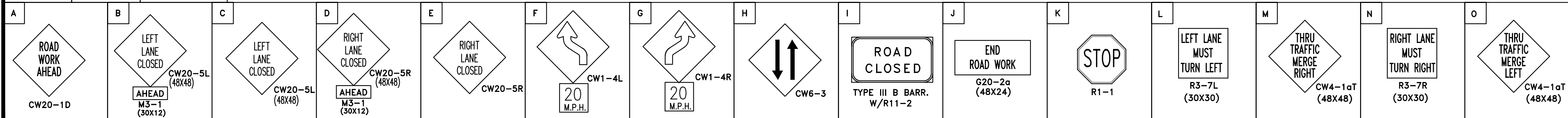
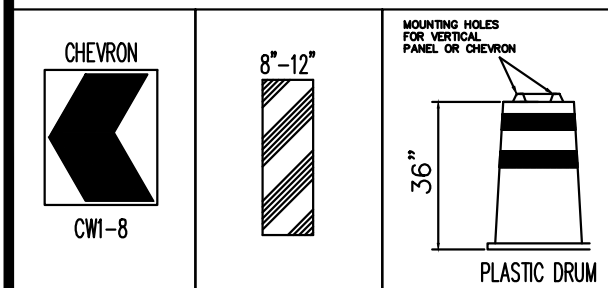
Posted Speed *	Formula	Minimum Desirable Taper Lengths			Suggested Maximum Spacing of Channelizing Devices		Minimum Sign Spacing Distance	Suggested Longitudinal Buffer Space **
		10' Offset	11' Offset	12' Offset	On a Taper	On a Tangent		
30	L = WS ² / 60	150'	165'	180'	30'	60'	120'	90'
35		205'	225'	245'	35'	70'	160'	120'
40	L = WS	265'	295'	320'	40'	80'	240'	155'
45		450'	495'	540'	45'	90'	320'	195'
50	L = WS	500'	550'	600'	50'	100'	400'	240'
55		550'	605'	660'	55'	110'	500'	295'
60	L = WS	600'	660'	720'	60'	120'	600'	350'
65		650'	715'	780'	65'	130'	700'	410'
70	L = WS	700'	770'	840'	70'	140'	800'	475'
75		750'	825'	900'	75'	150'	900'	540'

* Conventional Roads Only
** Taper lengths have been rounded off.
L=Length of Taper(F) W=Width of Offset(F) S=Posted Speed(MPH)

SEE SHEET 32 FOR TYPICAL DETOUR LAYOUT FOR CONSTRUCTION OF SIDE STREETS

GENERAL NOTES:

- CONTRACTOR SHALL PROVIDE AND INSTALL ALL TRAFFIC CONTROL DEVICES AS PER THE LATEST REVISION OF THE TEXAS MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES (TXMUTCD).
- THE TRAFFIC CONTROL PLAN AND DETAILS INCLUDED IN THE PLAN DRAWINGS ARE PROVIDED AS A GUIDE TO THE CONTRACTOR AND ARE THE MINIMUM REQUIREMENTS. CONTRACTOR IS RESPONSIBLE FOR PREPARATION AND SUBMITTAL OF A REVISED TRAFFIC CONTROL PLAN FOR REVIEW AND APPROVAL IF IMPLEMENTED DIFFERENTLY FROM WHAT IS SHOWN ON THE PLAN DRAWINGS.
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- THE CONTRACTOR IS RESPONSIBLE FOR MAINTAINING ACCESS TO ALL BUSINESS DURING CONSTRUCTION. THIS MAY REQUIRE LEAVING SEGMENTS OF EXISTING PAVEMENT AVAILABLE FOR ACCESS WHILE ADJACENT PAVEMENT IS POURED AND CURED.
- ANY ADJUSTMENTS TO THE TRAFFIC CONTROL PLAN, INCLUDING PROVISION OF ADDITIONAL TRAFFIC CONTROL DEVICES AND SIGNAGE AS NEEDED TO FACILITATE SMOOTH FLOW OF TRAFFIC AND TO ACCOMMODATE FIELD CONDITIONS SHALL BE CONSIDERED INCIDENTAL TO THE TRAFFIC CONTROL AND REGULATION BID ITEM.
- CONTRACTOR SHALL MAINTAIN ALL WEATHER ACCESS TO RESIDENTIAL AND COMMERCIAL PROPERTIES ADJACENT TO AND IN THE WORK AREAS AT ALL TIMES.
- CONTRACTOR IS RESPONSIBLE FOR MAINTAINING POSTAL SERVICE AND TRASH PICKUP SERVICE TO RESIDENTS DURING THE DURATION OF CONSTRUCTION OPERATIONS.



MK.	DESCRIPTION	DATE	DWN.	CHK.

STATE OF TEXAS
JOHN D. RUDLOFF
LICENSED PROFESSIONAL ENGINEER
83386
9-13-19

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Galveston County, Texas

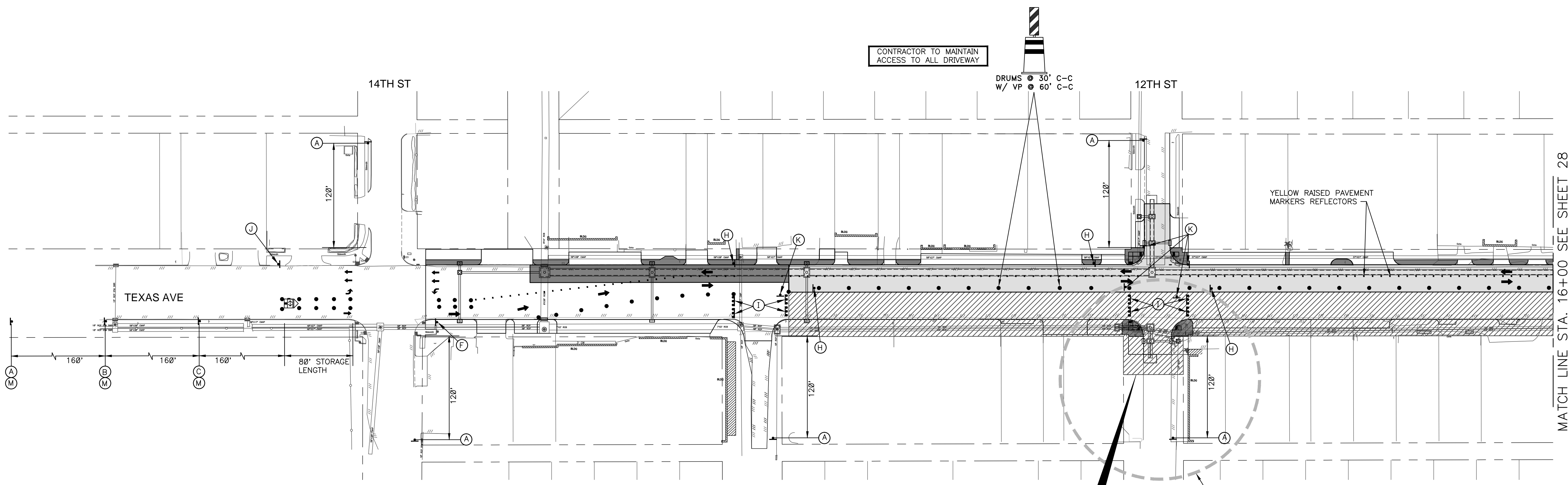
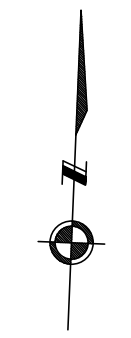
Texas Avenue Reconstruction

Phase 1 Traffic Layout - 2 of 3

Job No.: 18-015
Date: September, 2019
Dwn By: D. Fattig
Chk By: J Rudloff

Scale: HORIZ: 1"=40'
VERT: 1"=10'

SHEET 25 OF 52



MATCH LINE STA. 16+00 SEE SHEET 28

CONTRACTOR TO MAINTAIN ACCESS TO ALL DRIVEWAY

DRUMS @ 30' W/ VP @ 60' C-C

YELLOW RAISED PAVEMENT MARKERS REFLECTORS

11TH STREET PAVING & DRAINAGE MUST BE COMPLETE BEFORE 12TH STREET STORM SEWER (SOUTH SIDE) CAN BE BUILT

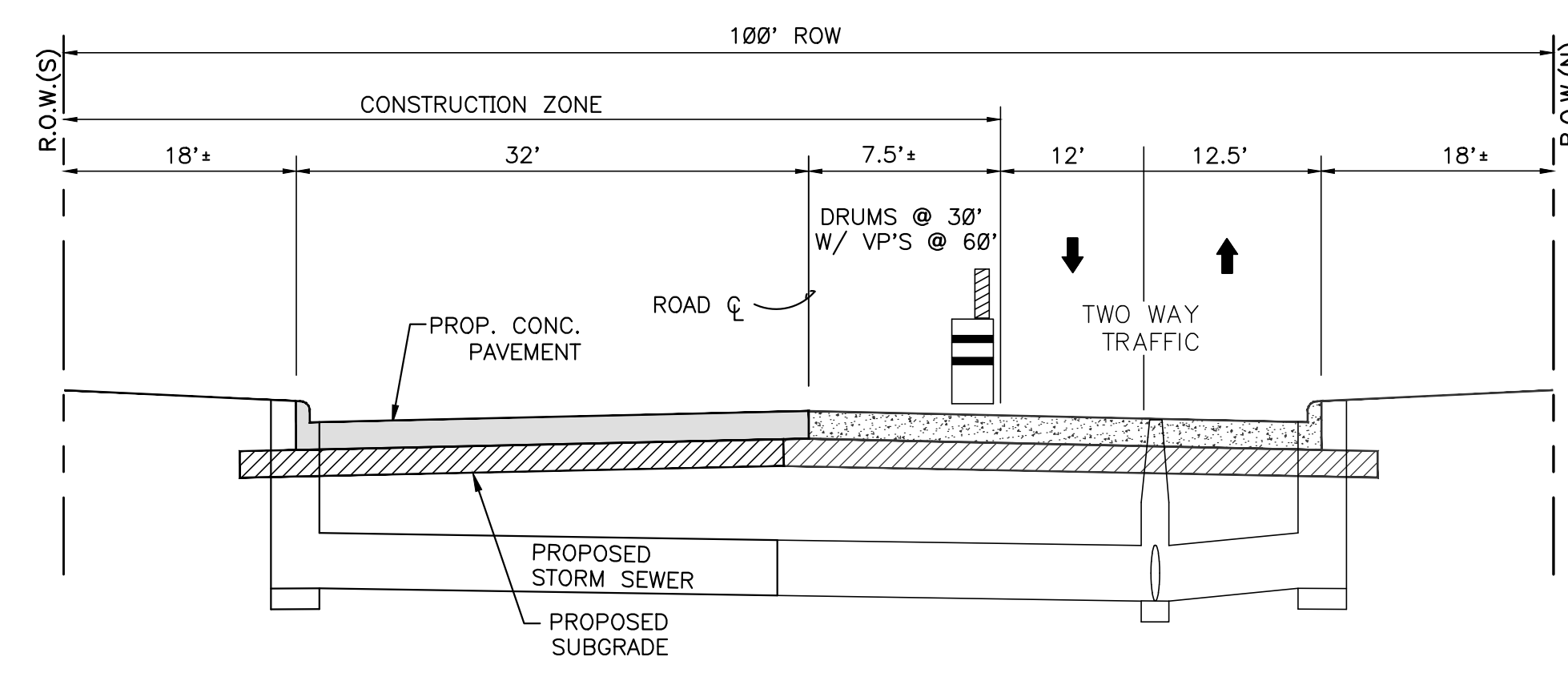
TYPICAL FOR ALL SIDE STREET INTERSECTION WORK SEE SHEET 32 FOR CONSTRUCTION LIMITS & SIGNAGE

LEGEND

- PHASE 1 PVMT CONSTRUCTION
- PHASE 1A STORM SEWER CONSTRUCTION ONLY (TEMPORARY BLACK BASE REPAIR)
- PHASE 2 PVMT CONSTRUCTION
- PHASE 3 PVMT CONSTRUCTION
- PHASE 4 PVMT CONSTRUCTION
- TEMPORARY BLACK BASE REPAIR
- COMPLETED CONCRETE PAVEMENT
- TRAFFIC FLOW
- DRUMS
- TRAFFIC SIGNS
- RAISED PAVEMENT MARKERS REFLECTORS
- TRAILER MOUNTED FLASHING ARROW BOARD

PHASE 2 PAVEMENT NOTES:

1. CLOSE EASTBOUND LANES FROM 6th STREET TO 13th STREET AND PLACE TRAFFIC CONTROL SIGNAGE, DETOUR SIGNS, DEVICES AND DRUMS.
2. PLACE TWO-WAY TRAFFIC ALONG WESTBOUND LANES TO PROVIDE TEMPORARY LOCAL ACCESS.
3. INSTALL STORM SEWER LATERALS AND INLETS ALONG THE SIDE OF THE ROADWAY AS INDICATED ON PLANS.
4. BACKFILL STORM SEWER IMMEDIATELY TO MAINTAIN ACCESS TO DRIVEWAYS AND SIDE STREETS. (NO SEPARATE PAY)
5. FOLLOW UP WITH PAVING ON EASTBOUND LANES FROM 13th STREET TO 6th STREET
6. CONTINUE TO MAINTAIN ACCESS TO DRIVEWAYS. (NO SEPARATE PAY)
7. NO TWO CONSECUTIVE INTERSECTION CAN BE CLOSE AT THE SAME TIME.



PHASE 2 - TYPICAL SECTION

TEXAS AVE SPEED LIMIT WEST OF 14th STREET - 35 MPH EAST OF 14th STREET - 30 MPH

Posted Speed *	Formula	Minimum Desirable Taper Lengths **			Suggested Maximum Spacing of Channelizing Devices		Minimum Sign Spacing *†	Suggested Longitudinal Buffer Space ‡
		10' Offset	11' Offset	12' Offset	On a Taper	On a Tangent		
30	$L = \frac{WS^2}{60}$	150'	165'	180'	30'	60'	120'	90'
35		205'	225'	245'	35'	70'	160'	120'
40		265'	295'	320'	40'	80'	240'	155'
45		450'	495'	540'	45'	90'	320'	195'
50		500'	550'	600'	50'	100'	400'	240'
55	$L=WS$	550'	605'	660'	55'	110'	500'	295'
60		600'	660'	720'	60'	120'	600'	350'
65		650'	715'	780'	65'	130'	700'	410'
70		700'	770'	840'	70'	140'	800'	475'
75		750'	825'	900'	75'	150'	900'	540'

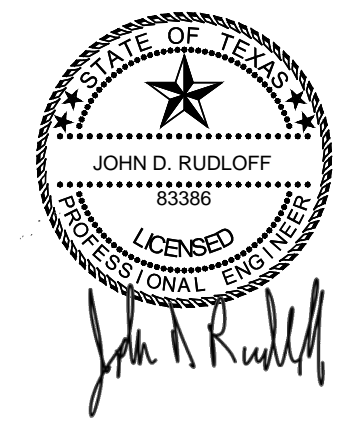
* Conventional Roads Only
** Taper lengths have been rounded off.
† Length of Taper (FT) W=Width of Offset (FT) S=Posted Speed (MPH)

GENERAL NOTES:

1. CONTRACTOR SHALL PROVIDE AND INSTALL ALL TRAFFIC CONTROL DEVICES AS PER THE LATEST REVISION OF THE TEXAS MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES (TXMUTCD).
2. THE TRAFFIC CONTROL PLAN AND DETAILS INCLUDED IN THE PLAN DRAWINGS ARE PROVIDED AS A GUIDE TO THE CONTRACTOR AND ARE THE MINIMUM REQUIREMENTS. CONTRACTOR IS RESPONSIBLE FOR PREPARATION AND SUBMITTAL OF A REVISED TRAFFIC CONTROL PLAN FOR REVIEW AND APPROVAL IF IMPLEMENTED DIFFERENTLY FROM WHAT IS SHOWN ON THE PLAN DRAWINGS.
3. THIS IS A GENERAL LAYOUT. IT IS NOT THE INTENT OF HAVING THE ENTIRE HALF OF ROADWAY REMOVE FROM END TO END AT ONE TIME. THE WORK SHALL BE LIMITED TO TWO BLOCKS AT A TIME.
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5. ANY ADJUSTMENTS TO THE TRAFFIC CONTROL PLAN, INCLUDING PROVISION OF ADDITIONAL TRAFFIC CONTROL DEVICES AND SIGNAGE, AS NEEDED TO FACILITATE SMOOTH FLOW OF TRAFFIC AND TO ACCOMMODATE FIELD CONDITIONS SHALL BE CONSIDERED INCIDENTAL TO THE TRAFFIC CONTROL AND REGULATION BID ITEM.
6. CONTRACTOR SHALL MAINTAIN ALL WEATHER ACCESS TO RESIDENTIAL AND COMMERCIAL PROPERTIES ADJACENT TO AND IN THE WORK AREAS AT ALL TIMES.
7. CONTRACTOR IS RESPONSIBLE FOR MAINTAINING POSTAL SERVICE AND TRASH PICKUP SERVICE TO RESIDENTS DURING THE DURATION OF CONSTRUCTION OPERATIONS.

SEE SHEET 32 FOR TYPICAL DETOUR LAYOUT FOR CONSTRUCTION OF SIDE STREETS

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19

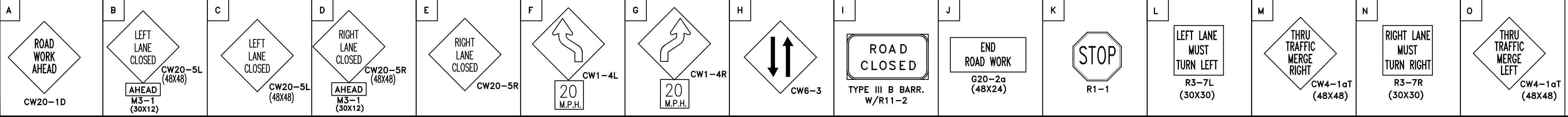
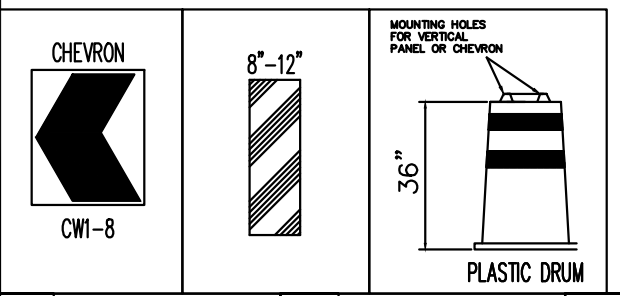


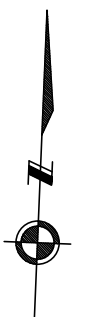
Galveston County, Texas

Texas Avenue Reconstruction

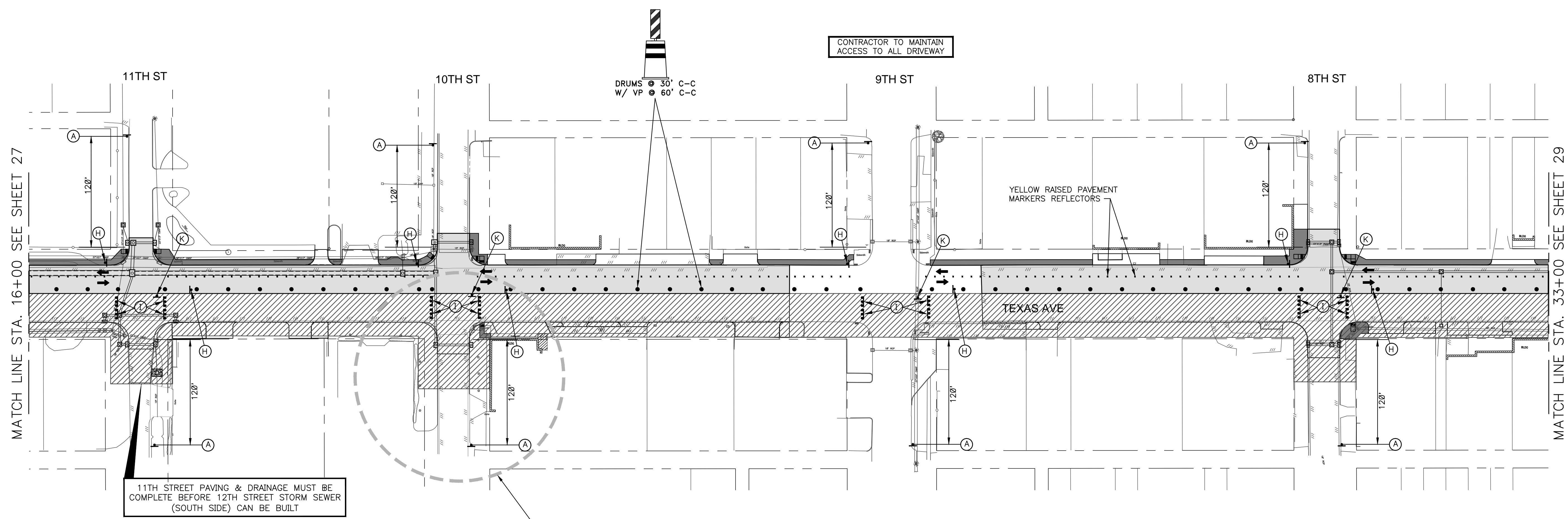
Phase 2 Traffic Layout - 1 of 3

Job No.: 18-015	Scale: HORIZ: 1"=40'	SHEET
Date: September, 2019	VERT: 1"=40'	27
Dwn By: D. Fattig	Chkd By: J. Rudloff	OF 52





CONTRACTOR TO MAINTAIN ACCESS TO ALL DRIVEWAY



11TH STREET PAVING & DRAINAGE MUST BE COMPLETE BEFORE 12TH STREET STORM SEWER (SOUTH SIDE) CAN BE BUILT

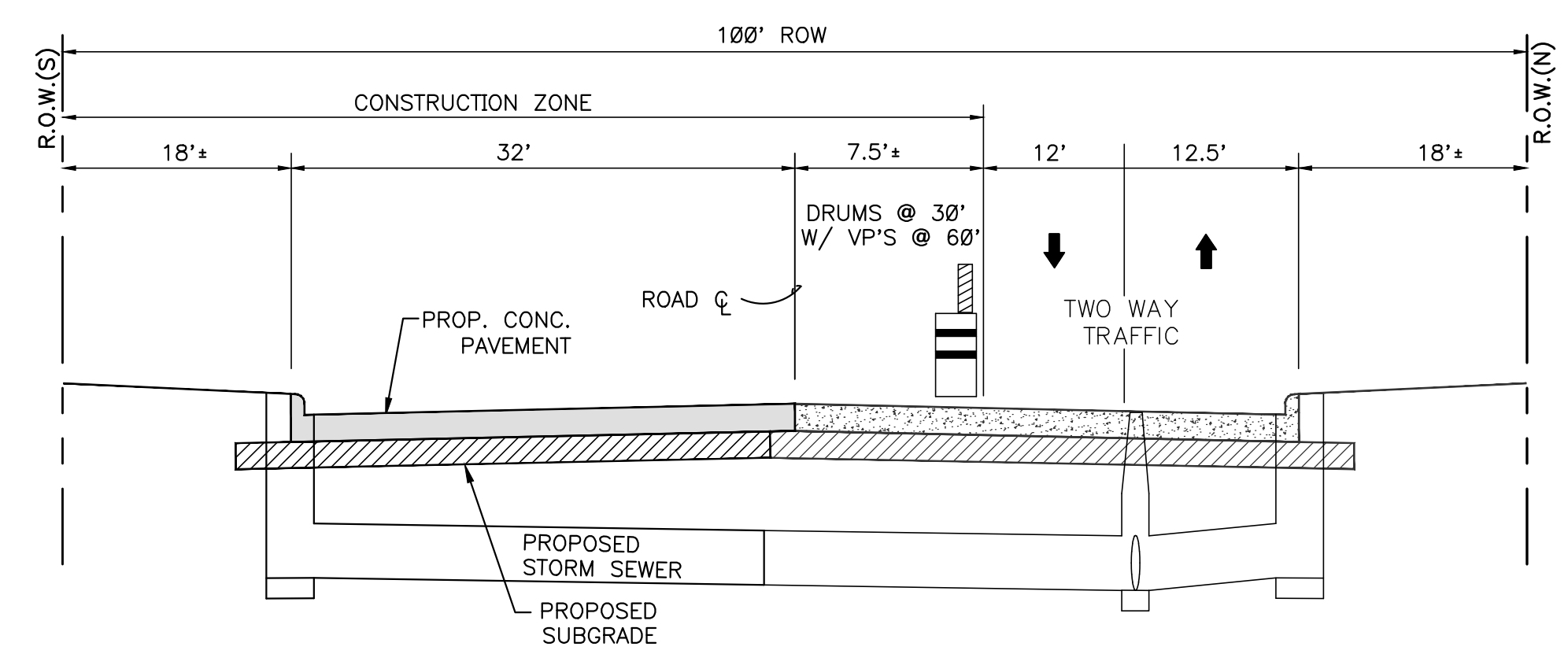
TYPICAL FOR ALL SIDE STREET INTERSECTION WORK SEE SHEET 32 FOR CONSTRUCTION LIMITS & SIGNAGE

LEGEND

- PHASE 1 PVMT CONSTRUCTION
- PHASE 1A STORM SEWER CONSTRUCTION ONLY (TEMPORARY BLACK BASE REPAIR)
- PHASE 2 PVMT CONSTRUCTION
- PHASE 3 PVMT CONSTRUCTION
- PHASE 4 PVMT CONSTRUCTION
- TEMPORARY BLACK BASE REPAIR
- COMPLETED CONCRETE PAVEMENT
- TRAFFIC FLOW
- DRUMS
- TRAFFIC SIGNS
- RAISED PAVEMENT MARKERS REFLECTORS
- TRAILER MOUNTED FLASHING ARROW BOARD

PHASE 2 PAVEMENT NOTES:

- CLOSE EASTBOUND LANES FROM 6th STREET TO 13th STREET AND PLACE TRAFFIC CONTROL SIGNAGE, DETOUR SIGNS, DEVICES AND DRUMS.
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- CONTINUE TO MAINTAIN ACCESS TO DRIVEWAYS. (NO SEPARATE PAY)
- NO TWO CONSECUTIVE INTERSECTION CAN BE CLOSE AT THE SAME TIME.



PHASE 2 - TYPICAL SECTION

TEXAS AVE SPEED LIMIT
WEST OF 14th STREET - 35 MPH
EAST OF 14th STREET - 30 MPH

Posted Speed	Formula	Minimum Desirable Taper Lengths			Suggested Maximum Spacing of Channelizing Devices		Minimum Sign Spacing Distance	Suggested Longitudinal Buffer Space
		10' Offset	11' Offset	12' Offset	On a Taper	On a Tangent		
30	$L = \frac{WS^2}{60}$	150'	165'	180'	30'	60'	120'	90'
35	$L = \frac{WS^2}{60}$	205'	225'	245'	35'	70'	160'	120'
40	$L = \frac{WS^2}{60}$	265'	295'	320'	40'	80'	240'	155'
45	$L = \frac{WS^2}{60}$	450'	495'	540'	45'	90'	320'	195'
50	$L = \frac{WS^2}{60}$	500'	550'	600'	50'	100'	400'	240'
55	$L = \frac{WS^2}{60}$	550'	605'	660'	55'	110'	500'	295'
60	$L = \frac{WS^2}{60}$	600'	660'	720'	60'	120'	600'	350'
65	$L = \frac{WS^2}{60}$	650'	715'	780'	65'	130'	700'	410'
70	$L = \frac{WS^2}{60}$	700'	770'	840'	70'	140'	800'	475'
75	$L = \frac{WS^2}{60}$	750'	825'	900'	75'	150'	900'	540'

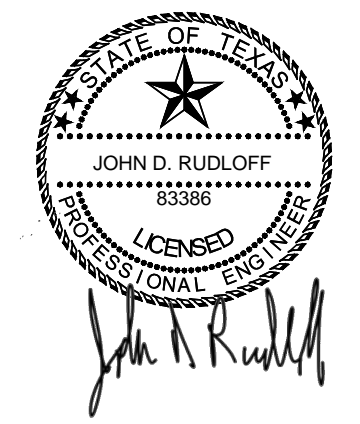
* Conventional Roads Only
** Taper lengths have been rounded off.
L=Length of Taper(F) W=Width of Offset(F) S=Posted Speed(MPH)

SEE SHEET 32 FOR TYPICAL DETOUR LAYOUT FOR CONSTRUCTION OF SIDE STREETS

MK.	DESCRIPTION	DATE	DWN.	CHK.

GENERAL NOTES:

- CONTRACTOR SHALL PROVIDE AND INSTALL ALL TRAFFIC CONTROL DEVICES AS PER THE LATEST REVISION OF THE TEXAS MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES (TXMUTCD).
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9-13-19



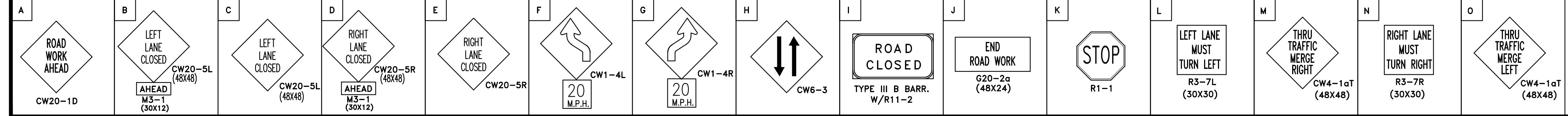
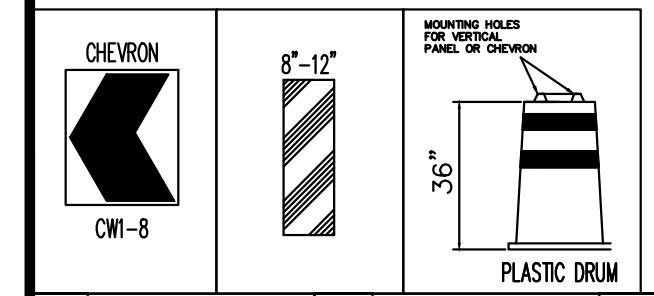
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(713) 400-2755 • www.arkkengineers.com • TX PE Firm No. 13872

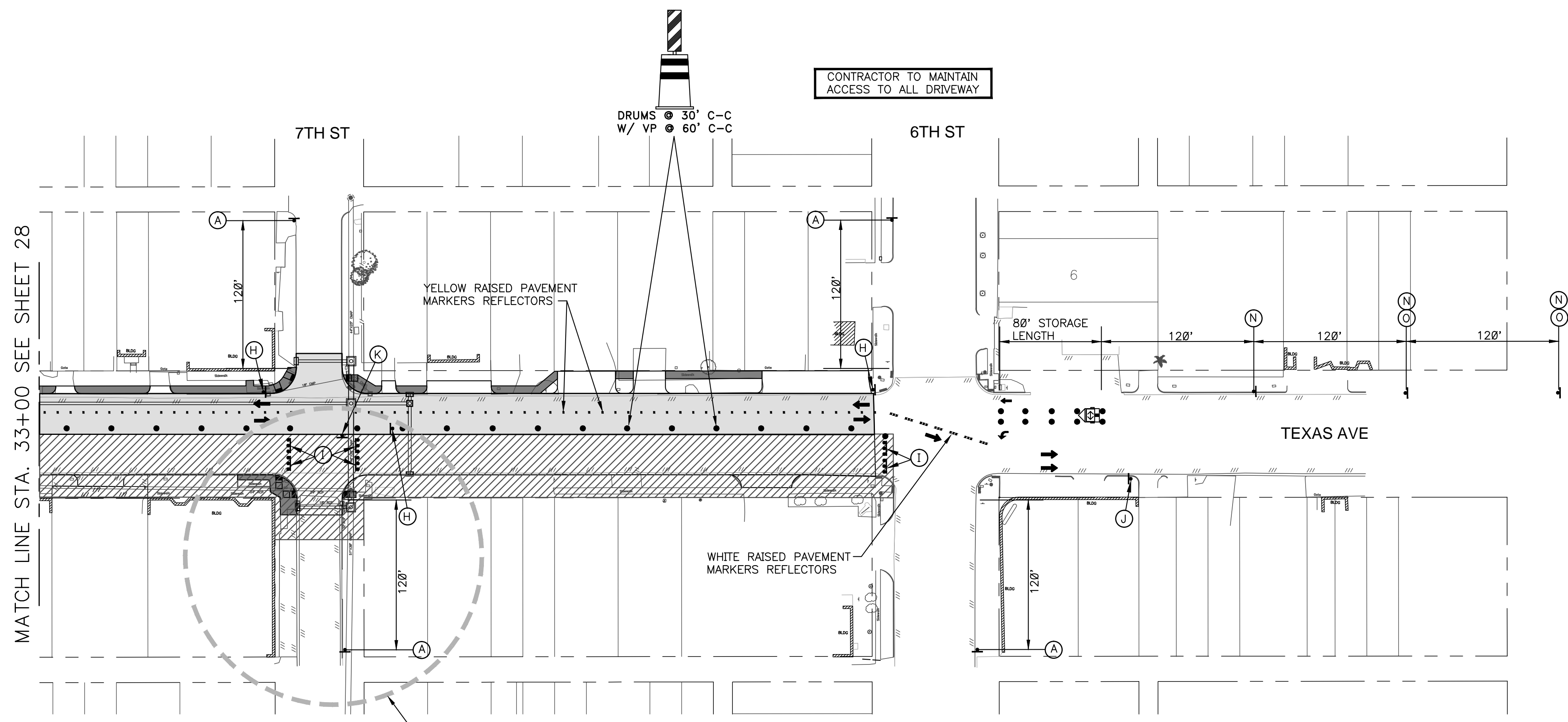
Galveston County, Texas

Texas Avenue Reconstruction

Phase 2 Traffic Layout - 2 of 3

Job No.: 18-015	Scale: 1"=40'	SHEET
Date: September, 2019	HORIZ: 1"=40'	28
Dwn By: D. Fattig	VERT:	
Chk By: J Rudloff		OF 52





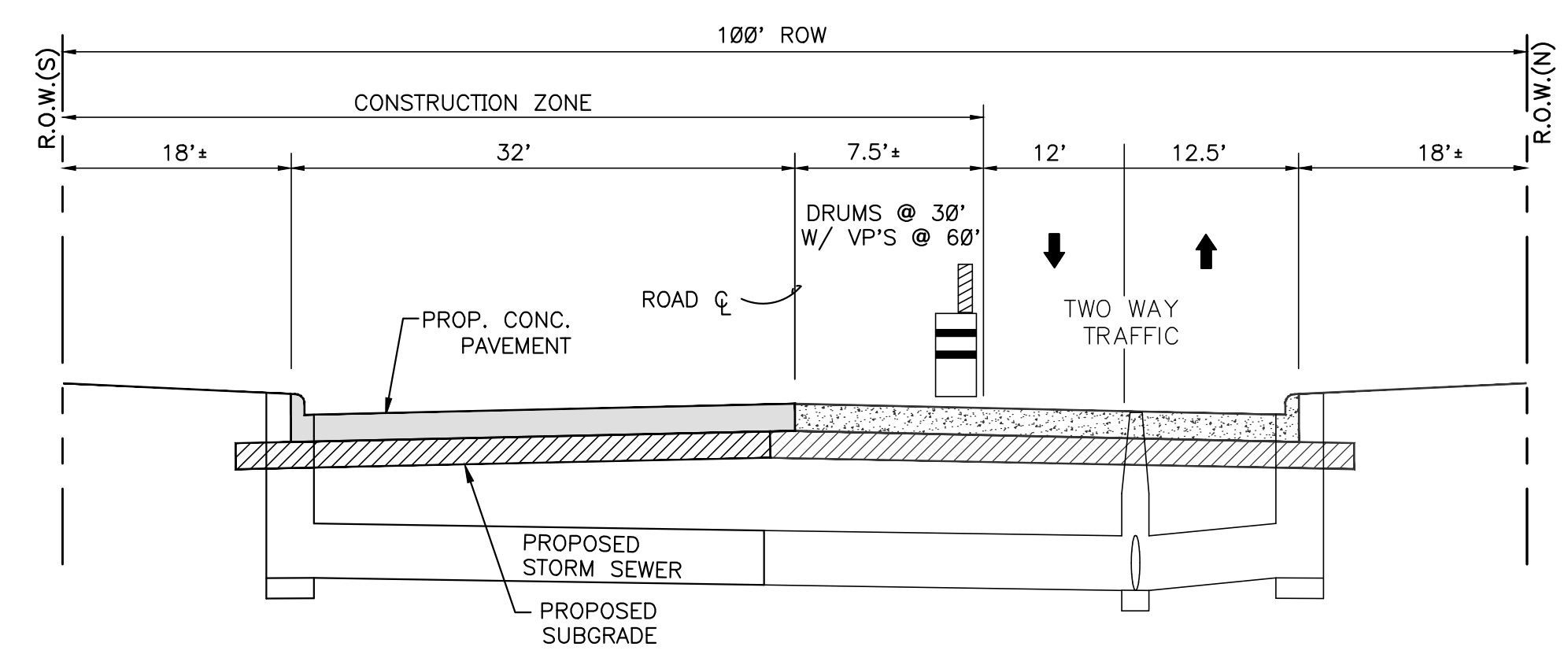
LEGEND

- PHASE 1 PVMT CONSTRUCTION
- PHASE 1A STORM SEWER CONSTRUCTION ONLY (TEMPORARY BLACK BASE REPAIR)
- PHASE 2 PVMT CONSTRUCTION
- PHASE 3 PVMT CONSTRUCTION
- PHASE 4 PVMT CONSTRUCTION
- TEMPORARY BLACK BASE REPAIR
- COMPLETED CONCRETE PAVEMENT
- TRAFFIC FLOW
- DRUMS
- TRAFFIC SIGNS
- RAISED PAVEMENT MARKERS REFLECTORS
- TRAILER MOUNTED FLASHING ARROW BOARD

PHASE 2 PAVEMENT NOTES:

- CLOSE EASTBOUND LANES FROM 6th STREET TO 13th STREET AND PLACE TRAFFIC CONTROL SIGNAGE, DETOUR SIGNS, DEVICES AND DRUMS.
- PLACE TWO-WAY TRAFFIC ALONG WESTBOUND LANES TO PROVIDE TEMPORARY LOCAL ACCESS.
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- CONTINUE TO MAINTAIN ACCESS TO DRIVEWAYS. (NO SEPARATE PAY)
- NO TWO CONSECUTIVE INTERSECTION CAN BE CLOSE AT THE SAME TIME.

TYPICAL FOR ALL SIDE STREET INTERSECTION
WORK SEE SHEET 32
FOR CONSTRUCTION LIMITS & SIGNAGE



PHASE 2 - TYPICAL SECTION

TEXAS AVE SPEED LIMIT
WEST OF 14th STREET - 35 MPH
EAST OF 14th STREET - 30 MPH

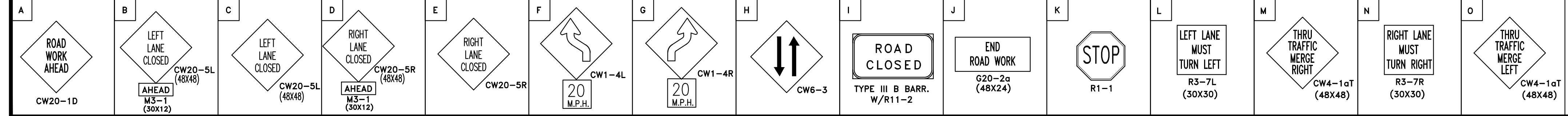
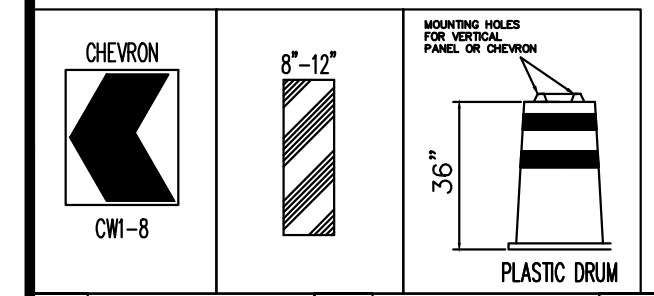
Posted Speed *	Formula	Minimum Desirable Taper Lengths **			Suggested Maximum Spacing of Channelizing Devices		Minimum Sign Spacing Distance	Suggested Longitudinal Buffer Space "B"
		10' Offset	11' Offset	12' Offset	On a Taper	On a Tangent		
30	L=WS	150'	165'	180'	30'	60'	120'	90'
35		205'	225'	245'	35'	70'	160'	120'
40	L=WS	265'	285'	320'	40'	80'	240'	155'
45		450'	495'	540'	45'	90'	320'	195'
50	L=WS	500'	550'	600'	50'	100'	400'	240'
55		550'	605'	660'	55'	110'	500'	295'
60	L=WS	600'	660'	720'	60'	120'	600'	350'
65		650'	715'	780'	65'	130'	700'	410'
70	L=WS	700'	770'	840'	70'	140'	800'	475'
75		750'	825'	900'	75'	150'	900'	540'

* Conventional Roads Only
** Taper lengths have been rounded off.
L=Length of Taper(FT) W=Width of Offset(FT) S=Posted Speed(MPH)

SEE SHEET 32 FOR TYPICAL
DETOUR LAYOUT FOR
CONSTRUCTION OF SIDE STREETS

GENERAL NOTES:

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MK. DESCRIPTION DATE DWN. CHK.

9-13-19

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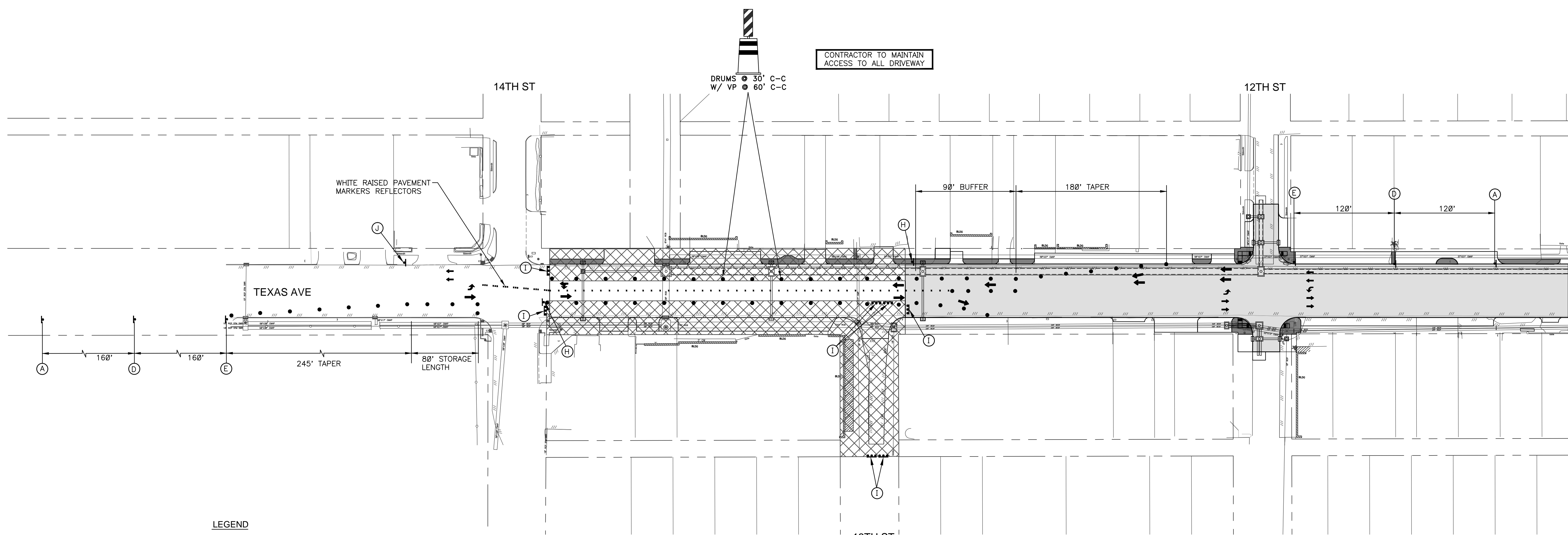
Galveston County, Texas

Texas Avenue Reconstruction

Phase 2 Traffic Layout - 3 of 3

Job No.: 18-015 Scale: 1"=40'
Date: September, 2019 HORIZ: 1"=40'
Dwn By: D. Fattig VERT:
Chk By: J Rudloff

SHEET **29** OF 52

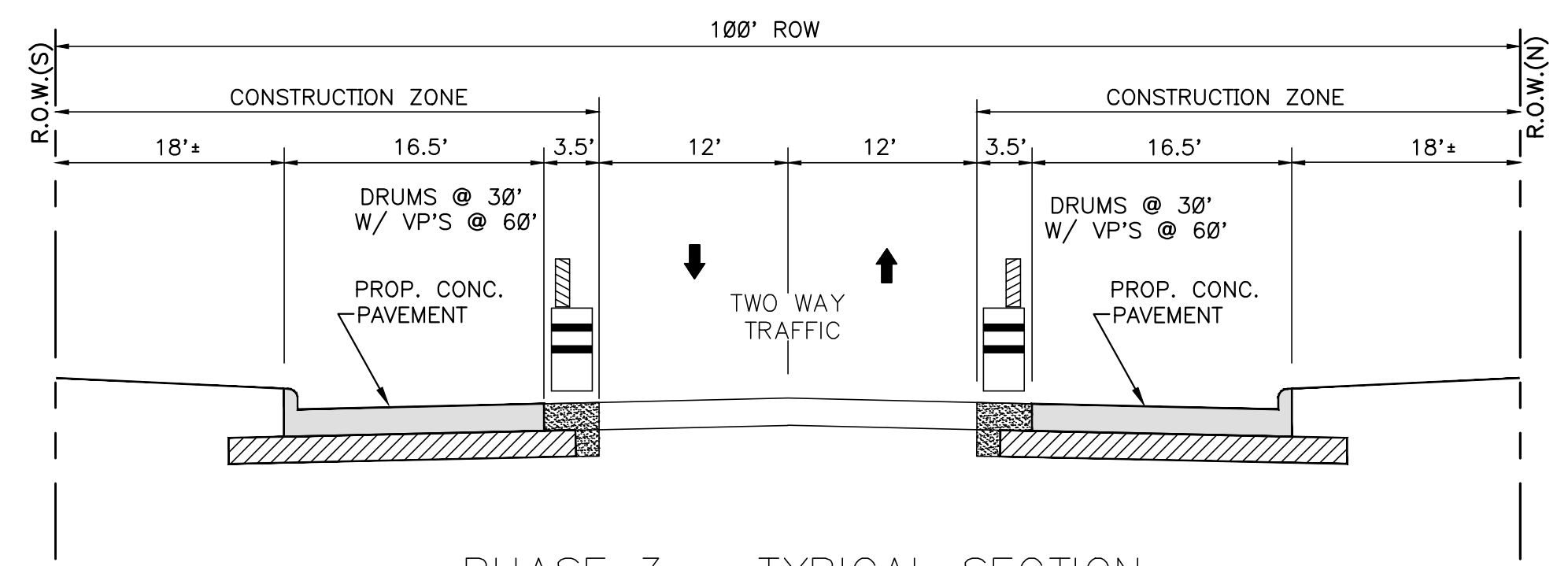


LEGEND

- PHASE 1 PVMT CONSTRUCTION
- PHASE 1A STORM SEWER CONSTRUCTION ONLY (TEMPORARY BLACK BASE REPAIR)
- PHASE 2 PVMT CONSTRUCTION
- PHASE 3 PVMT CONSTRUCTION
- PHASE 4 PVMT CONSTRUCTION
- TEMPORARY BLACK BASE REPAIR
- COMPLETED CONCRETE PAVEMENT
- TRAFFIC FLOW
- DRUMS
- TRAFFIC SIGNS
- RAISED PAVEMENT MARKERS REFLECTORS
- TRAILER MOUNTED FLASHING ARROW BOARD

PHASE 3 PAVEMENT NOTES:

- CLOSE EASTBOUND LANES FROM 14th STREET TO 13th STREET AND PLACE TRAFFIC CONTROL SIGNAGE, DETOUR SIGNS, DEVICES AND DRUMS.
- PLACE TWO-WAY TRAFFIC AND PROVIDE TEMPORARY LOCAL ACCESS.
- FOLLOW UP WITH PAVING ON LANES FROM 14th STREET TO 13th STREET
- CONTINUE TO MAINTAIN ACCESS TO DRIVEWAYS. (NO SEPARATE PAY)



PHASE 3 - TYPICAL SECTION

TEXAS AVE SPEED LIMIT
WEST OF 14th STREET - 35 MPH
EAST OF 14th STREET - 30 MPH

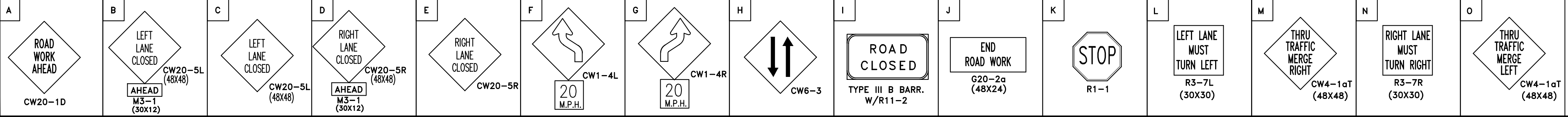
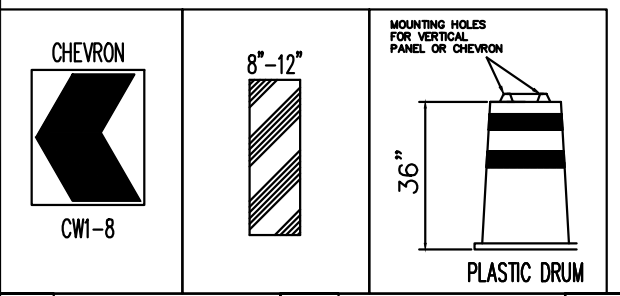
Posted Speed *	Formula	Minimum Desirable Taper Lengths			Suggested Maximum Spacing of Channelizing Devices		Minimum Sign Spacing * Distance	Suggested Longitudinal Buffer Space Distance
		10' Offset	11' Offset	12' Offset	On a Taper	On a Tangent		
30	L=WS	150'	165'	180'	30'	60'	120'	90'
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55		550'	605'	660'	55'	110'	500'	295'
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* Conventional Roads Only
** Taper lengths have been rounded off.
L=Length of Taper(FT) W=Width of Offset(FT) S=Posted Speed(MPH)

SEE SHEET 32 FOR TYPICAL DETOUR LAYOUT FOR CONSTRUCTION OF SIDE STREETS

GENERAL NOTES:

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MK. DESCRIPTION DATE DWN. CHK.

STATE OF TEXAS
JOHN D. RUDLOFF
LICENSED PROFESSIONAL ENGINEER
83386

9-13-19

ARKK ENGINEERS
7322 Southwest Freeway, Suite 1040 • Houston, Texas 77074
(713) 400-2755 • www.arkkengineers.com • TX PE Firm No. 13872

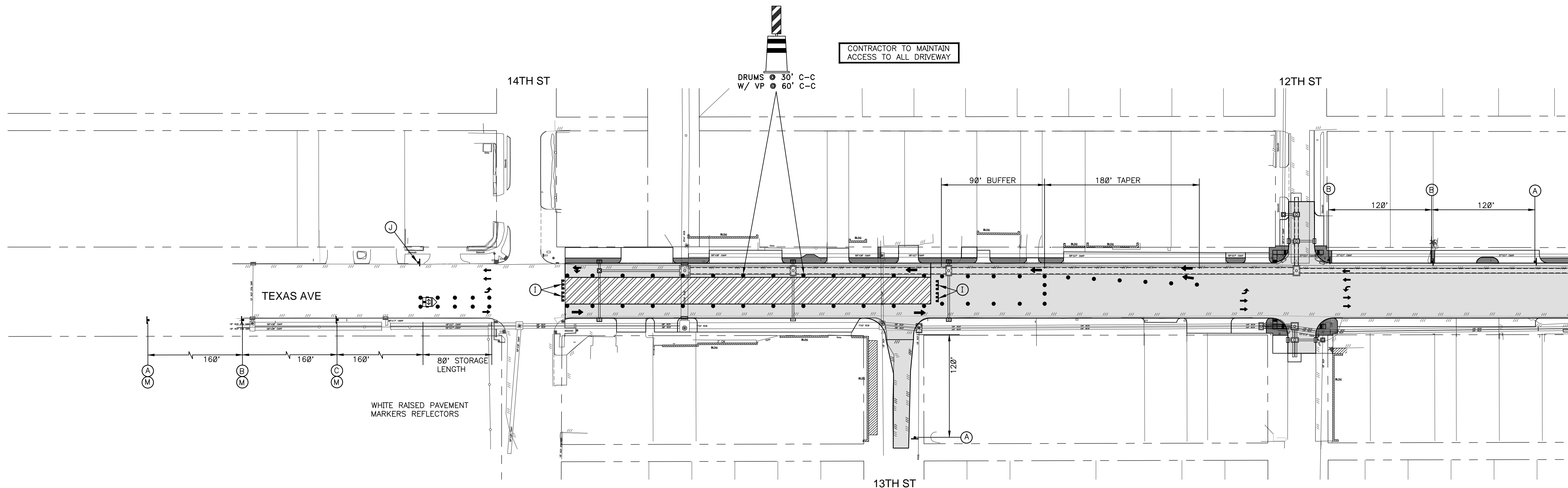
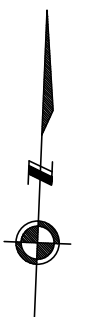
Galveston County, Texas

Texas Avenue Reconstruction

Phase 3 Traffic Layout

Job No.: 18-015 Scale: 1"=40'
Date: September, 2019 HORZ: 1"=40'
Dwn By: D. Fattig VERT:
Chk By: J Rudloff

SHEET 30 OF 52

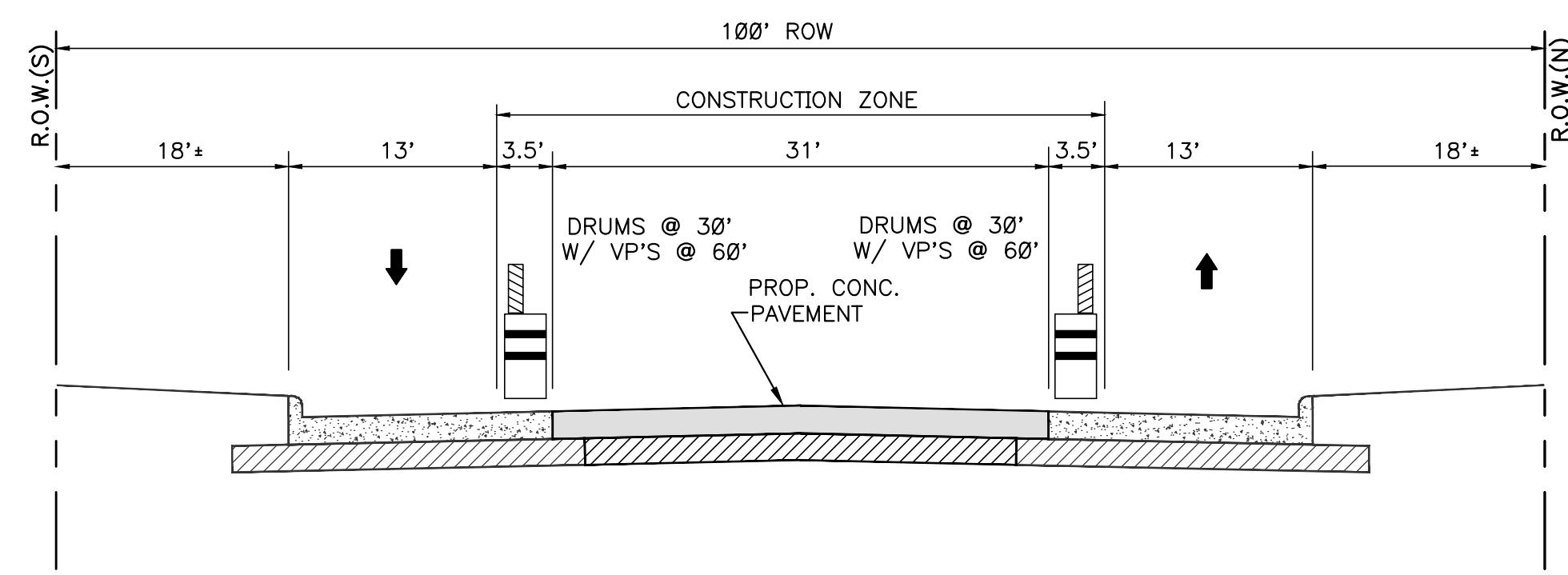


LEGEND

- PHASE 1 PVTM CONSTRUCTION
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- PHASE 2 PVTM CONSTRUCTION
- PHASE 3 PVTM CONSTRUCTION
- PHASE 4 PVTM CONSTRUCTION
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- COMPLETED CONCRETE PAVEMENT
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- RAISED PAVEMENT MARKERS REFLECTORS
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PHASE 4 PAVEMENT NOTES:

- CLOSE WESTBOUND LANES FROM 14th STREET TO 13th STREET PLACE TRAFFIC CONTROL SIGNAGE, DETOUR SIGNS, DEVICES AND DRUMS.
- PLACE TWO-WAY TRAFFIC AND PROVIDE TEMPORARY LOCAL ACCESS.
- FOLLOW UP WITH PAVING ON LANES FROM 14th STREET TO 13th STREET.
- CONTINUE TO MAINTAIN ACCESS TO DRIVEWAYS. (NO SEPARATE PAY)



PHASE 4 - TYPICAL SECTION

TEXAS AVE SPEED LIMIT
WEST OF 14th STREET - 35 MPH
EAST OF 14th STREET - 30 MPH

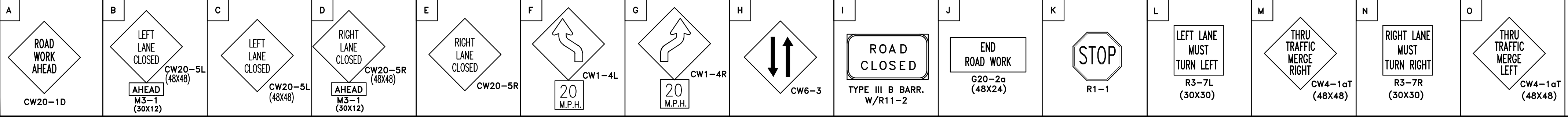
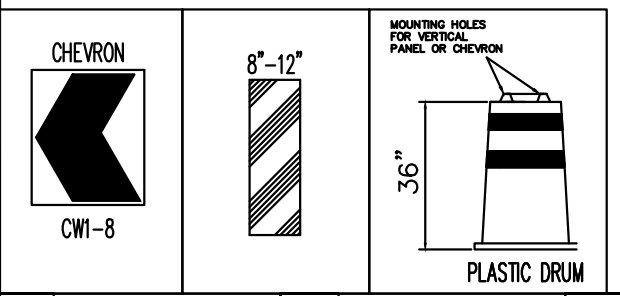
Posted Speed *	Formula	Minimum Desirable Taper Lengths **		Suggested Maximum Spacing of Channelizing Devices		Minimum Sign Spacing "x" Distance	Suggested Longitudinal Buffer Space "y"
		10' Offset	11' Offset	On a Taper	On a Tangent		
30	L=WS ² /60	150'	165'	30'	60'	120'	90'
35		205'	225'	35'	70'	160'	120'
40	L=WS ² /60	285'	295'	320'	40'	240'	155'
45		450'	495'	540'	45'	320'	195'
50		500'	550'	600'	50'	400'	240'
55		550'	605'	660'	55'	500'	295'
60		600'	660'	720'	60'	600'	350'
65		650'	715'	780'	65'	700'	410'
70		700'	770'	840'	70'	800'	475'
75	750'	825'	900'	75'	900'	540'	

* Conventional Roads Only
** Taper lengths have been rounded off.
L=Length of Taper(FT) W=Width of Offset(FT) S=Posted Speed(MPH)

SEE SHEET 32 FOR TYPICAL DETOUR LAYOUT FOR CONSTRUCTION OF SIDE STREETS

GENERAL NOTES:

- CONTRACTOR SHALL PROVIDE AND INSTALL ALL TRAFFIC CONTROL DEVICES AS PER THE LATEST REVISION OF THE TEXAS MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES (TXMUTCD).
- THE TRAFFIC CONTROL PLAN AND DETAILS INCLUDED IN THE PLAN DRAWINGS ARE PROVIDED AS A GUIDE TO THE CONTRACTOR AND ARE THE MINIMUM REQUIREMENTS. CONTRACTOR IS RESPONSIBLE FOR PREPARATION AND SUBMITTAL OF A REVISED TRAFFIC CONTROL PLAN FOR REVIEW AND APPROVAL IF IMPLEMENTED DIFFERENTLY FROM WHAT IS SHOWN ON THE PLAN DRAWINGS.
- THIS IS A GENERAL LAYOUT. IT IS NOT THE INTENT OF HAVING THE ENTIRE HALF OF ROADWAY REMOVE FROM END TO END AT ONE TIME. THE WORK SHALL BE LIMITED TO TWO BLOCKS AT A TIME.
- THE CONTRACTOR IS RESPONSIBLE FOR MAINTAINING ACCESS TO ALL BUSINESS DURING CONSTRUCTION. THIS MAY REQUIRE LEAVING SEGMENTS OF EXISTING PAVEMENT AVAILABLE FOR ACCESS WHILE ADJACENT PAVEMENT IS POURED AND CURED.
- ANY ADJUSTMENTS TO THE TRAFFIC CONTROL PLAN, INCLUDING PROVISION OF ADDITIONAL TRAFFIC CONTROL DEVICES AND SIGNAGE, AS NEEDED TO FACILITATE SMOOTH FLOW OF TRAFFIC AND TO ACCOMMODATE FIELD CONDITIONS SHALL BE CONSIDERED INCIDENTAL TO THE TRAFFIC CONTROL AND REGULATION BID ITEM.
- CONTRACTOR SHALL MAINTAIN ALL WEATHER ACCESS TO RESIDENTIAL AND COMMERCIAL PROPERTIES ADJACENT TO AND IN THE WORK AREAS AT ALL TIMES.
- CONTRACTOR IS RESPONSIBLE FOR MAINTAINING POSTAL SERVICE AND TRASH PICKUP SERVICE TO RESIDENTS DURING THE DURATION OF CONSTRUCTION OPERATIONS.



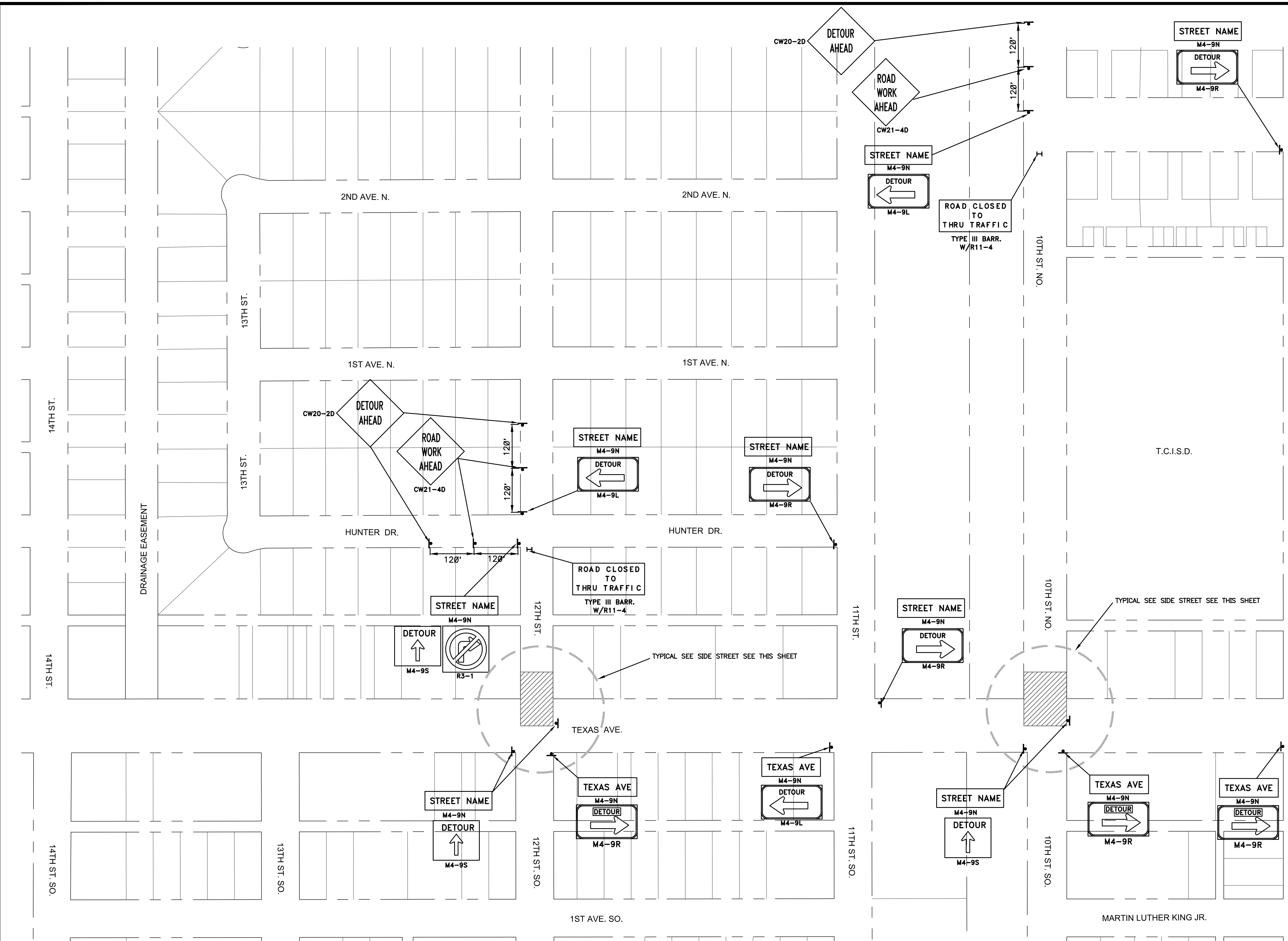
MK.	DESCRIPTION	DATE	DWN.	CHK.

STATE OF TEXAS
JOHN D. RUDLOFF
83386
LICENSED PROFESSIONAL ENGINEER
John D. Rudloff

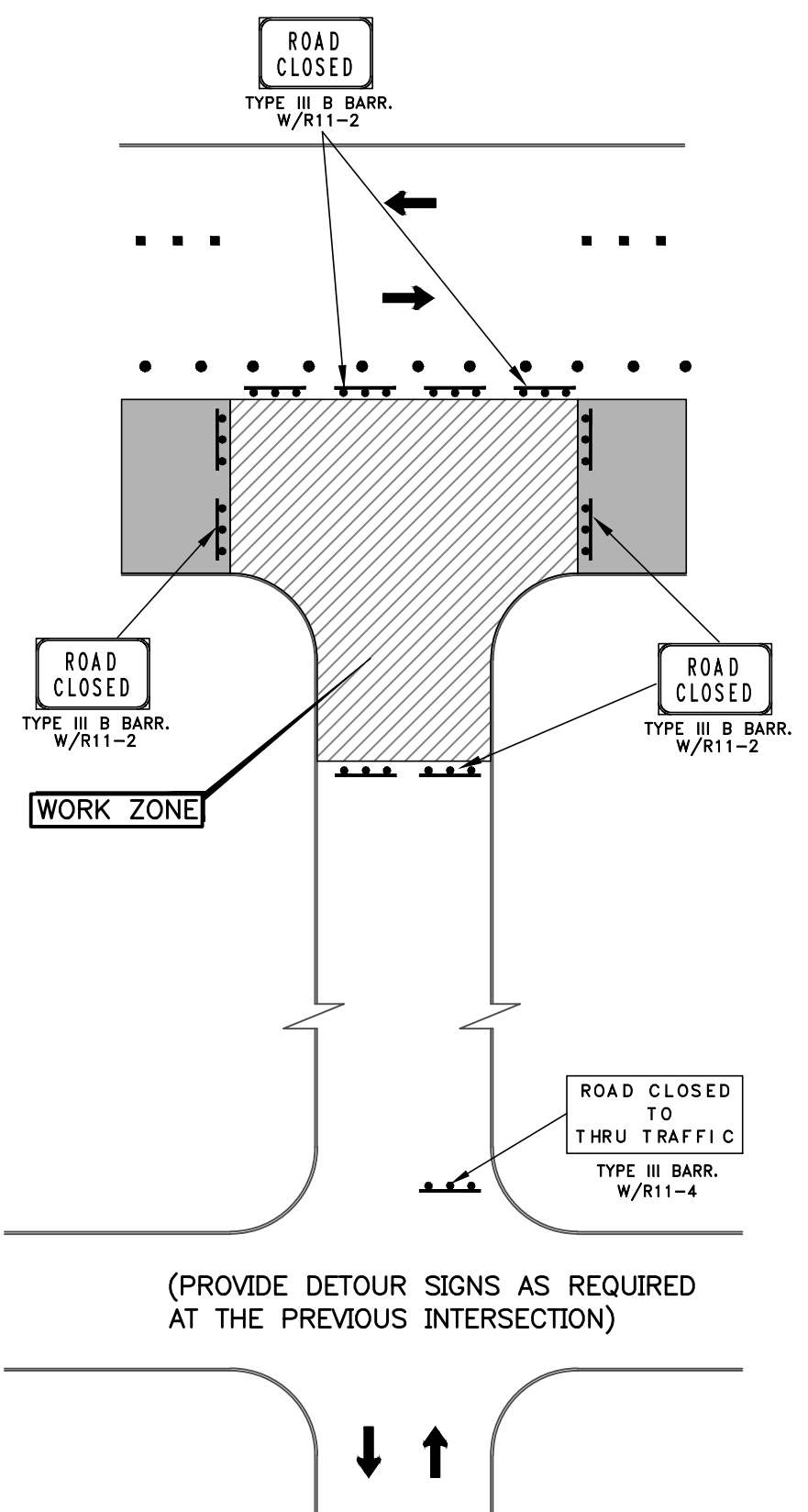
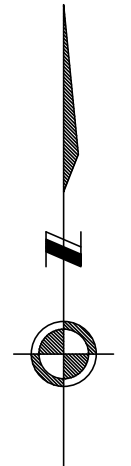
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Galveston County, Texas
Texas Avenue Reconstruction

Phase 4 Traffic Layout
Job No.: 18-015
Date: September, 2019
Dwn By: D. Fattig
Chk By: J. Rudloff
Scale: HORZ: 1"=40'
VERT:
SHEET 31 OF 52



9TH ST. NO.
10TH ST. NO.
11TH ST. NO.
10TH ST. SO.
11TH ST. SO.

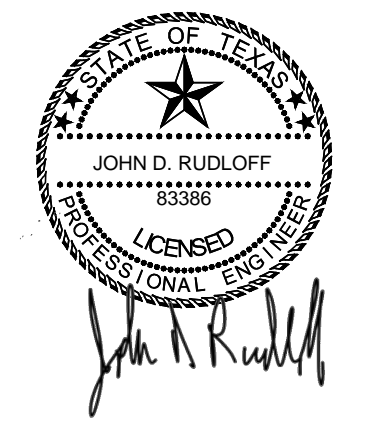


(PROVIDE DETOUR SIGNS AS REQUIRED AT THE PREVIOUS INTERSECTION)

SIDE STREET DETAIL

- LEGEND:**
- NEW PAVEMENT COMPLETED
 - PROP. PAVEMENT

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19



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Galveston County, Texas

Texas Avenue Reconstruction

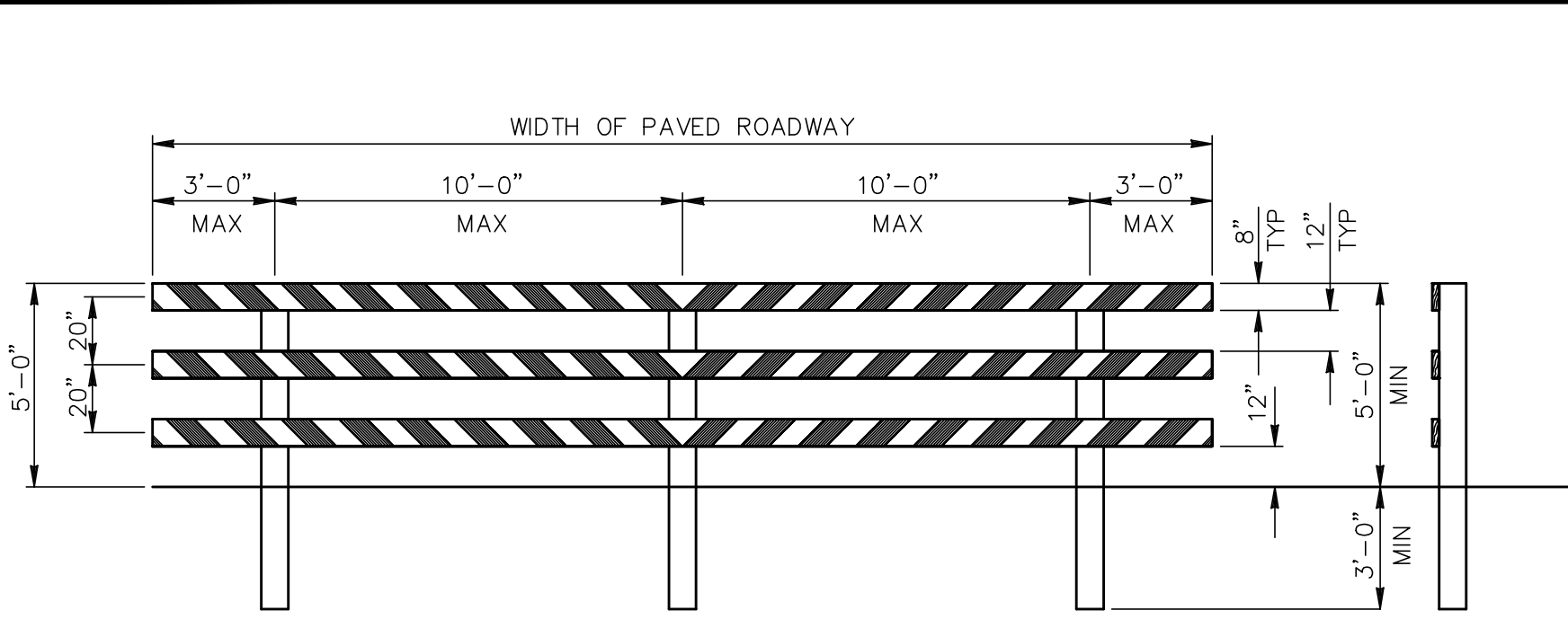
TYPICAL CONSTRUCTION PHASE LAYOUT FOR SIDE STREET DETAILS

Job No.: 18-015	Scale: HORIZ: NTS	SHEET 32 OF 52
Date: September, 2019	VERT: NA	
Dwn By: D. Fattig		
Chkd By: J. Rudloff		

TYPICAL SIDE STREET PAVEMENT NOTES:

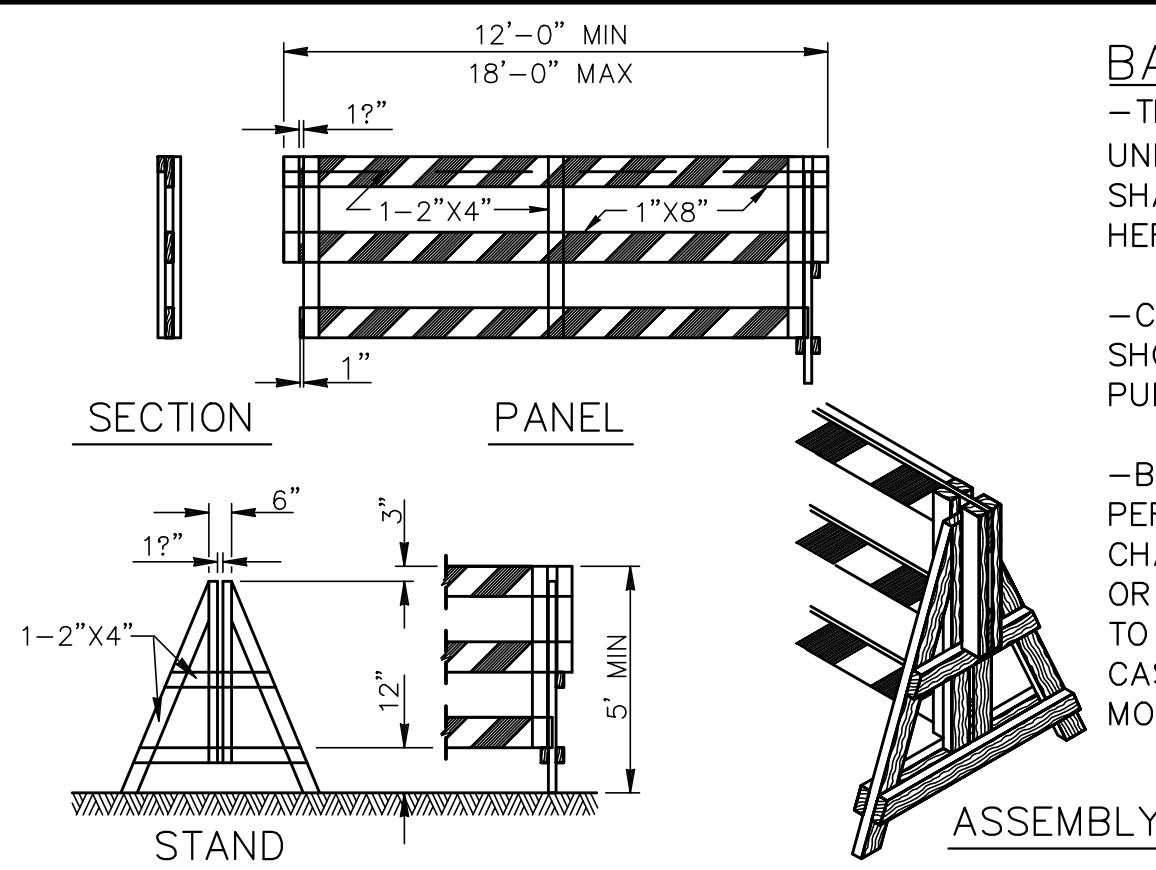
1. THIS IS A TYPICAL GENERAL LAYOUT FOR ALL INTERSECTION WORK (NORTH OR SOUTH SIDE). ADDITIONAL SIGNAGE & DETOUR SIGNS WILL BE REQUIRED FOR TO DETOUR TRAFFIC. CONTRACTOR TO PLACE ALL APPROPRIATE SIGNAGE TO DETOUR TRAFFIC AROUND CLOSED INTERSECTION.
2. CLOSE INTERSECTION AND PLACE TRAFFIC CONTROL SIGNAGE, DEVICES AND DRUMS AND APPROPRIATE DETOUR SIGNAGE AS REQUIRED.
3. NO TWO CONSECUTIVE INTERSECTION CAN BE CLOSE AT THE SAME TIME.
4. FOLLOW UP WITH PAVING.
5. CONTINUE TO MAINTAIN ACCESS TO DRIVEWAYS. (NO SEPARATE PAY)
6. CONTRACTOR TO REMOVE ALL SIGNAGE & DETOUR SIGNS UPON COMPLETION OF CONSTRUCTION AT INTERSECTING. THEN MOVE AND SET UP SIGNAGE AND DETOUR SIGNS FOR THE NEXT INTERSECTION.

SEE SHEET 24-31 FOR CONSTRUCTION PHASE LAYOUTS & SIGNAGE



TYPE III BARRICADE FOR END OF ROAD

FOR TYPE III BARRICADE FOR END OF ROAD, THE THREE (3) RAILS SHALL BE REFLECTIVE RED AND REFLECTIVE WHITE STRIPES ON SIDE FACING TRAFFIC



DEMOUNTABLE TYPE III BARRICADE

BARRICADE NOTES

-THE MOST RECENT EDITION OF THE TEXAS MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES, AND ITS REVISIONS, SHALL GOVERN THE CONSTRUCTION AND USE OF ALL ITEMS HEREIN DESCRIBED.

-CHANNELIZATION DEVICES OTHER THAN BARRICADES SHOULD NORMALLY BE USED FOR CHANNELIZATION PURPOSES.

-BARRICADES SHOULD NORMALLY BE PLACED PERPENDICULAR TO THE TRAFFIC FLOW. OTHER CHANNELIZING DEVICES, SUCH AS DRUMS, VERTICAL PANELS OR PORTABLE BARRIERS, SHOULD BE USED WHERE NEEDED TO SEPARATE TRAFFIC FROM THE WORK AREA. IN ALL CASES, THE BARRICADES SHOULD BE SO LOCATED AS TO MOST ADVANTAGEOUSLY WARN AND DIRECT TRAFFIC.

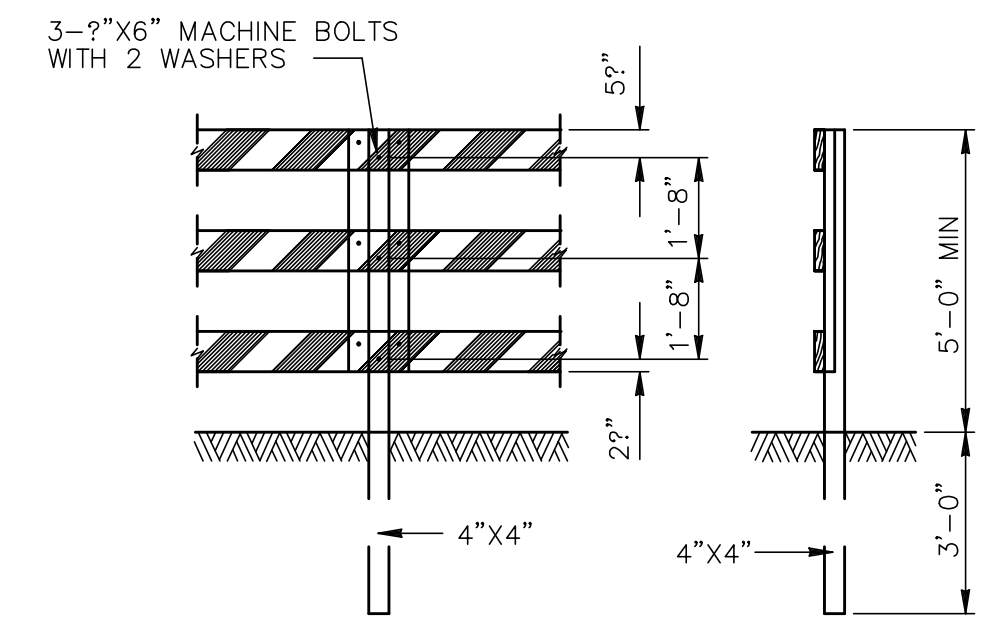
-BARRICADES MAY BE DESIGNED AND CONSTRUCTED FROM WOOD OR ANY OTHER SUITABLE MATERIAL IN A MANNER APPROVED BY THE DEPARTMENT OF TRAFFIC AND TRANSPORTATION. THE CONSTRUCTION DETAILS SHOWN HEREON ARE TYPICAL AND ARE SUGGESTED DETAILS FOR WOOD SUPPORT SYSTEMS FOR BARRICADES. THE DETAILS OF RAIL WIDTH AND STRIPING, NUMBER AND SPACING OF RAILS, MINIMUM LENGTH AND HEIGHT (ABOVE PAVEMENT) OF RAILS MUST BE ADHERED TO WHEN ALTERNATE DESIGNS ARE USED.

-BARRICADES ARE TO BE CONSTRUCTED OF CLEAN SOUND MATERIAL. ALL SURFACES ABOVE GROUND, WHICH ARE NOT STRIPED, SHALL BE WHITE EXCEPT THE UNPAINTED GALVANIZED METAL OR ALUMINUM COMPONENTS MAY BE USED. COMPONENTS MADE OF LUMBER SHALL BE PAINTED WITH A MINIMUM OF TWO COATS OF AN APPROVED BRAND OF WHITE PAINT TO SECURE THOROUGH COVERAGE AND A UNIFORM WHITE COLOR.

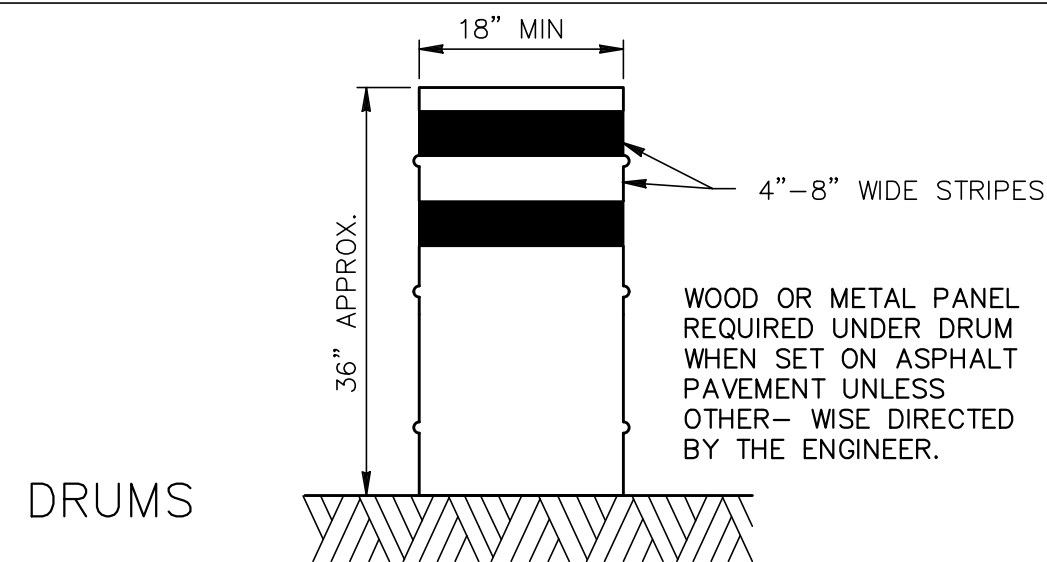
-THE REFLECTORIZED WHITE AND REFLECTORIZED ORANGE (REFLECTORIZED RED) STRIPES FOR BARRICADES, DRUMS AND VERTICAL PANELS SHALL BE CONSTRUCTED OF "HIGH INTENSITY" SHEETING AND SHALL BE MAINTAINED TO MEET THE APPEARANCE, COLOR AND REFLECTIVITY REQUIREMENTS SET BY DOT.

-THE CONTRACTOR SHALL MAINTAIN EACH BARRICADE IN A CLEAN AND GOOD CONDITION.

-BARRICADES SHALL BE REMOVED UPON COMPLETION OF THE WORK AND/OR THE ELIMINATION OF THE HAZARD ON ANY SECTION.



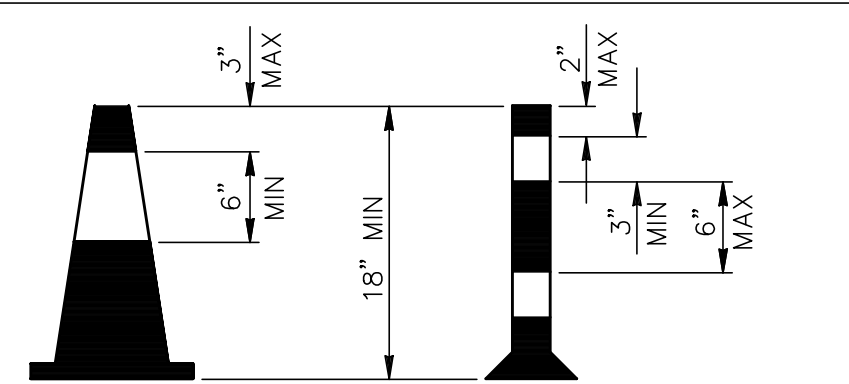
POST FOR TYPE III BARRICADE



DRUMS

-DRUMS, SET ON END, AND USED FOR TRAFFIC WARNING OR CHANNELIZATION SHALL BE APPROX 36" IN HEIGHT AND A MIN OF 18" IN DIAMETER. THE CONTRACTOR, AT HIS OPTION, MAY USE DRUMS MADE FROM STEEL BARRELS OR BLACK POLYETHYLENE PLASTIC DRUM LINERS WEIGHING APPROX EIGHT POUNDS EACH. THE MARKINGS ON DRUMS SHALL BE HORIZONTAL, CIRCUMFERENTIAL, REFLECTORIZED ORANGE AND REFLECTORIZED WHITE STRIPES, 4 TO 8 INCHES WIDE. THE FIRST REFLECTORIZED STRIPE SHOULD START WITHIN TWO (2) INCHES OF THE TOP OF THE DRUM. THERE SHALL BE AT LEAST TWO ORANGE AND TWO WHITE STRIPES ON EACH DRUM. IF THERE ARE NON- REFLECTORIZED SPACES BETWEEN THE HORIZONTAL ORANGE AND WHITE STRIPES, THEY SHALL BE NO MORE THAN 2 INCHES WIDE. METAL DRUMS SHALL BE PAINTED BLACK OR ORANGE BEFORE REFLECTORIZED STRIPES ARE ADDED. ALL DRUMS ON PROJECT WILL BE THE SAME COLOR. WHEN DRUMS ARE PLACED IN THE ROADWAY, APPROPRIATE WARNING SIGNS SHOULD BE USED. DURING HOURS OF DARKNESS, A FLASHING WARNING LIGHT SHOULD BE PLACED ON DRUMS USED SINGLY AS A WARNING DEVICE. STEADY BURN ELECTRIC LIGHTS OR DELINEATORS SHOULD BE PLACED ON DRUMS USED IN SERIES FOR TRAFFIC CHANNELIZATION. DRUMS SHALL BE WEIGHTED WITH SAND TO THE EXTENT INDICATED IN THE PLANS.

-CWI-8 CHEVRON SIGNS, CWI-6A ARROW SIGNS OR VP-1 VERTICAL PANELS MOUNTED ABOVE DRUMS MAY BE USED AS SUPPLEMENTS TO DRUM DELINEATION.

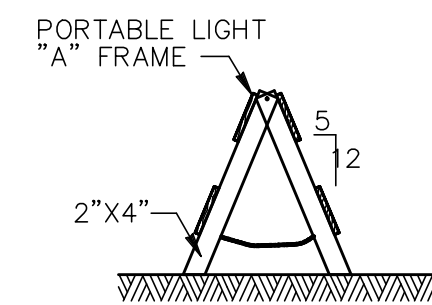


CONES

-TRAFFIC CONES AND TUBULAR MARKERS SHALL BE A MIN OF 18" INCHES IN HEIGHT WITH A BROADENED BASE AND MAY BE MADE OF VARIOUS MATERIALS TO WITHSTAND IMPACT WITHOUT DAMAGE TO THEMSELVES OR TO VEHICLES. LARGER SIZES SHOULD BE USED ON FREEWAYS AND OTHER ROADWAYS WHERE SPEED ARE RELATIVELY HIGH OR WHERE EVER MORE CONSPICUOUS GUIDANCE IS NEEDED. ORANGE SHALL BE THE PREDOMINANT COLOR ON CONES AND TUBULAR MARKERS. THEY SHOULD BE KEPT CLEAN AND BRIGHT FOR MAX TARGET VALUE. FOR NIGHTTIME USE THEY SHALL BE REFLECTORIZED OR EQUIPPED WITH LIGHTING DEVICES FOR MAX VISIBILITY. REFLECTORIZED MATERIAL SHALL HAVE A SMOOTH, SEALED OUTER SURFACE WHICH WILL DISPLAY THE SAME APPROX COLOR DAY AND NIGHT.

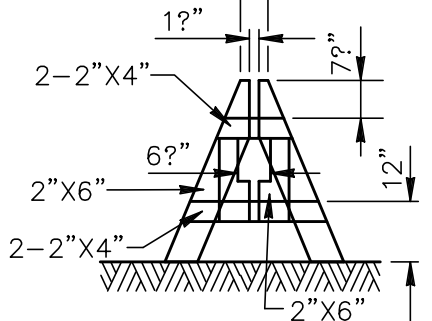
-REFLECTORIZATION OF TUBULAR MARKERS SHALL BE A MIN OF TWO THREE-INCH BANDS PLACED A MAX OF 2" FROM THE TOP WITH A MAX OF 6" BETWEEN THE BANDS. REFLECTORIZATION OF CONES SHALL BE PROVIDED BY A MIN 6" BAND PLACED A MAX OF 3" FROM THE TOP.

-CONES OR TUBULAR MARKERS ARE GENERALLY ONLY SUITABLE FOR TEMPORARY USAGE (UP TO 8 HOURS) WITH OTHER CHANNELIZATION DEVICES SUCH AS VERTICAL PANELS OR BARRICADES PREFERRED FOR LONGER TERM USAGE. CARE SHOULD BE TAKEN TO INSURE THAT THEY REMAIN IN THEIR PROPER LOCATION AND IN AN UPRIGHT POSITION.

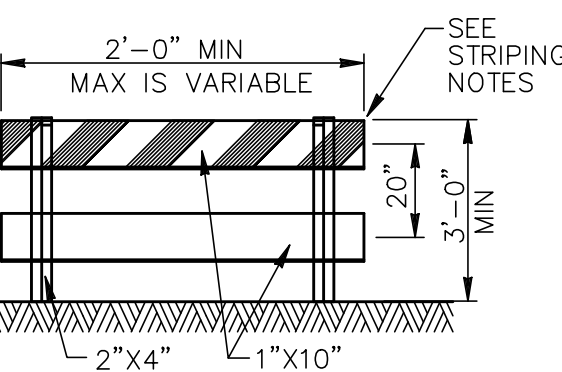


"A" FRAME

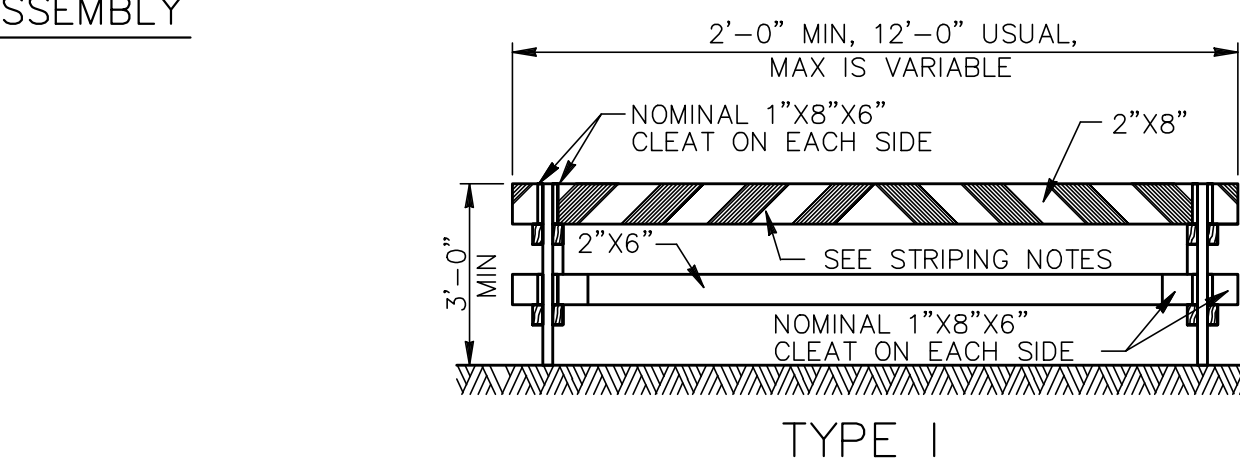
DEMOUNTABLE



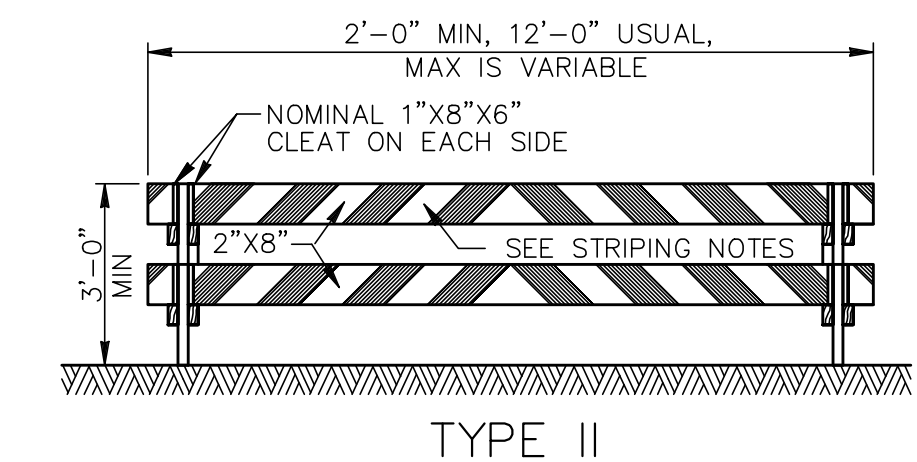
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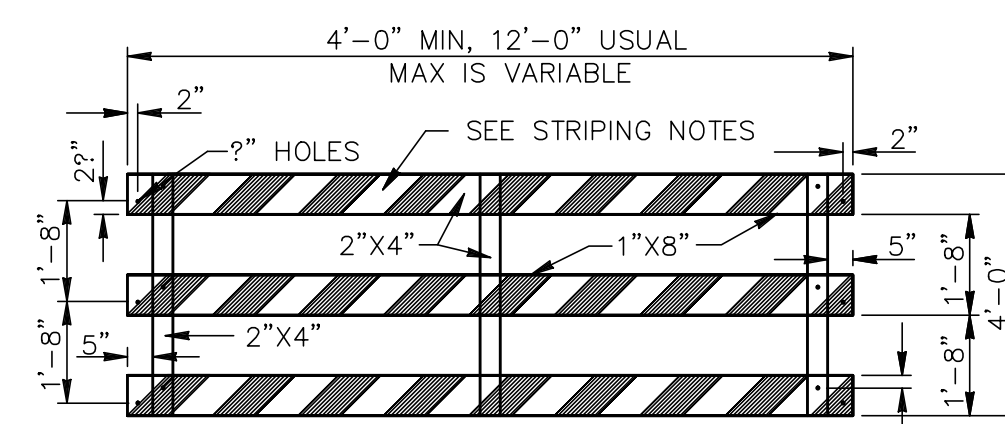
TYPE I



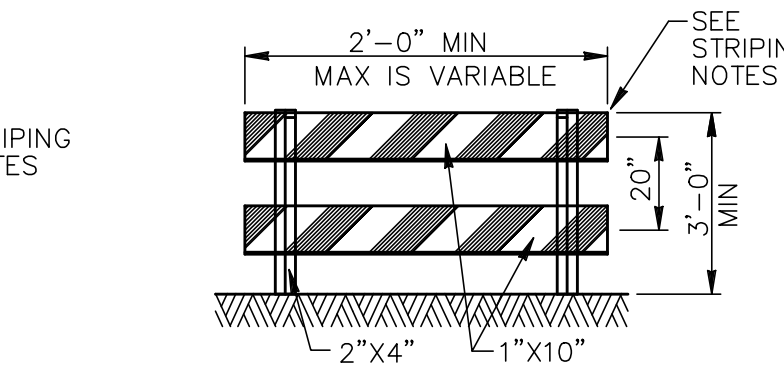
TYPE I



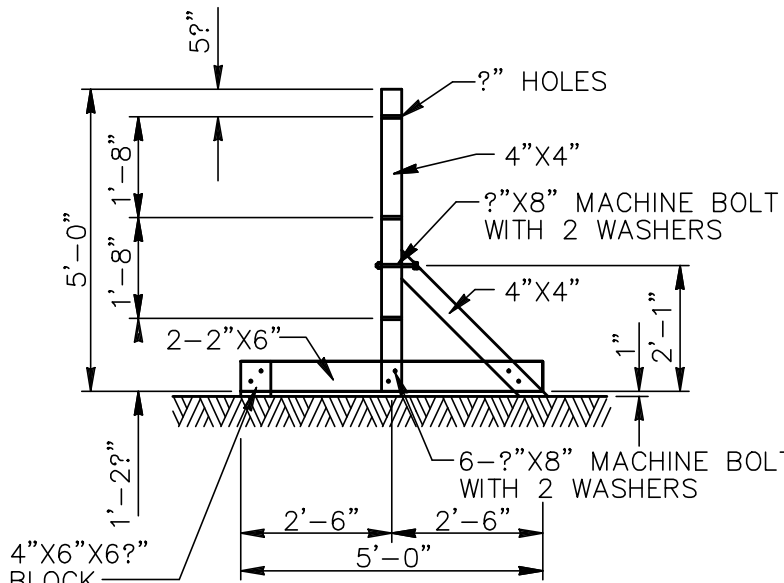
TYPE II



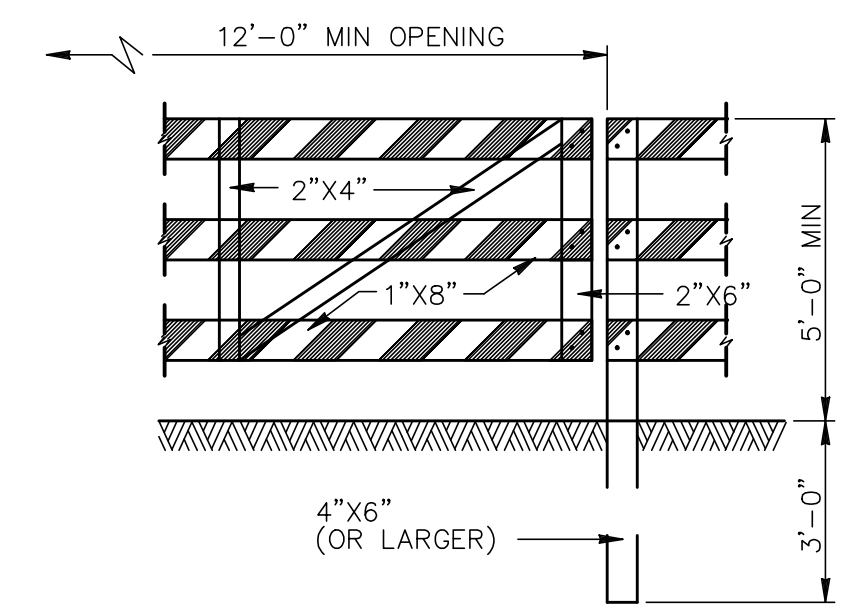
PANEL FOR TYPE III BARRICADE



TYPE II



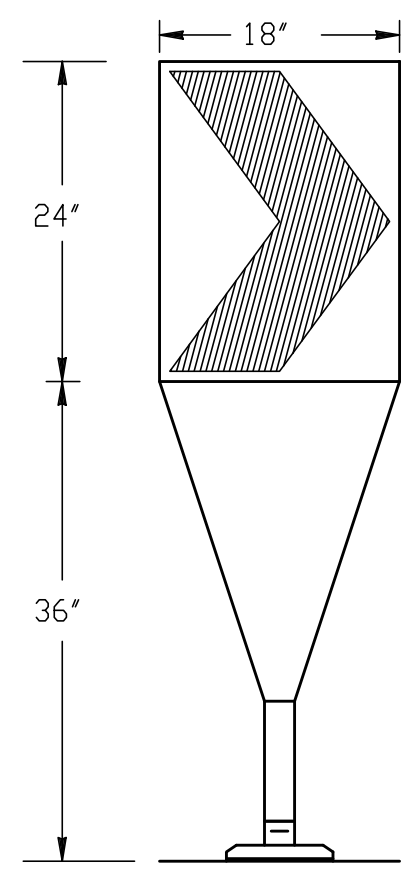
STAND FOR TYPE III BARRICADE



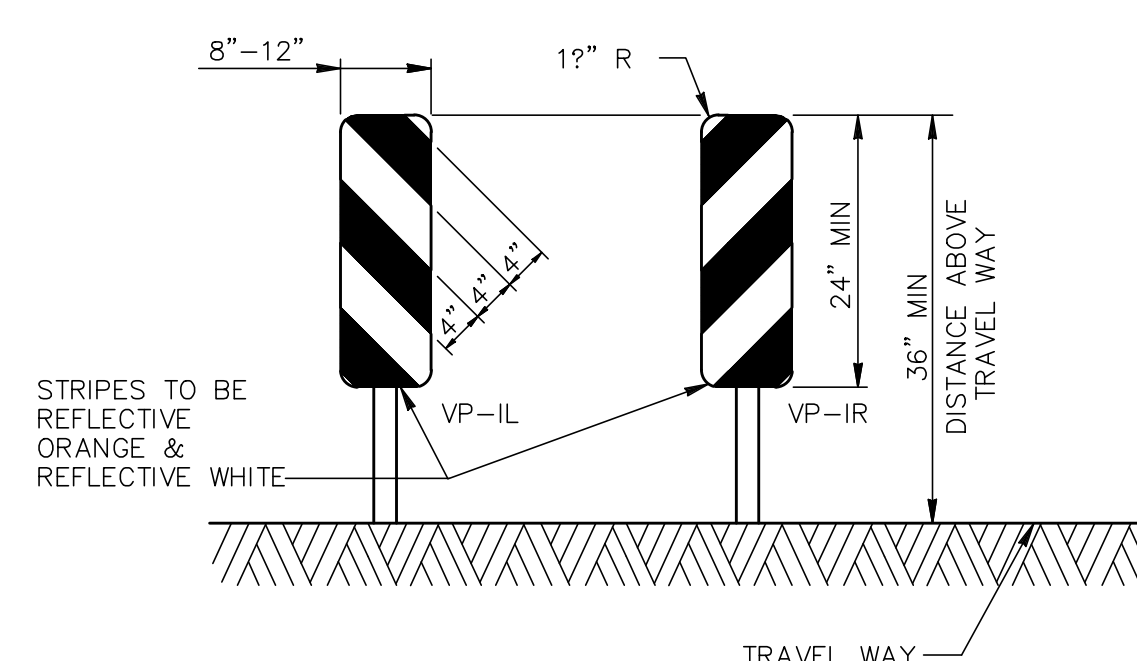
GATE FOR TYPE III BARRICADE

CHEVRONS

1. THE CHEVRON SHALL BE A VERTICAL RECTANGLE WITH A MINIMUM SIZE OF 12 BY 18 INCHES.
2. CHEVRONS ARE INTENDED TO GIVE NOTICE OF A SHARP CHANGE OF ALIGNMENT WITH THE DIRECTION OF TRAVEL AND PROVIDE ADDITIONAL EMPHASIS AND GUIDANCE FOR VEHICLE OPERATORS WITH REGARD TO CHANGES IN HORIZONTAL ALIGNMENT OF THE ROADWAY.
3. CHEVRONS, WHEN USED, SHALL BE ERECTED ON THE OUTSIDE OF A SHARP CURVE OR TURN, OR ON THE FAR SIDE OF AN INTERSECTION. THEY SHALL BE IN LINE WITH AND AT RIGHT ANGLES TO APPROACH-ING TRAFFIC. SPACING SHOULD BE SUCH THAT THE MOTORIST ALWAYS HAS THREE IN VIEW, UNTIL THE CHANGE IN ALIGNMENT ELIMINATES ITS NEED.
4. TO BE EFFECTIVE, THE CHEVRON SHOULD BE VISIBLE FOR AT LEAST 500 FEET.
5. CHEVRONS SHALL BE ORANGE WITH A BLACK NON-REFLECTIVE LEGEND. SHEETING FOR THE CHEVRON SHALL BE RETROREFLECTIVE TYPE E (FLUORESCENT PRISMATIC) CONFORMING TO DEPARTMENTAL MATERIAL SPECIFICATION DMS-8300, UNLESS NOTED OTHERWISE. THE LEGEND SHALL BE BLACK VINYL NON-REFLECTIVE DECAL SHEETING MEETING THE REQUIREMENTS OF DMS-8320.

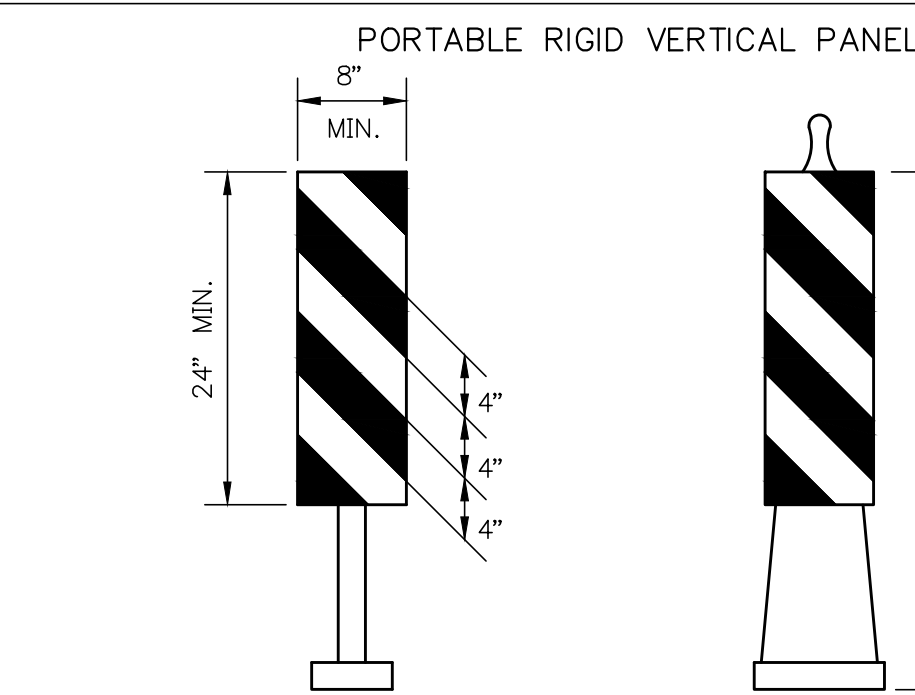


Fixed Base w/ Approved Adhesive (Driveable Base, or Flexible Support can be used)



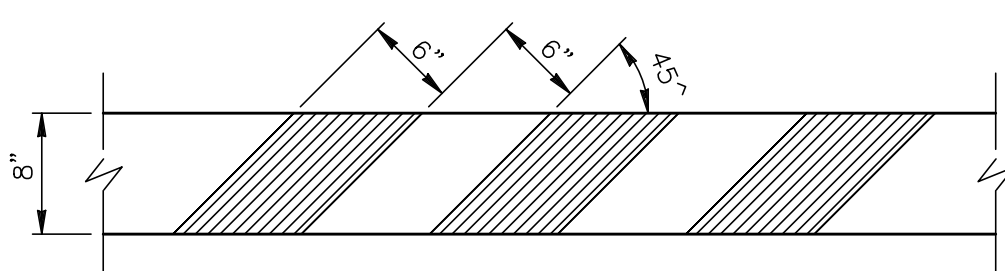
VERTICAL PANELS (VP)

VERTICAL PANELS ARE NORMALLY USED AS CHANNELIZING DEVICES TO INDICATE TANGENT OR NEARLY TANGENT ROADWAY ALIGNMENT WHERE GOOD TARGET VALUE OF A DEVICE IS NEEDED IN DAYTIME AS WELL AS THE NIGHTTIME. IN ADDITION, VERTICAL PANELS SHOULD BE USED AT THE EDGE OF SHOULDER DROP-OFFS AND OTHER SUCH AREAS AS LANE TRANSITIONS WHERE POSITIVE DAY AND NIGHT DELINEATION MAY BE REQUIRED. VERTICAL PANELS SHOULD BE MOUNTED BACK TO BACK IF USED AT THE EDGE OF CUTS ADJACENT TO TWO-WAY TWO LANE ROADWAYS. STRIPES SHOULD ALWAYS SLOPE DOWNWARD TOWARD THE TRAVELED WAY.



See Compliant Products List for alternate designs.

1. CHANNELIZING DEVICES ON SELF-RIGHTING SUPPORTS MAY BE A VERTICAL PANEL, OPPOSING LANE DIVIDER OR CHEVRON.
2. CHANNELIZING DEVICES ON SELF-RIGHTING SUPPORTS SHALL BE USED AT LOCATIONS DETAILED ELSEWHERE IN THE PLANS. THESE DEVICES SHALL CONFORM TO THE "TEXAS MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES".
3. THE CONTRACTOR SHALL MAINTAIN DEVICES IN A CLEAN CONDITION AND REPLACED DAMAGED, NON-REFLECTIVE, FADED, OR BROKEN DEVICES AND BASES AS NECESSARY.
4. PORTABLE BASES SHALL BE FABRICATED FROM VIRGIN AND/OR RECYCLED RUBBER. APPROXIMATE WEIGHT OF PORTABLE BASES SHALL BE 35 LBS.



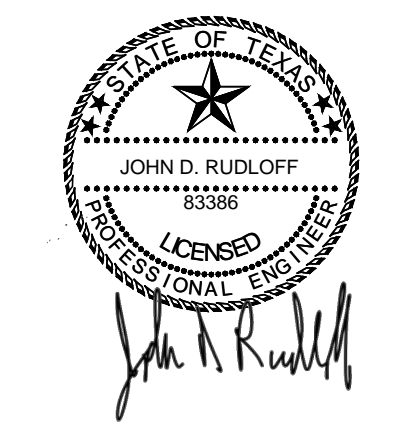
STRIPING FOR BARRICADE

FOR ALL TYPES OF BARRICADES WITH RAILS LESS THAN 3'-0" LONG, STRIPES 4" WIDE SHALL BE USED. IDENTIFICATION MARKINGS MAY BE SHOWN ONLY ON BACK SIDE OF BARRICADE RAILS.

-STRIPING SHOULD COVER THE FULL WIDTH OF THE RAIL. STRIPING OF RAILS, PANELS, ETC, SHOULD SLOPE DOWNWARD AT AN ANGLE OF 45° DEGREES IN DIRECTIONS TRAFFIC IS TO PASS.

-WHERE A BARRICADE EXTENDS ENTIRELY ACROSS A ROADWAY, IT IS DESIRABLE THAT THE STRIPES SLOPE DOWNWARD IN THE DIRECTION TOWARD WHICH TRAFFIC MUST TURN IN DETOURING. WHEN BOTH RIGHT AND LEFT TURNS ARE PROVIDED FOR, THE CHEVRON STRIPING SHOULD SLOPE DOWNWARD IN BOTH DIRECTIONS FROM THE CENTER OF THE BARRICADE.

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19



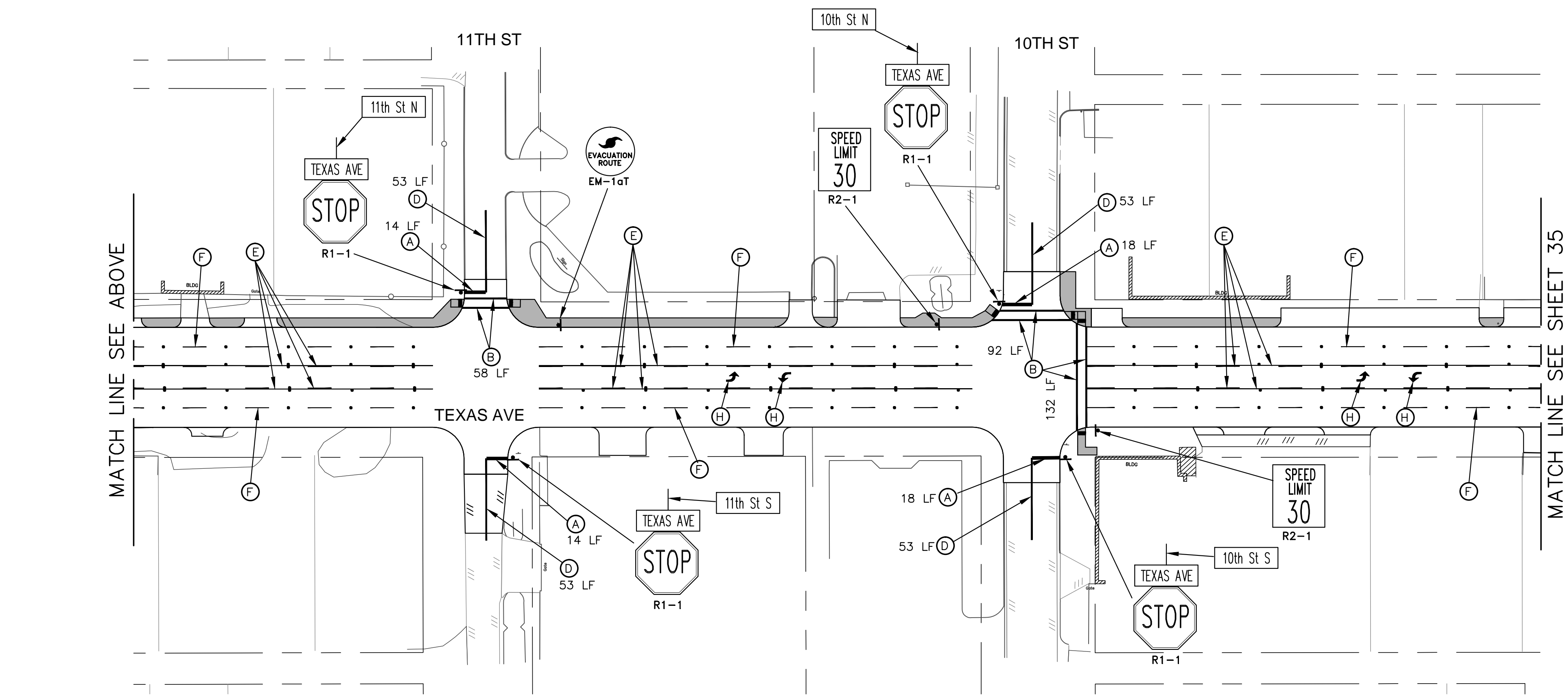
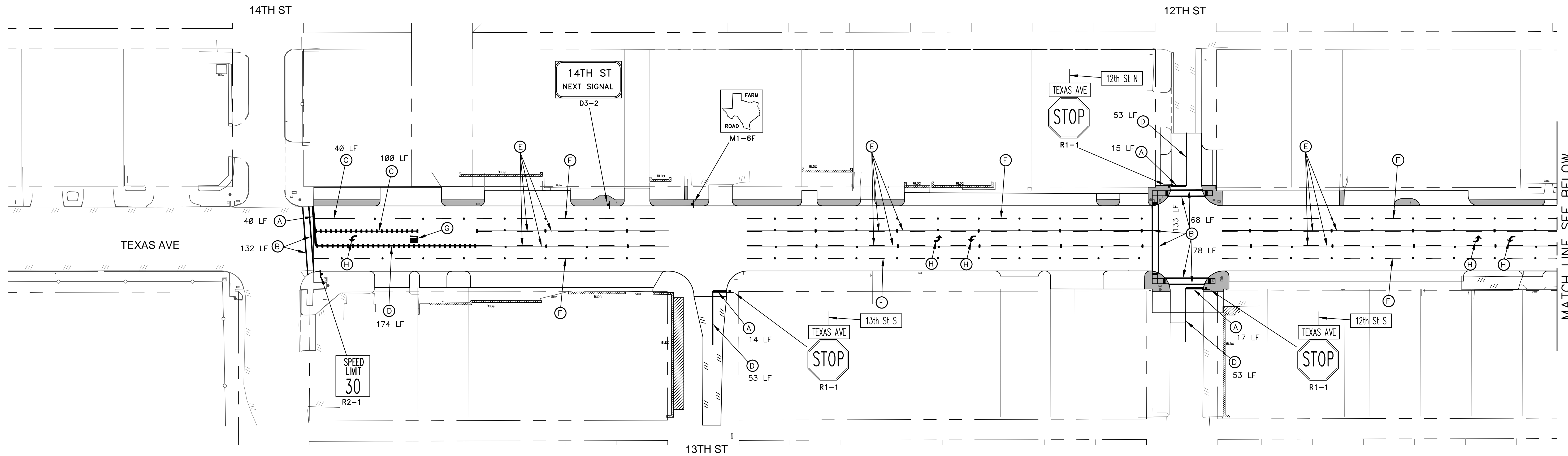
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Galveston County, Texas

Texas Avenue Reconstruction

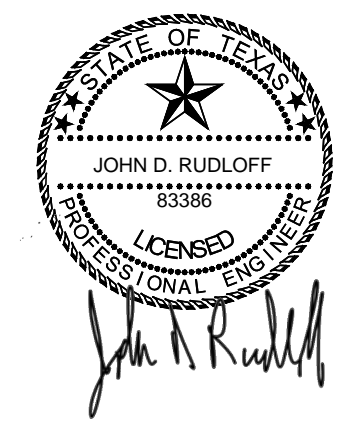
Traffic Control Details

Job No.: 18-015	Scale: N/A	SHEET
Date: September, 2019	HORZ: N/A	33
Dwn By: D. Fattig	VERT: N/A	
Chk By: J Rudloff		OF 52



- NOTES:**
- ALL STRIPING & MARKERS SHALL CONFORM TO THE TEXAS MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES FOR STREETS AND HIGHWAYS, LATEST EDITION.
 - EXISTING STRIPING & MARKERS NOT SHOWN TO BE REPLACED THAT ARE DAMAGED DURING CONSTRUCTION SHALL BE REPLACED AT NO ADDITIONAL COST TO THE PROJECT.
 - REMOVAL OF EXISTING STRIPING AND MARKERS SHALL BE CONSIDERED INCIDENTAL TO THE PROJECT.

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19

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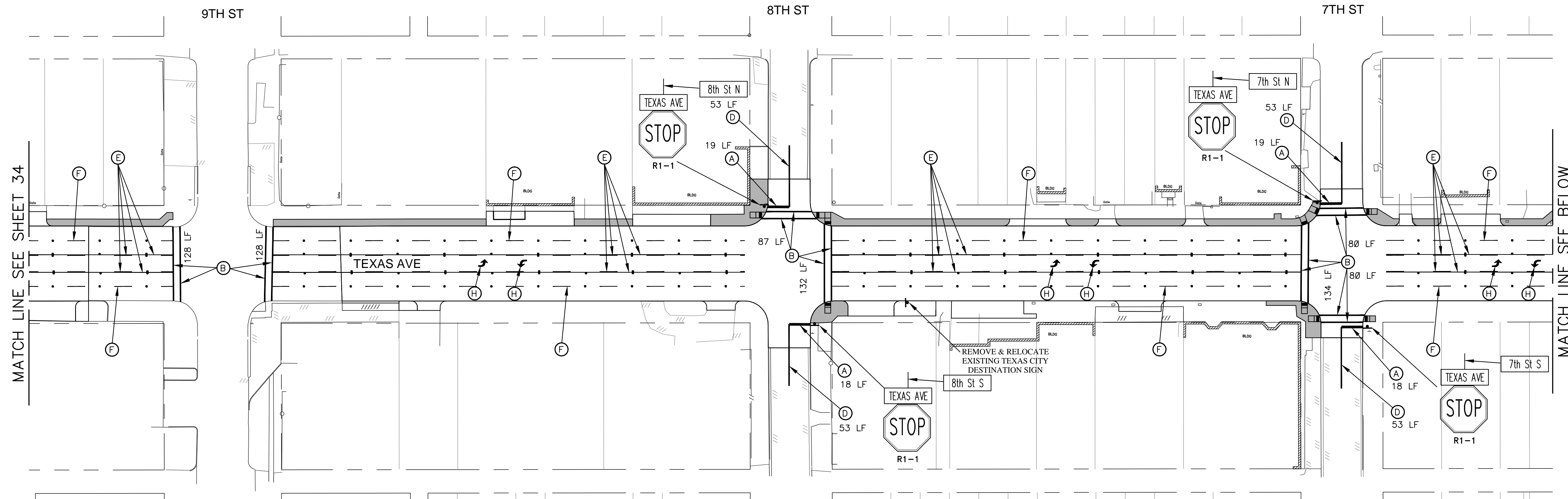
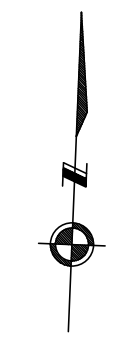
Galveston County, Texas

Texas Avenue Reconstruction

Striping Layout - I

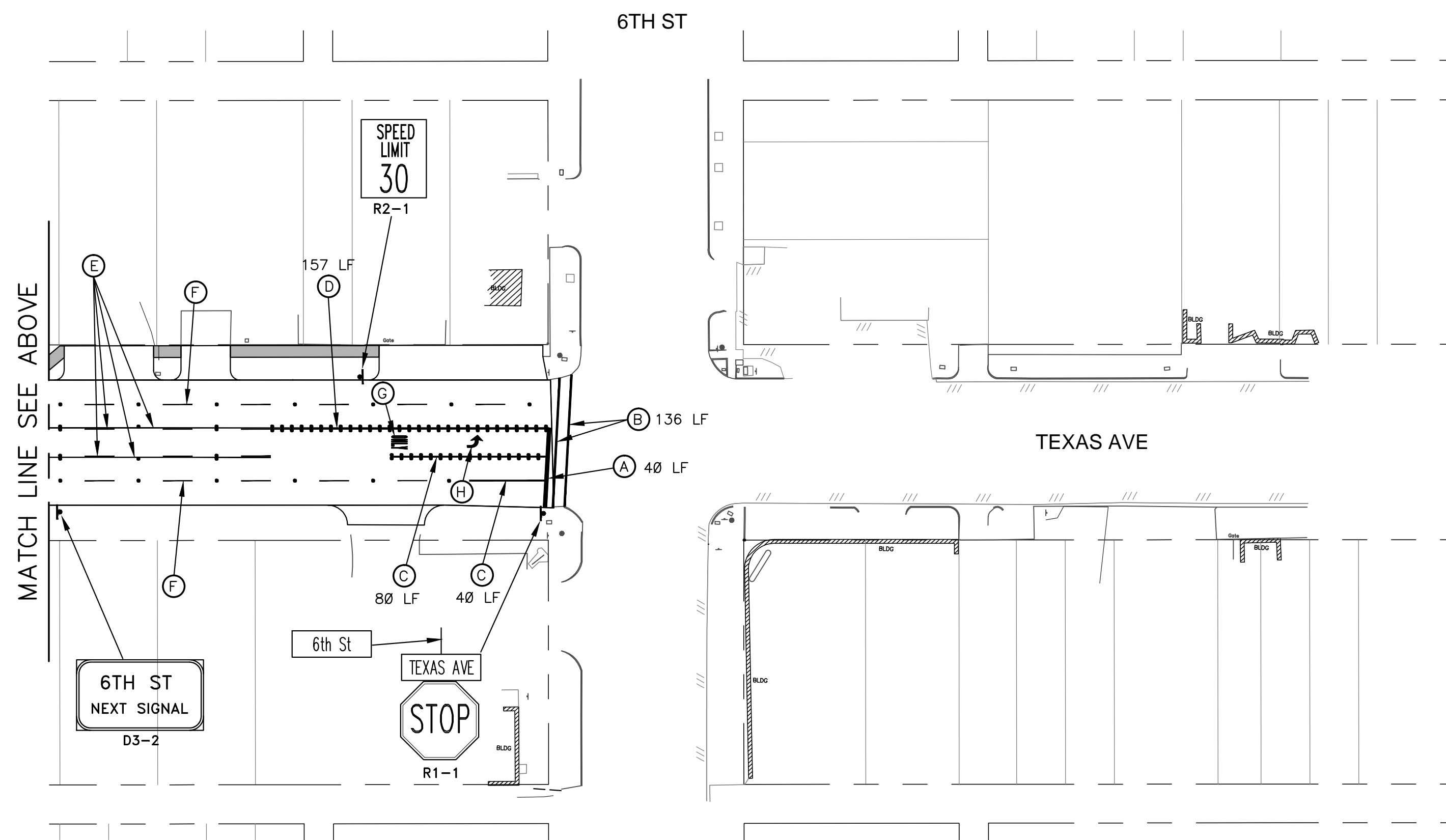
- LEGEND:**
- (A) REFLECTIVE MARKING 24" SOLID (WHITE)
 - (B) REFLECTIVE MARKING 12" SOLID (WHITE)
 - (C) REFLECTIVE MARKING 8" SOLID (WHITE)
 - (D) REFLECTIVE MARKING 4" SOLID DOUBLE (YELLOW) (LENGTH SHOWN IS THE TOTAL SINGLE)
 - (E) REFLECTIVE MARKING 4" BROKEN/SOLID (YELLOW)
 - (F) REFLECTIVE MARKING 4" BROKEN/SOLID (WHITE)
 - (G) REFLECTIVE MARKING (WORD "ONLY") (WHITE)
 - (H) REFLECTIVE MARKING (ARROW) (WHITE)
 - (R1) REMOVE & REPLACE SIGN (NO SEPARATE PAY)
 - (R2) REMOVE OLD SIGN & REPLACE WITH NEW SIGN
 - RPM (RAISED PAVEMENT MARKERS/BUTTONS)

Job No.: 18-015	Scale: HORZ: 1"=50'	SHEET 34 OF 52
Date: September, 2019	VERT: 1"=50'	
Dwn By: D. Fattig		
Chkd By: J. Rudloff		



MATCH LINE SEE SHEET 34

MATCH LINE SEE BELOW

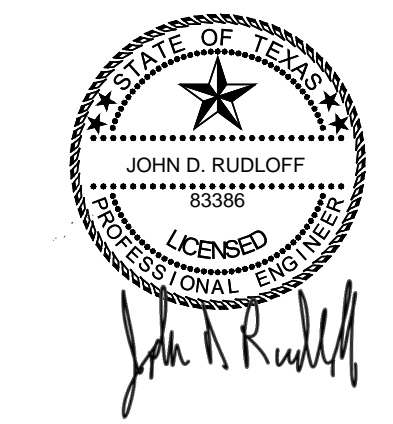


MATCH LINE SEE ABOVE

- NOTES:**
- ALL STRIPING & MARKERS SHALL CONFORM TO THE TEXAS MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES FOR STREETS AND HIGHWAYS, LATEST EDITION.
 - EXISTING STRIPING & MARKERS NOT SHOWN TO BE REPLACED THAT ARE DAMAGED DURING CONSTRUCTION SHALL BE REPLACED AT NO ADDITIONAL COST TO THE PROJECT.
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MK.	DESCRIPTION	DATE	DWN.	CHK.

- LEGEND:**
- (A) REFLECTIVE MARKING 24" SOLID (WHITE)
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 - (G) REFLECTIVE MARKING (WORD "ONLY") (WHITE)
 - (H) REFLECTIVE MARKING (ARROW) (WHITE)
 - (R) REMOVE & REPLACE SIGN (NO SEPARATE PAY)
 - (N) REMOVE OLD SIGN & REPLACE WITH NEW SIGN
 - RPM (RAISED PAVEMENT MARKERS/BUTTONS)



9-13-19

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Galveston County, Texas

Texas Avenue Reconstruction

Striping Layout - II

Job No.: 18-015	Scale: HORZ: 1"=50'	SHEET 35 OF 52
Date: September, 2019	VERT:	
Dwn By: D. Fattig		
Chkd By: J. Rudloff		

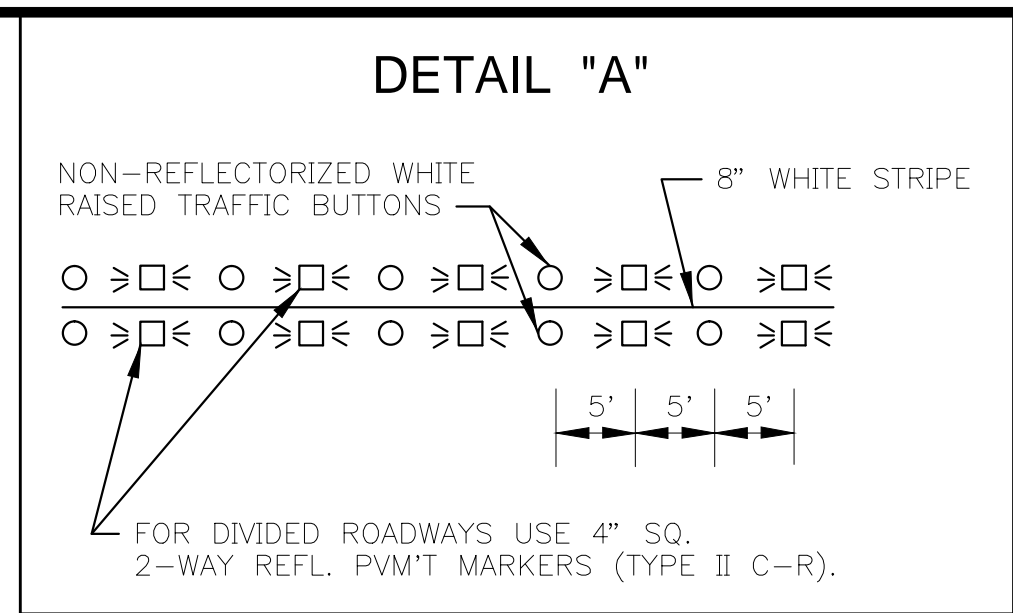
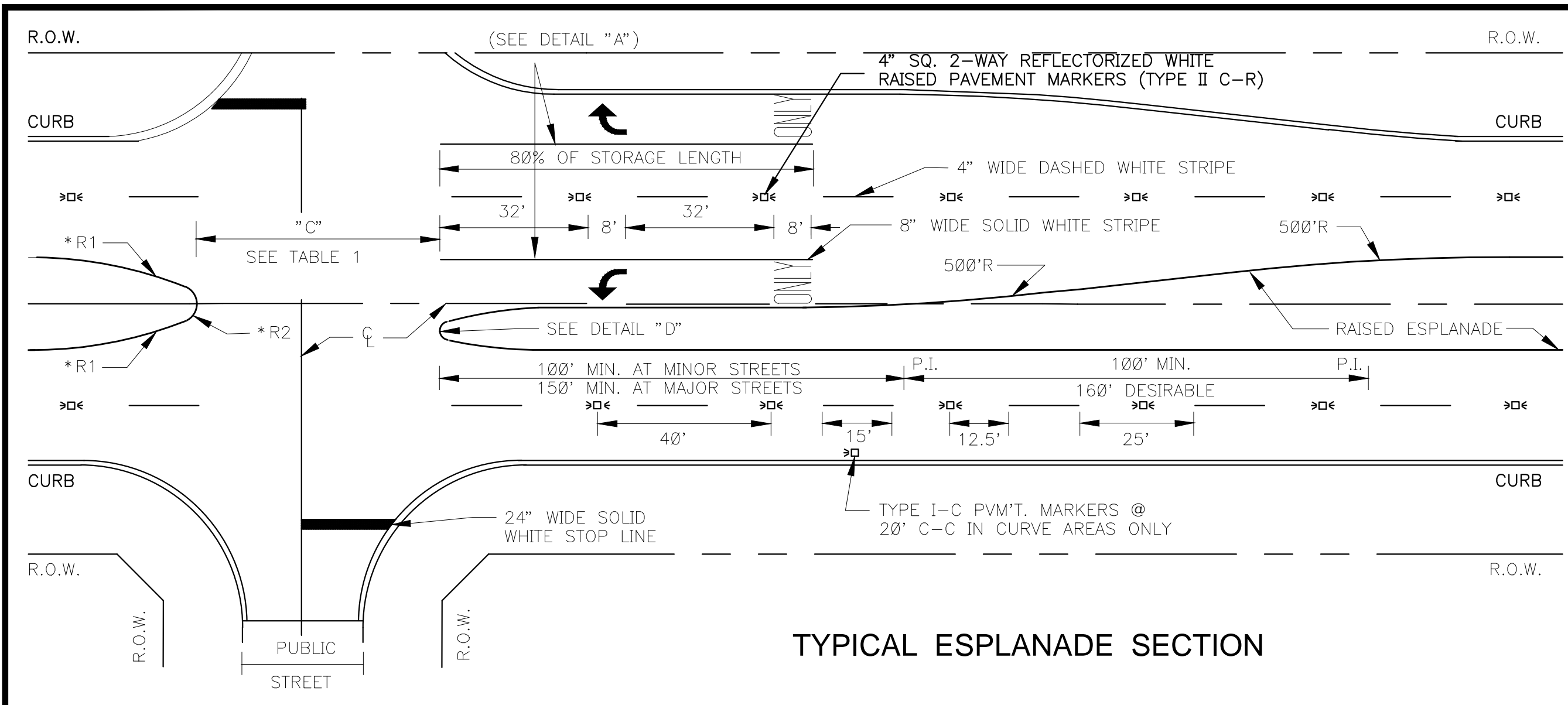


TABLE 1

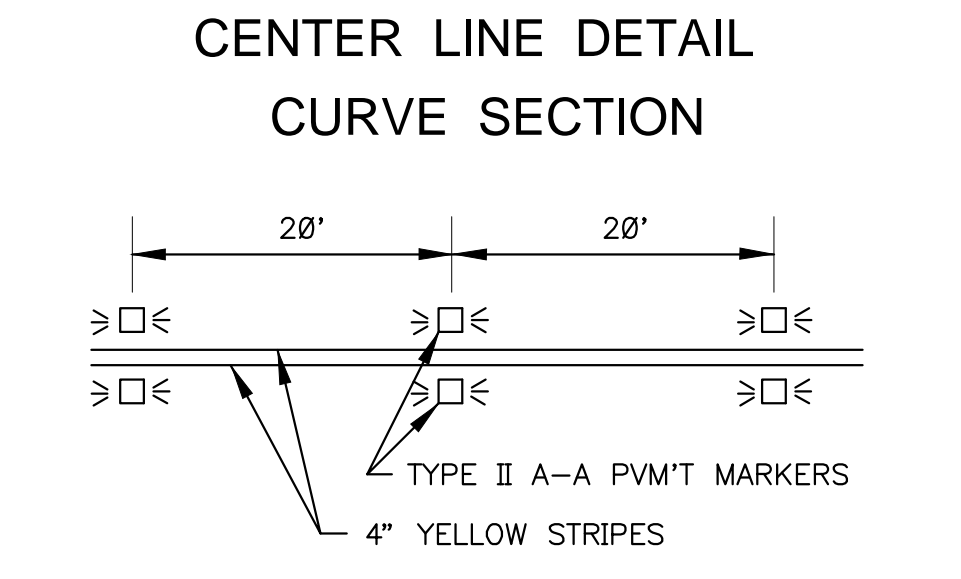
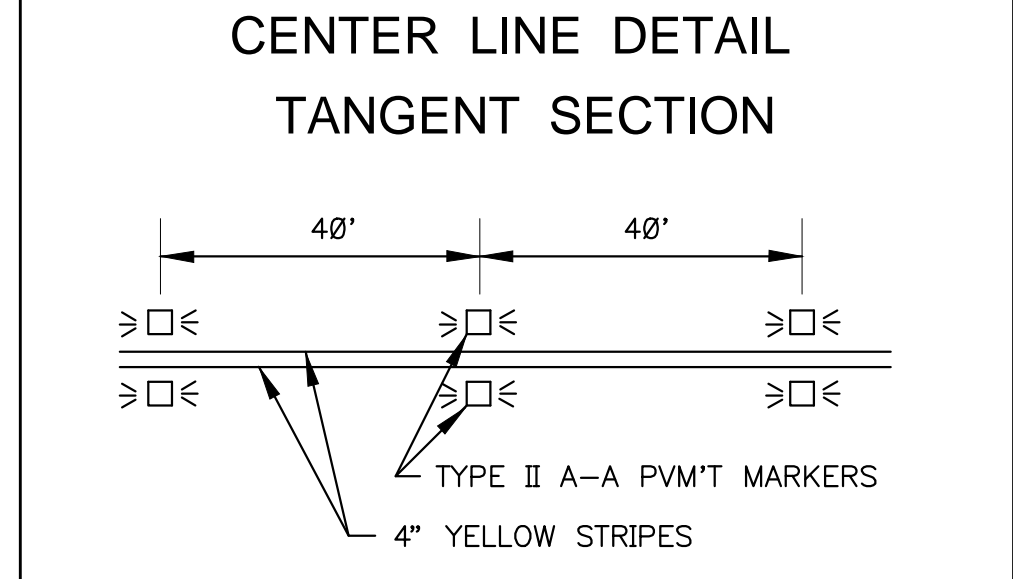
TYPICAL LENGTH OF ESPLANADE OPENING "C" FOR PUBLIC STREET

ESPLANADE INTERRUPTION	(1) NO LTB	(1) 1 LTB	(1) 2LTB
UNDIVIDED STREET < 40'	45'	52(2)	60'
44'	50'	56(2)	60'
DIVIDED STREET	D+10'	D+10'	D+10'

NOTES:
 (1) LEFT TURN BAY
 (2) DISTANCE FROM CENTERLINE OF OPENING TO ESPLANADE NOSE WITH LEFT TURN LANE MUST BE 30'

RADIUS DIMENSIONS

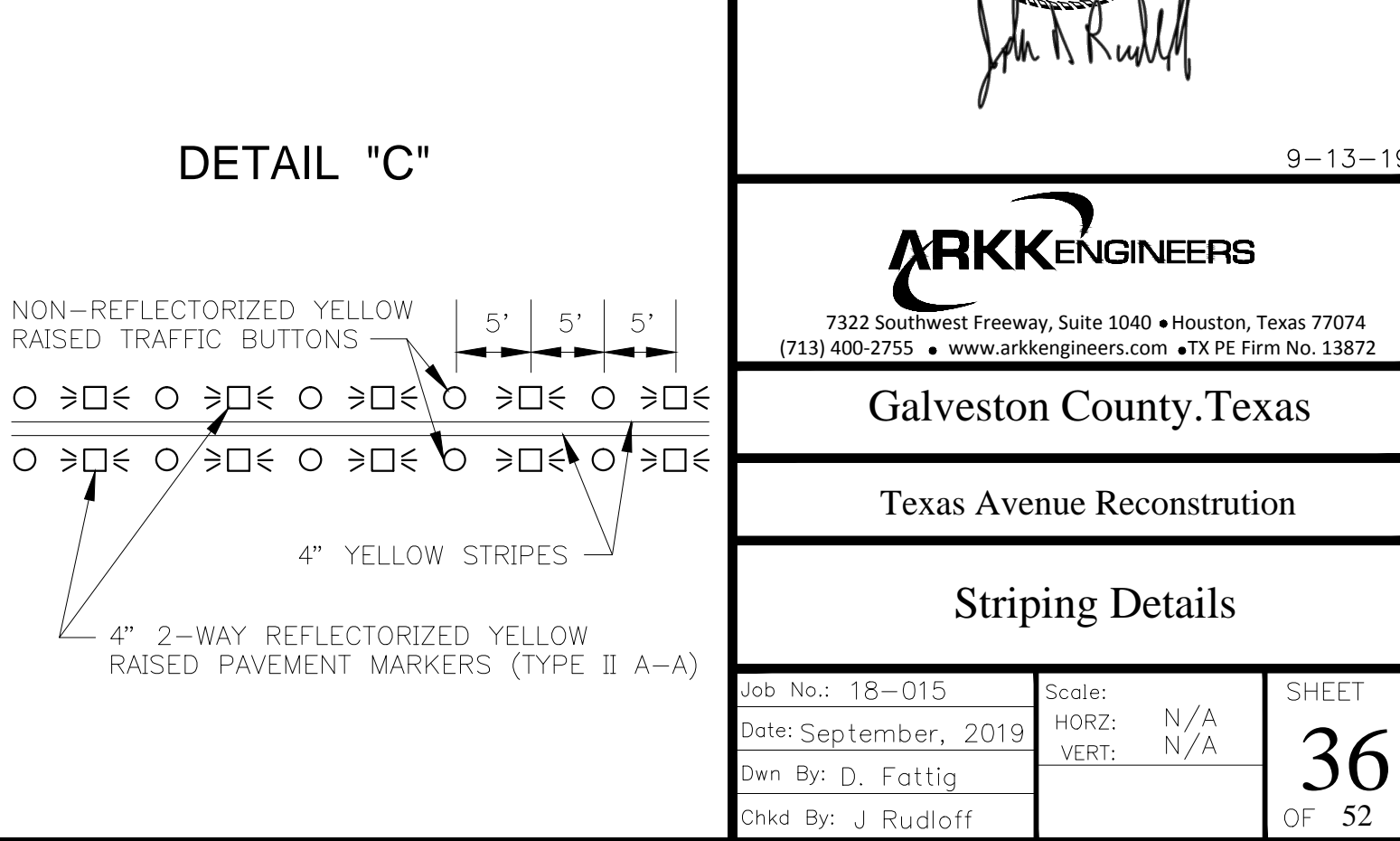
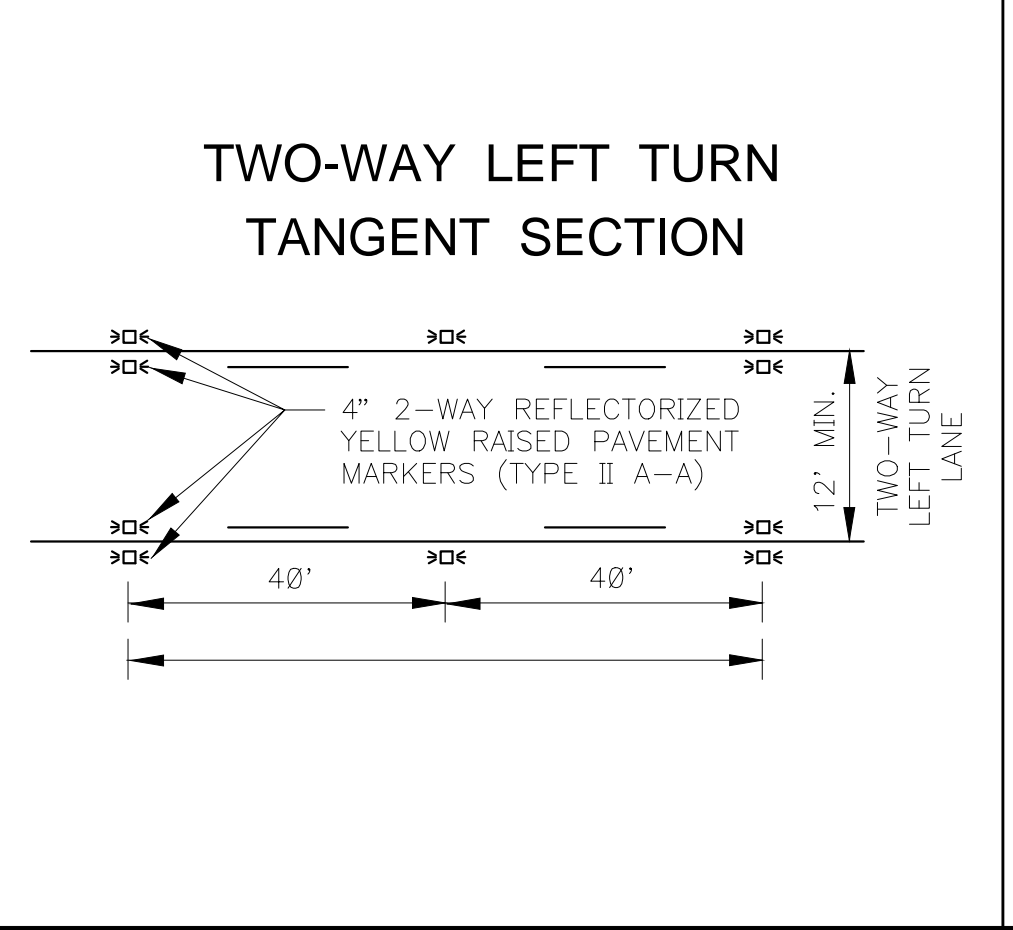
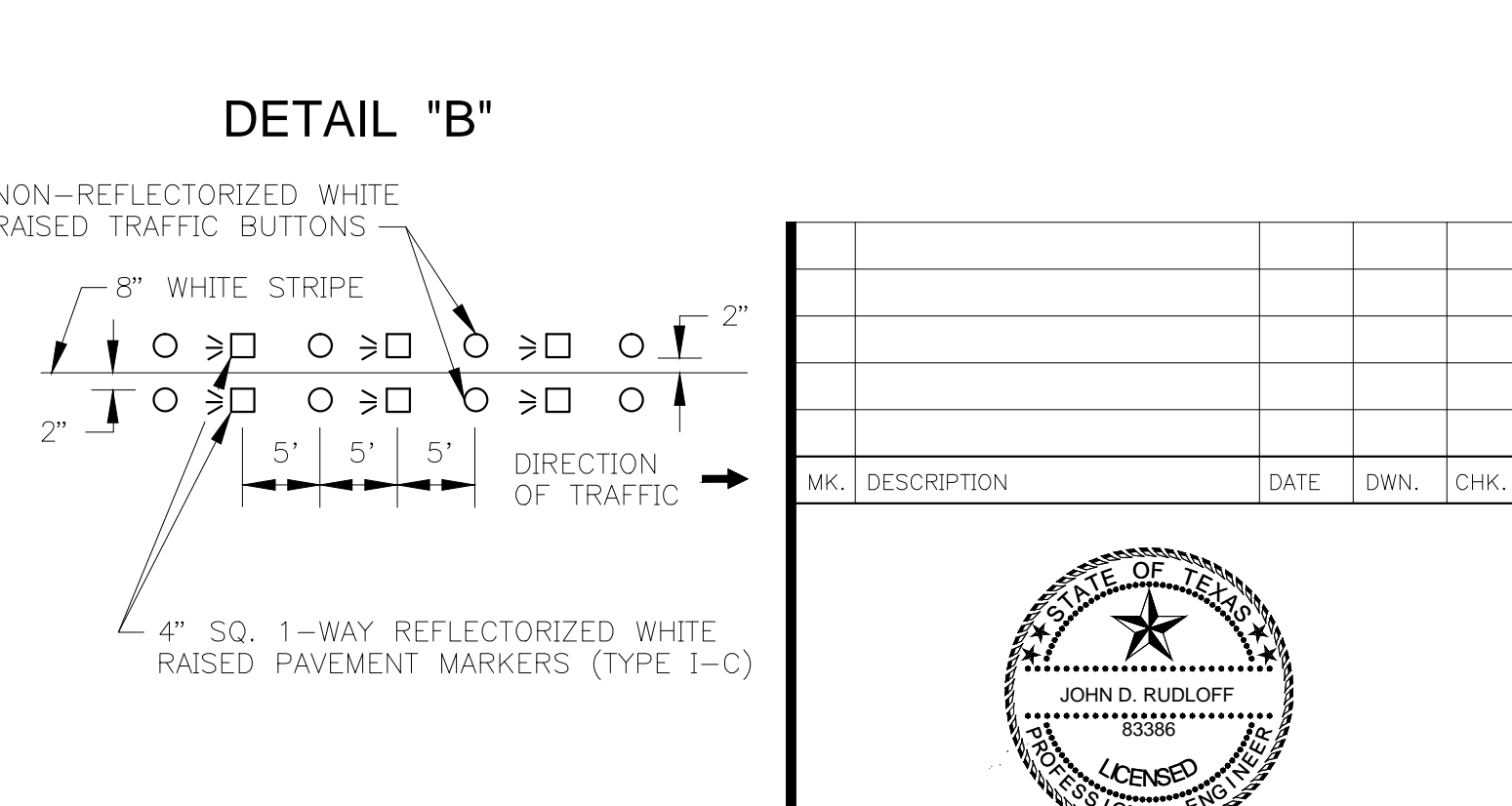
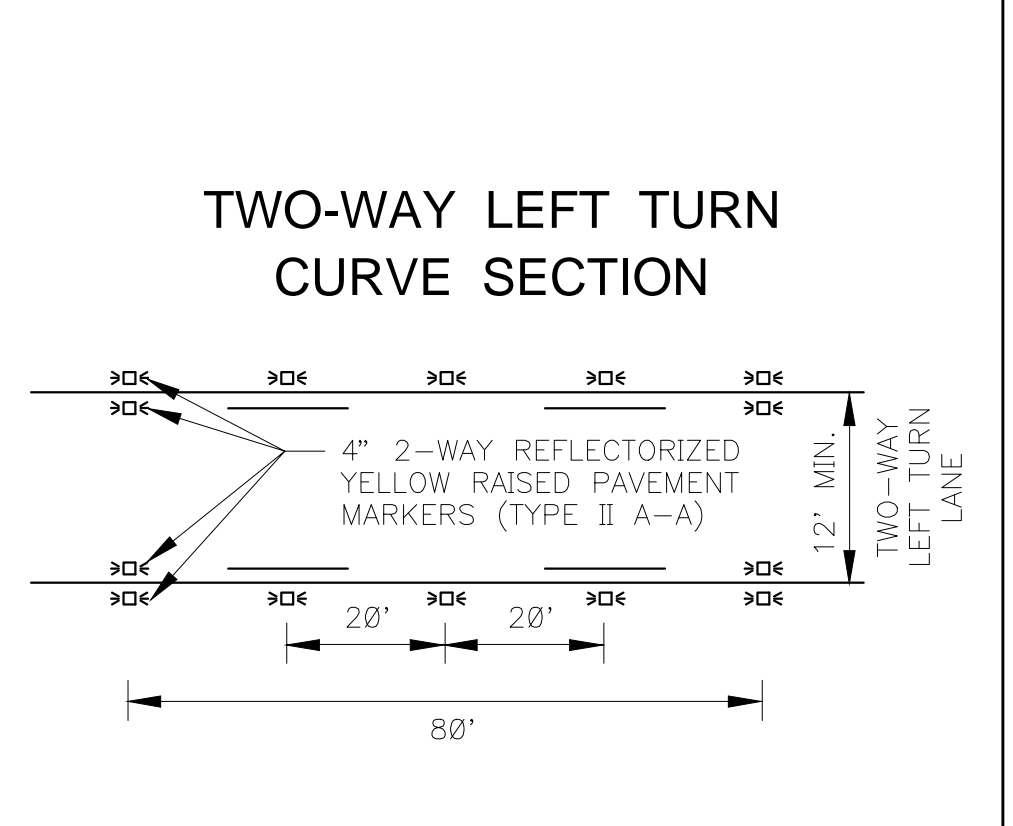
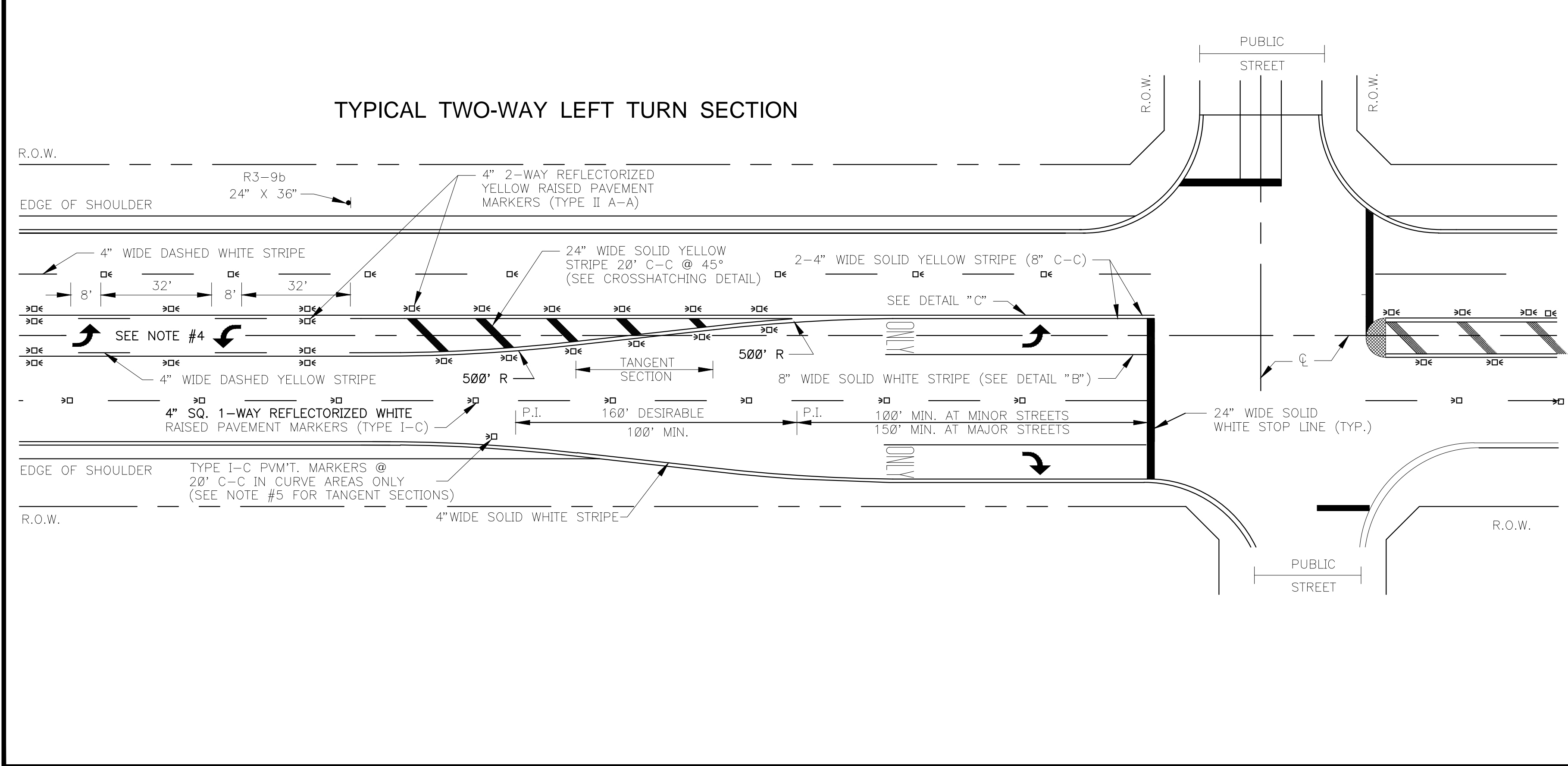
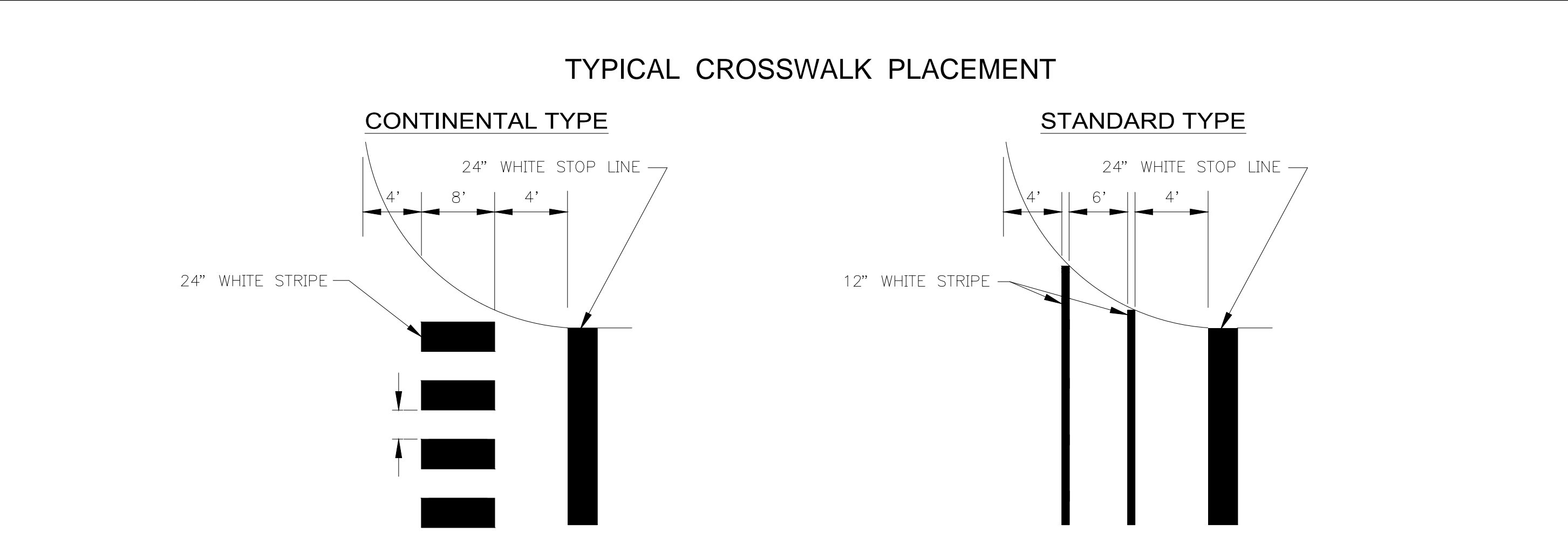
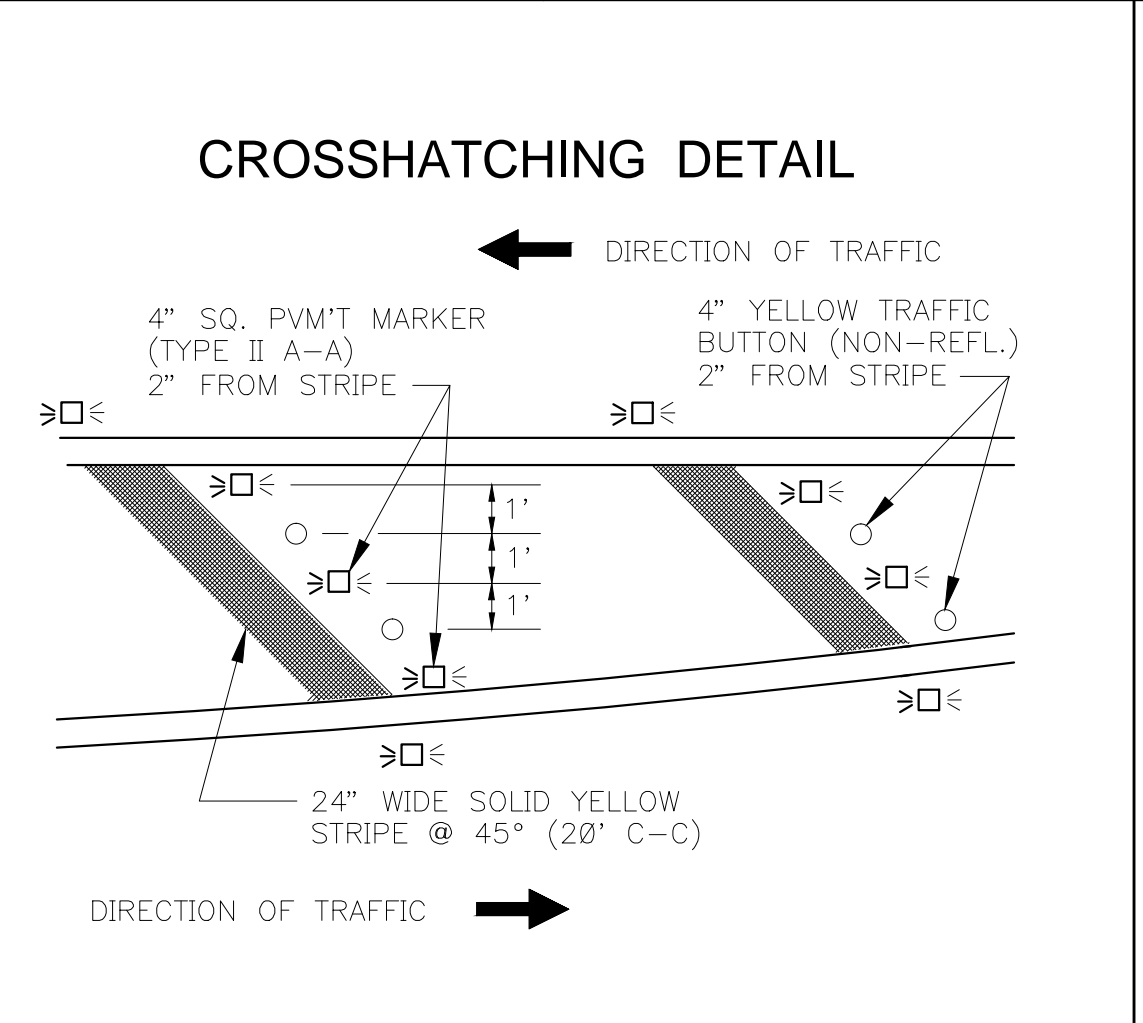
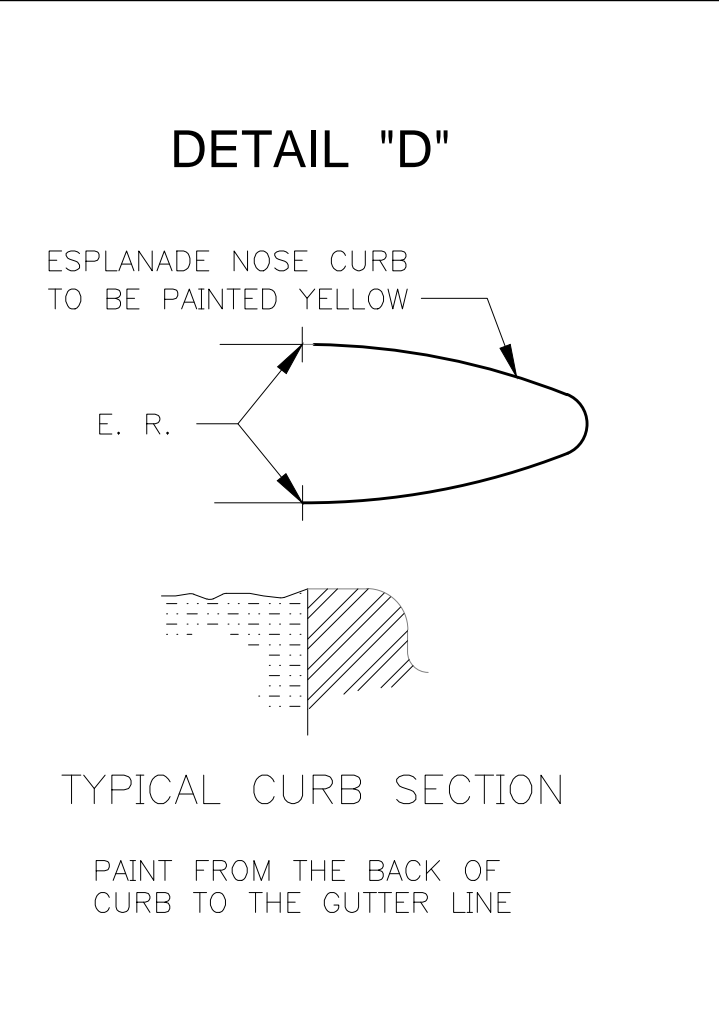
ESPLANADE	*R1	*R2
<8'	N/A	W/2
8'-38'	90'	W/5
>38'	N/A	15'



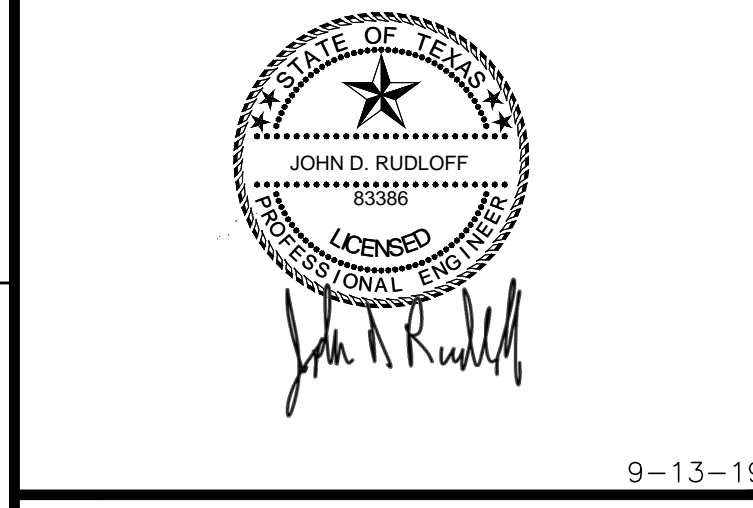
PAVEMENT MARKER LEGEND

SYMBOL	DESCRIPTION
▷◻◁	TWO SIDED REFLECTORIZED RAISED PAVEMENT MARKER
◻◁	ONEE SIDED REFLECTORIZED PAVEMENT MARKER
○	NON-REFLECTIVE 4" DIA. RAISED TRAFFIC BUTTON

- NOTES:**
1. ALL STRIPING & MARKERS SHALL CONFORM WITH THE TEXAS MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES FOR STREETS AND HIGHWAYS.
 2. ALL TRAFFIC BUTTONS AND MARKERS SHALL BE INSTALLED ADJACENT TO STRIPES (APPROX. 2").
 3. LEFT TURN STORAGE BAYS SHALL BE A MIN. OF 100' AT MINOR STREETS AND A MIN. OF 150' AT MAJOR STREETS.
 4. REPEAT ARROWS AT APPROX. 1000' INTERVALS WITHIN TWO-WAY LEFT TURN SECTION.
 5. WITHIN A TANGENT SECTION THE TYPE I-C PAVEMENT MARKERS CAN BE PLACED AT 40' C-C ON ROADWAYS WITHOUT CURB AND GUTTERS.

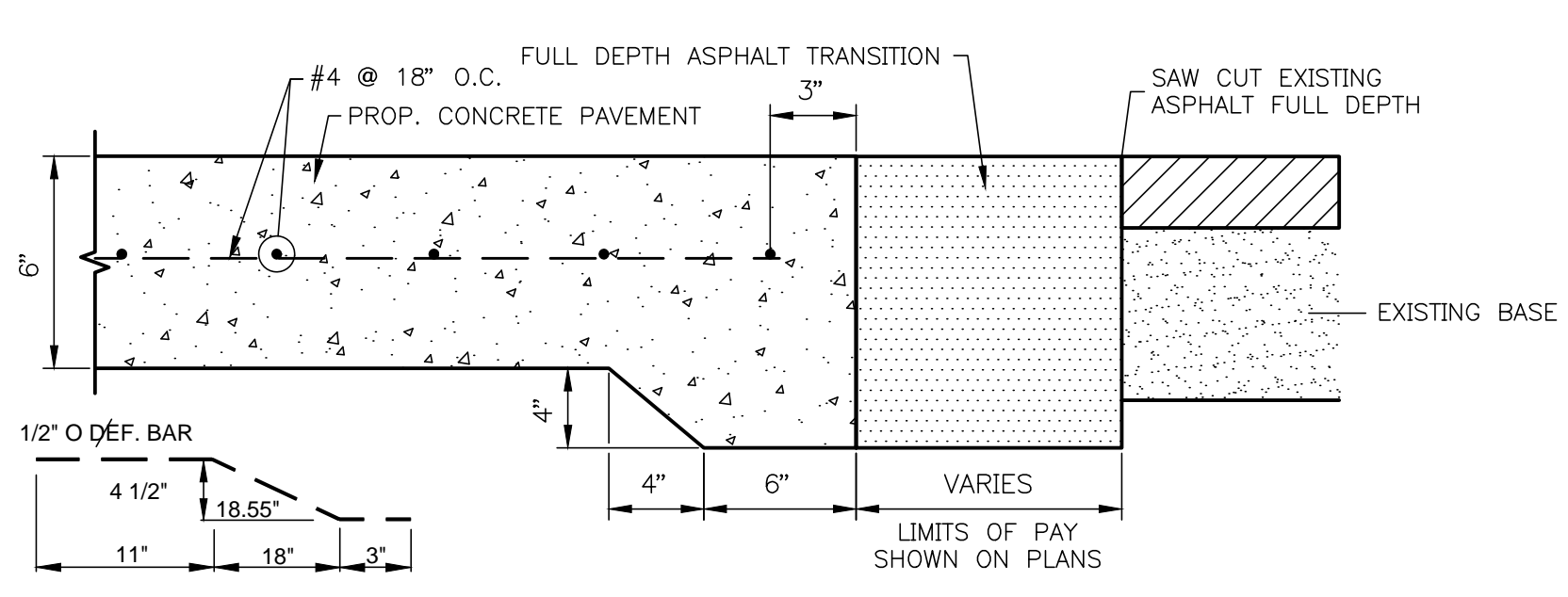


MK.	DESCRIPTION	DATE	DWN.	CHK.



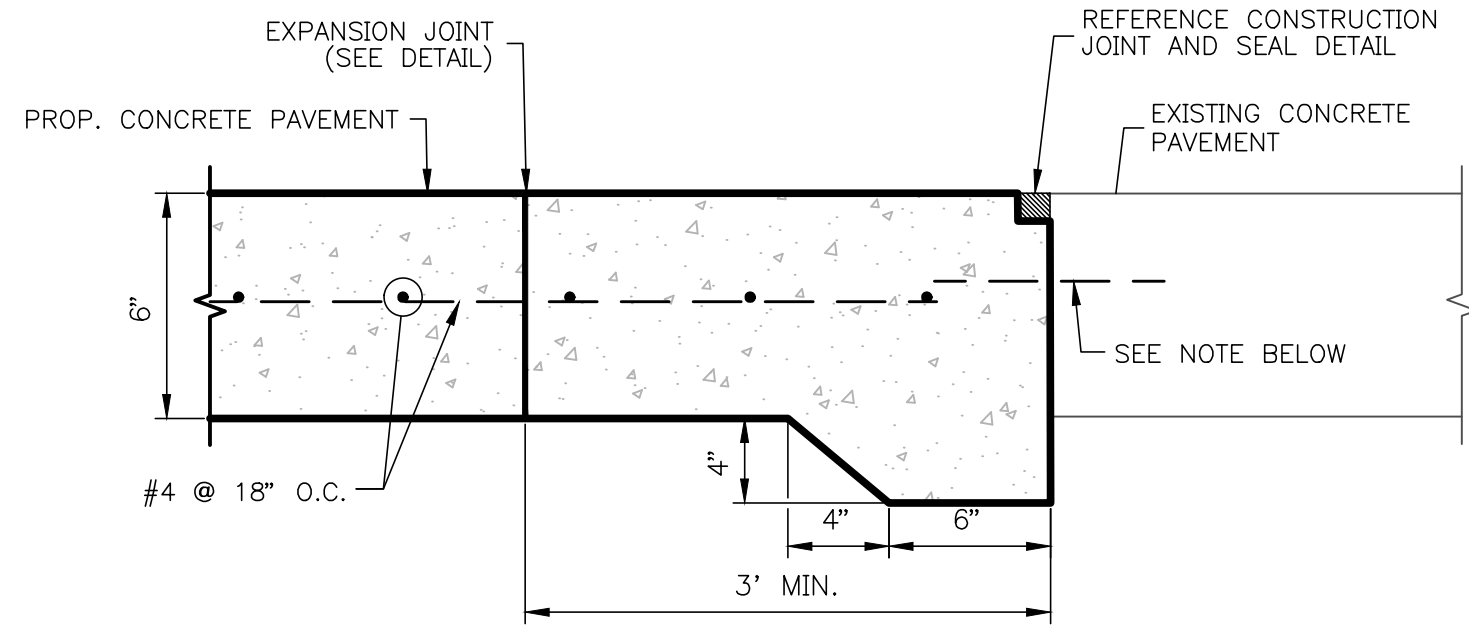
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Galveston County, Texas
 Texas Avenue Reconstruction
 Striping Details
 Job No.: 18-015 Scale: N/A SHEET
 Date: September, 2019 HORZ: N/A 36
 Dwn By: D. Fattig VERT: N/A OF 52
 Chkd By: J. Rudloff



CONCRETE PAVING HEADER AT ASPHALT PAVING

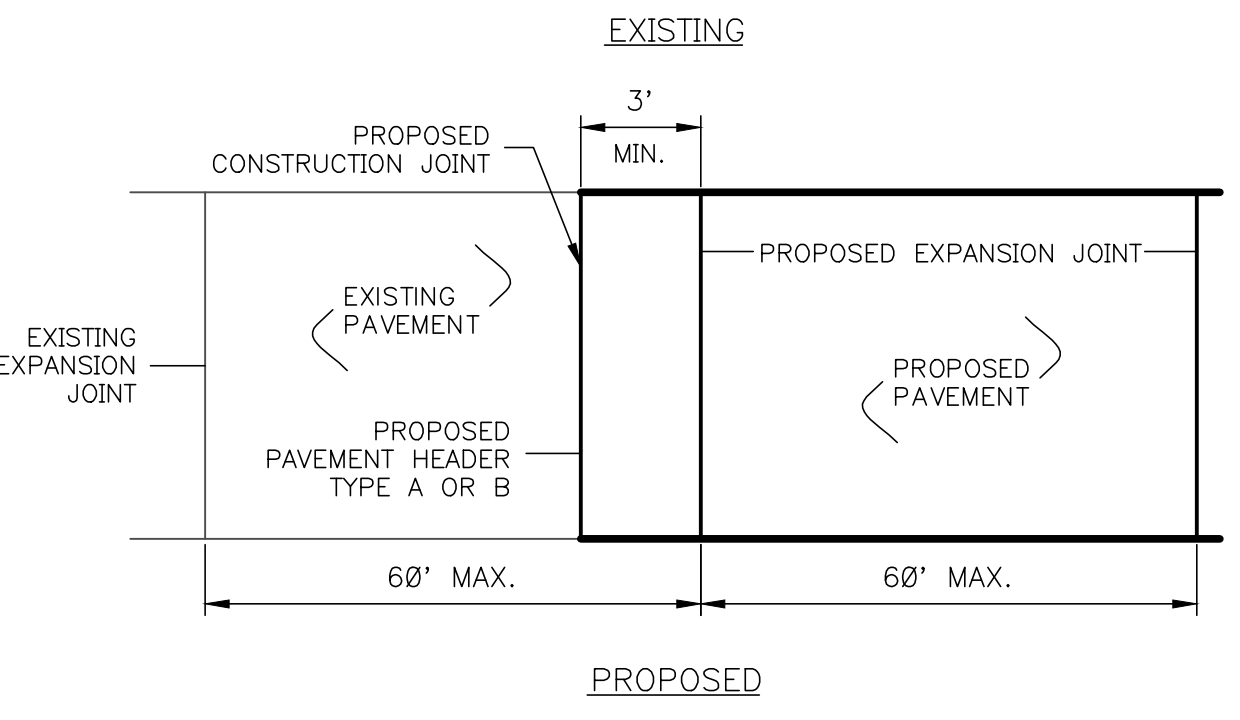
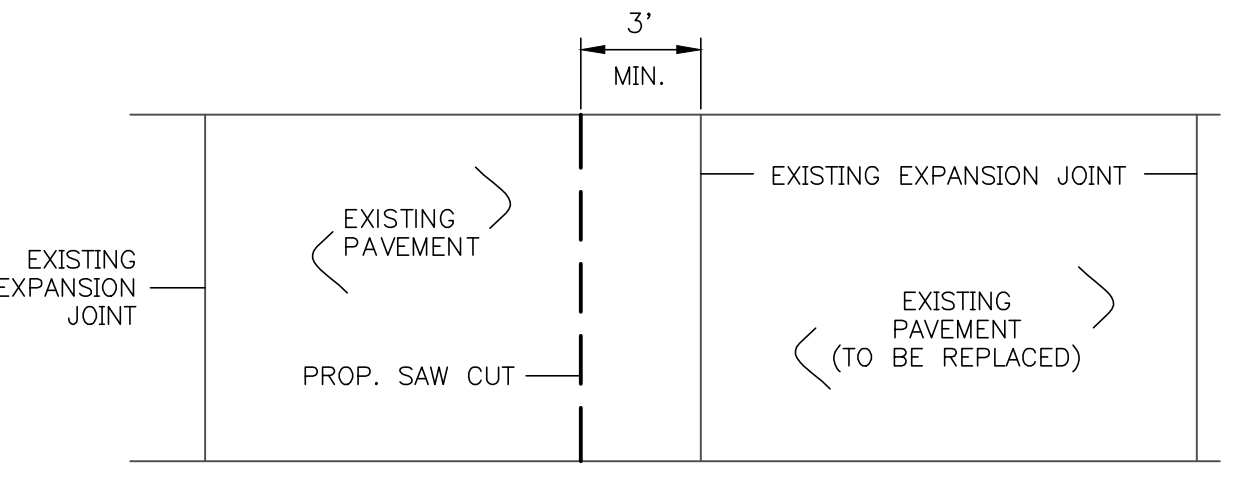
NOT TO SCALE



CONCRETE PAVING HEADER AT EXISTING CONCRETE PAVING

NOT TO SCALE

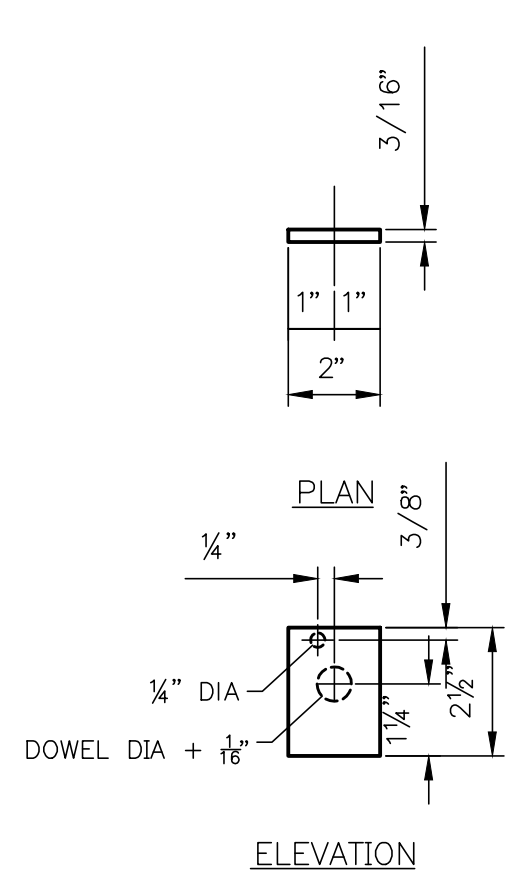
NOTES:
PROVIDE 3/4" DIAMETER SMOOTH STEEL BAR, 20" LONG ON 12" CENTERS. DRILL AND EPOXY DOWEL INTO EXISTING PAVEMENT WITH "PO ROC" OR EQUAL.



PAVEMENT JOINT LOCATION DETAIL WHERE PROPOSED PAVEMENT MEETS EXISTING

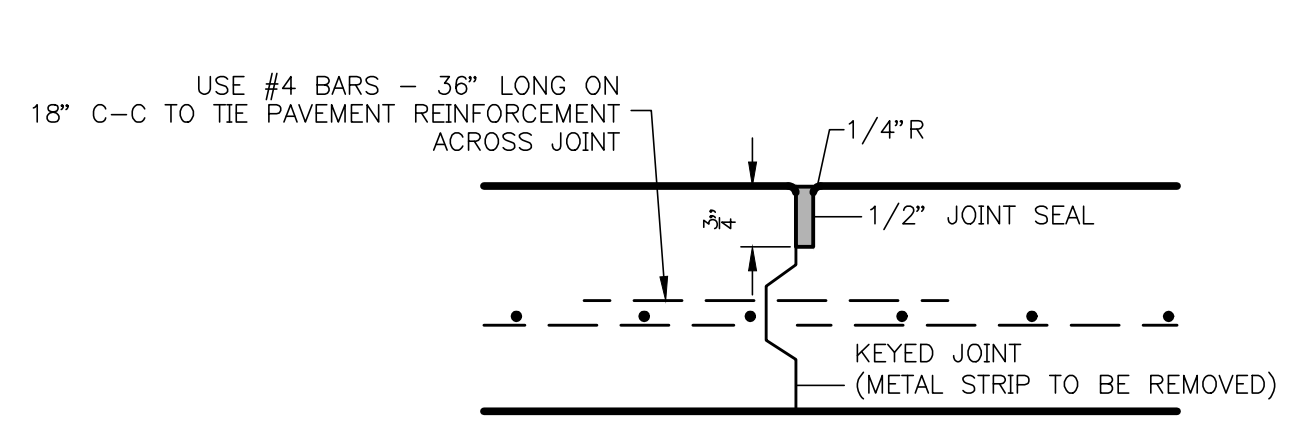
NOT TO SCALE

- GENERAL NOTES:
- ALL REINFORCING STEEL SHALL CONFORM TO A.S.T.M. DESIGNATION A-615, GRADE 60.
 - THE LOCATION OF EXPANSION JOINTS MAY BE REQUIRED TO SUIT THE PROPOSED METHODS OF THE CONTRACTOR. THE MAXIMUM WIDTH BETWEEN TRANSVERSE EXPANSION JOINTS SHALL NOT EXCEED 60'-0".
 - CONTROL JOINTS DEEP SHALL BE SAW CUT A DEPTH OF ONE QUARTER OF PAVEMENT THICKNESS PLUS 1/2 INCH AND FILLED WITH JOINT SEALANT @ 20' MAXIMUM SPACING BETWEEN CONTROL JOINTS.



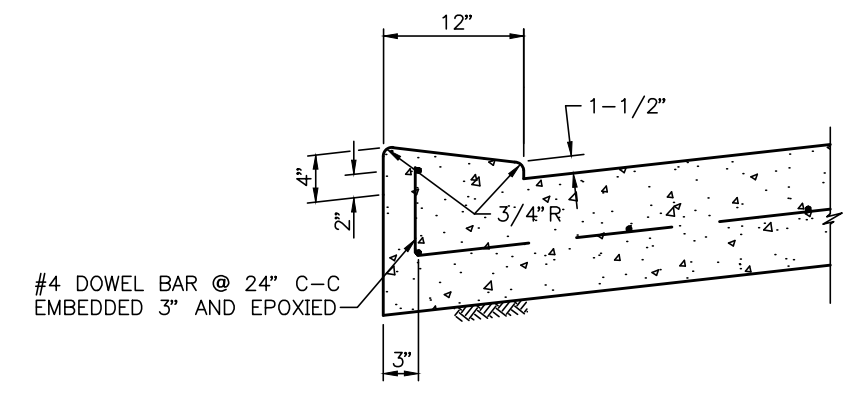
JOINT PLATE DETAIL

NOT TO SCALE



CONSTRUCTION JOINT AND SEAL DETAIL

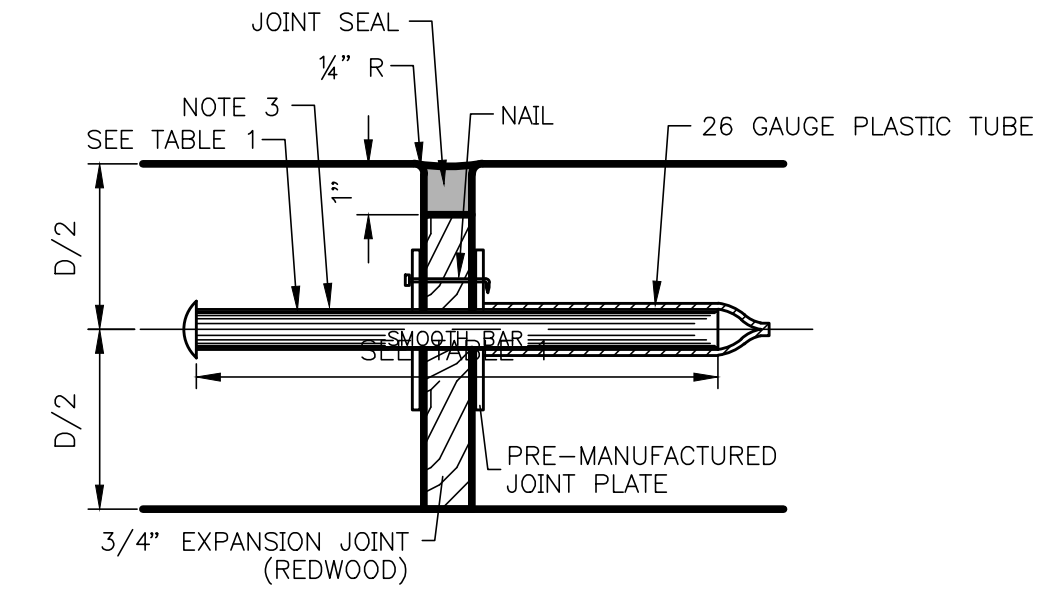
NOT TO SCALE



4"x12" LAYDOWN CURB

NOT TO SCALE

- NOTES:
- STEEL TO MEET ASTM STANDARD SPECIFICATIONS FOR CONCRETE REINFORCING BARS. UNITS TO BE SPACED ON 12" CENTERS.
 - EXPANSION JOINT TO BE PLACED AT THE END OF EACH CURB RADIUS AND SPACED AT A MAXIMUM DISTANCE OF 60 FEET.
 - CENTER DOWEL HORIZONTALLY ON JOINT.
 - CENTER DOWEL VERTICALLY IN CONCRETE BASE. EXTEND THICKENED CONCRETE AS NEEDED TO MAINTAIN 3" MIN. COVER.



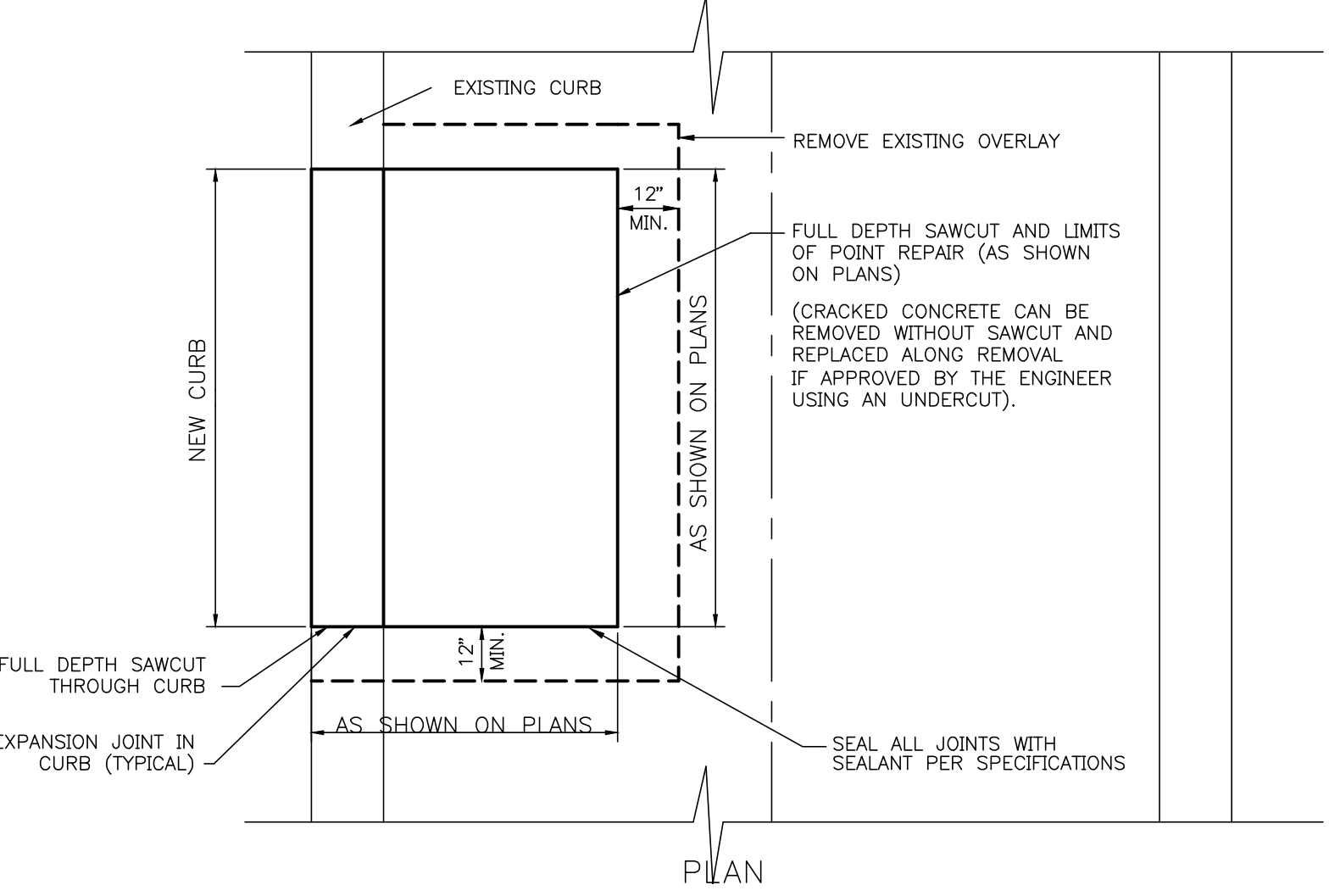
SECTION DOWEL TYPE EXPANSION JOINT

TABLE 1

PAVEMENT THICKNESS (IN)	DOWEL SIZES AND SPACINGS		
	DIAMETER (IN)	LENGTH (IN)	SPACING (IN)
6	3/4"	18	12
7	1"	18	12
8	1 1/4"	18	12

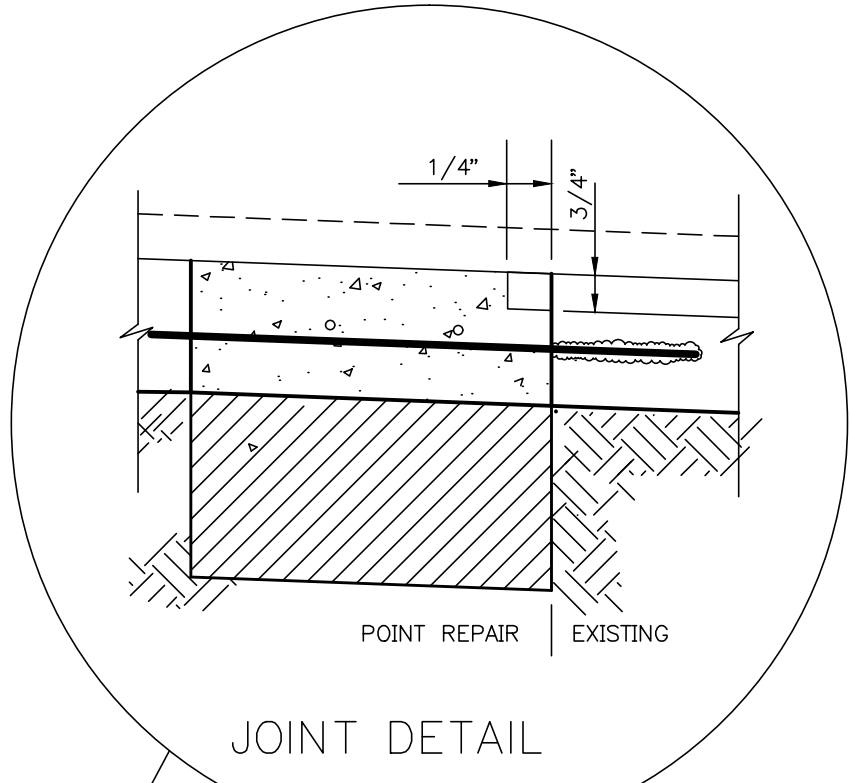
EXPANSION AND CONSTRUCTION JOINT DETAILS

NOT TO SCALE

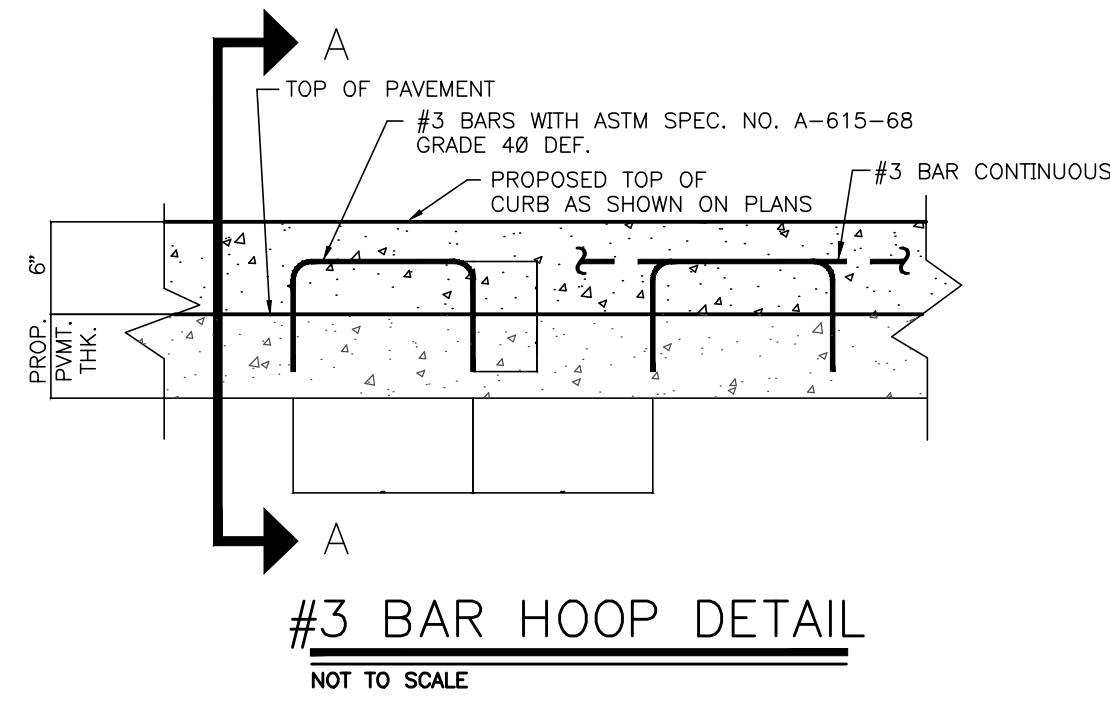


TYPICAL POINT REPAIR DETAIL FOR CONCRETE STREETS ON CEMENT STABILIZED SAND SUBGRADE

NOT TO SCALE

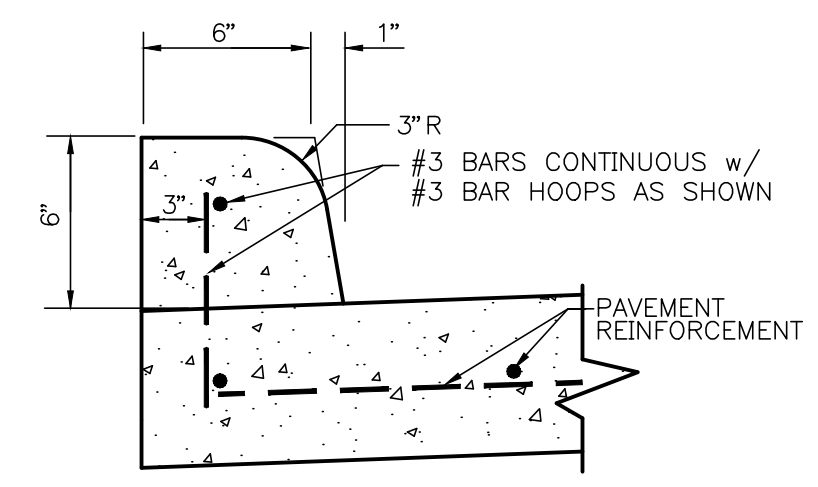


JOINT DETAIL



#3 BAR HOOP DETAIL

NOT TO SCALE

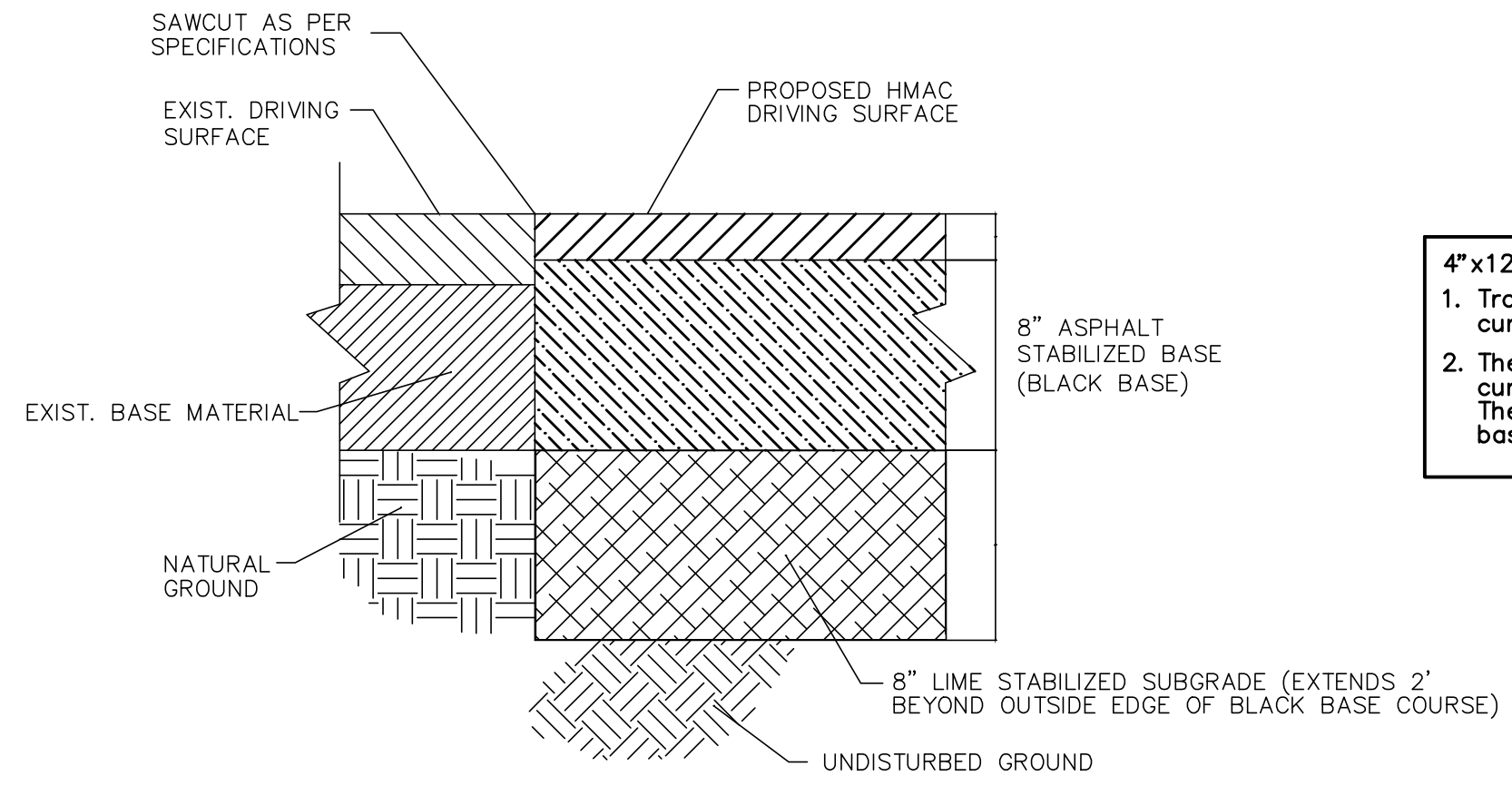


SECTION A-A

NOT TO SCALE

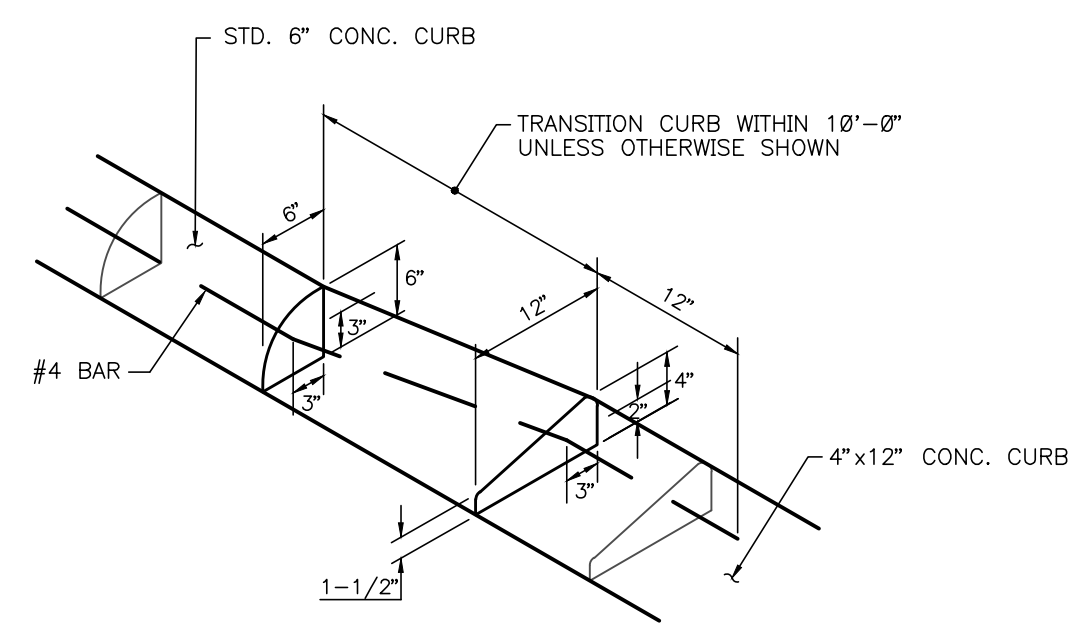
CONCRETE CURB NEW CONSTRUCTION

NOT TO SCALE



FULL DEPTH ASPHALT TRANSITION DETAIL

NOT TO SCALE



TYPICAL CURB TRANSITION

NOT TO SCALE

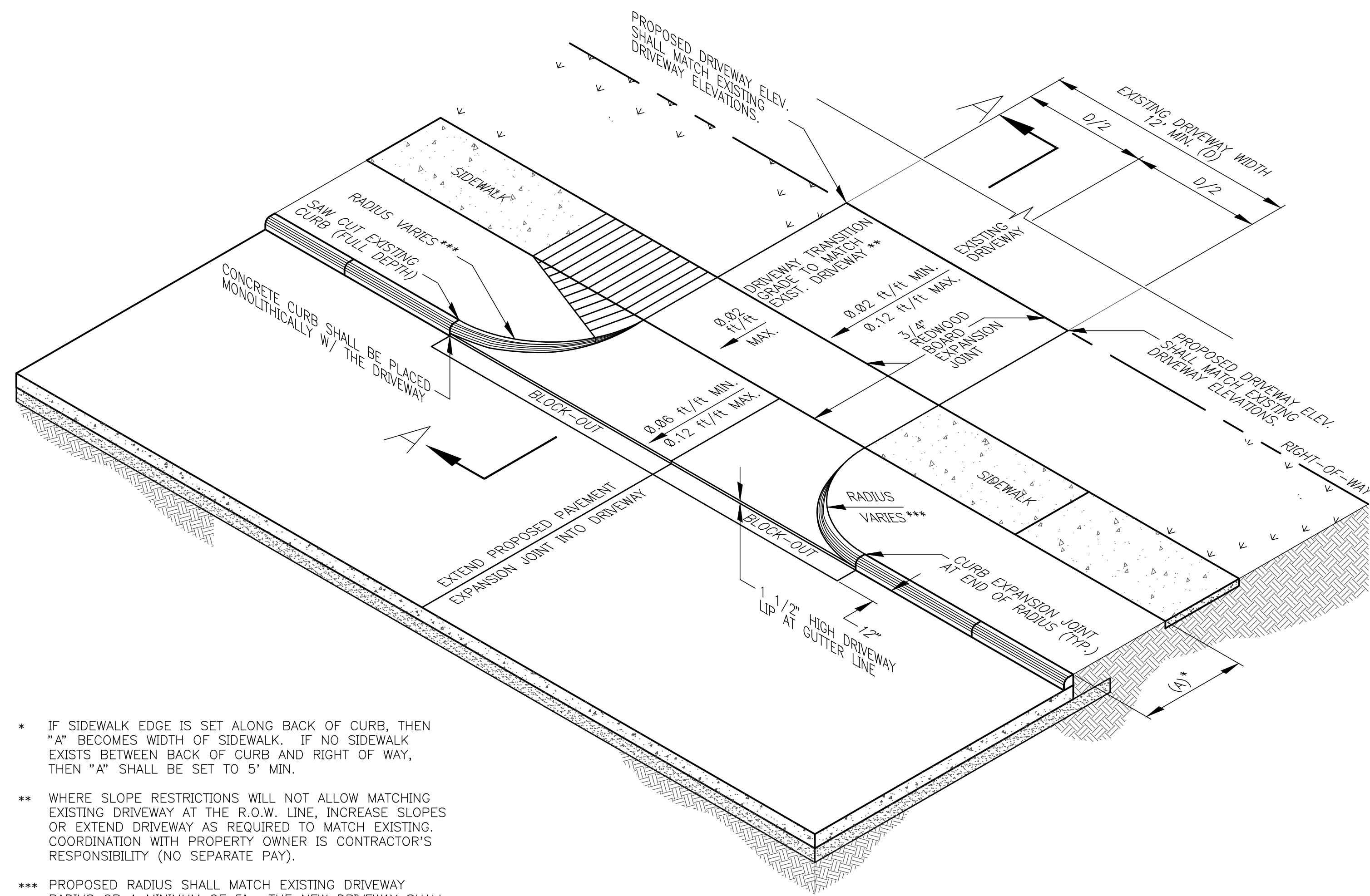
- 4"x12" LAYDOWN TRANSITION CURB NOTES:
- Transitions from 6-inch concrete curb to 4-inch x 12-inch concrete curb to be accomplished within 10 feet, unless otherwise shown.
 - The gutter elevation is calculated from the proposed top of curb line elevation shown in profile minus 6-inch concrete curb. The gutter elevation for laydown will also be calculated based on 6-inch concrete curb.

MK.	DESCRIPTION	DATE	DWN.	CHK.

STATE OF TEXAS
 JOHN D. RUDLOFF
 83386
 LICENSED PROFESSIONAL ENGINEER
 9-13-19

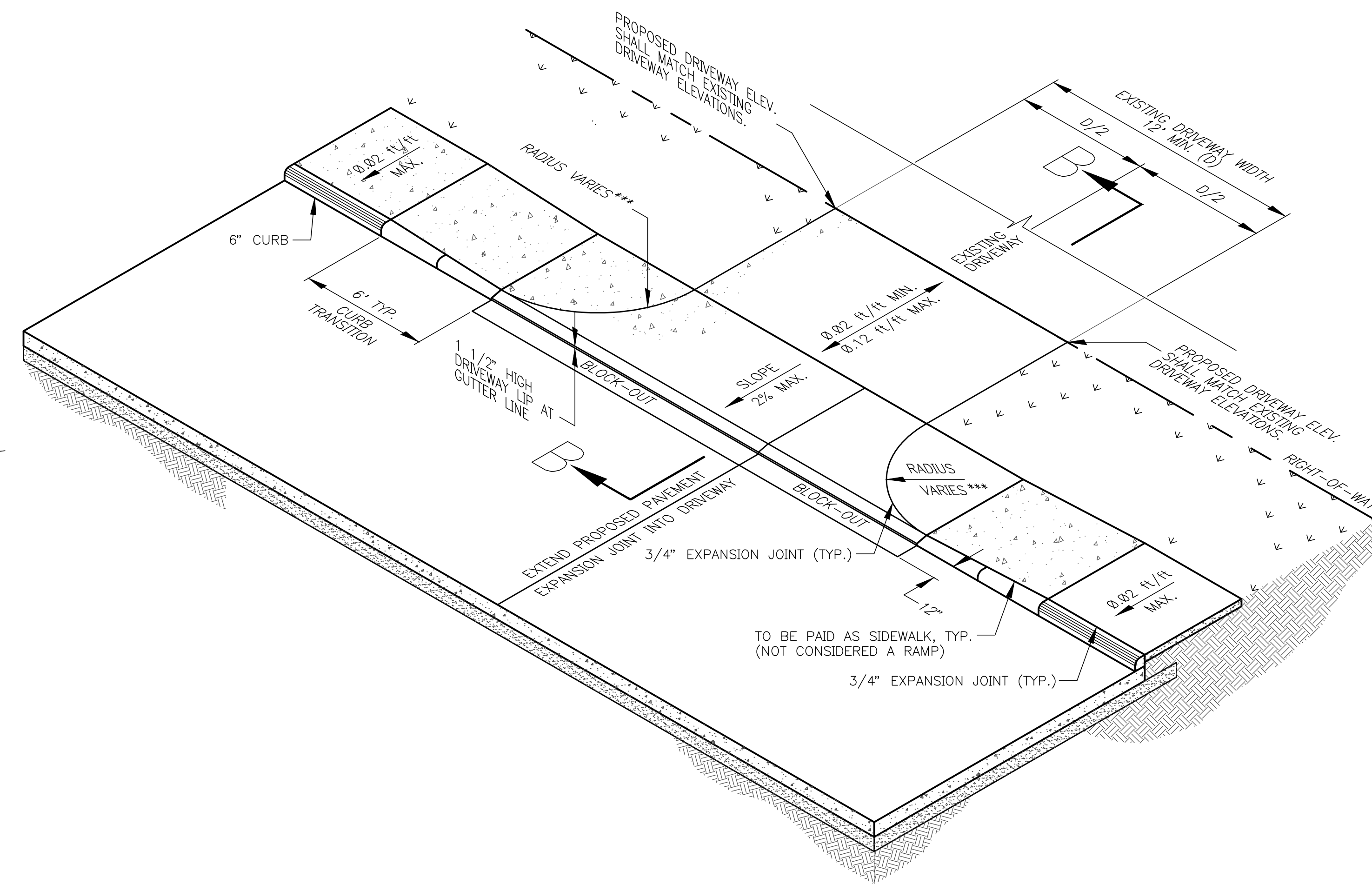
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Galveston County, Texas
 Texas Avenue Reconstruction

Pavement Details I
 Job No.: 18-015
 Date: September, 2019
 Dwn By: D. Fattig
 Chkd By: J. Rudloff
 Scale: HORZ: N/A
 VERT: N/A
 SHEET
37
 OF 52

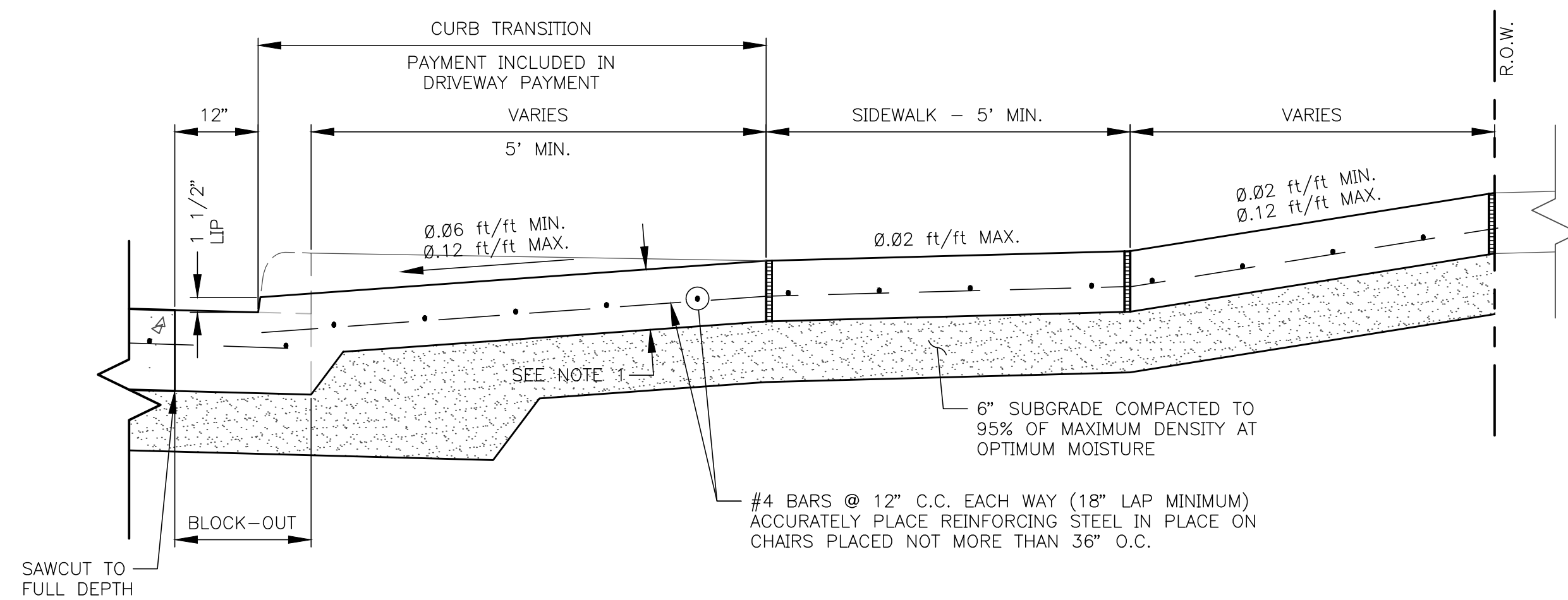


- * IF SIDEWALK EDGE IS SET ALONG BACK OF CURB, THEN "A" BECOMES WIDTH OF SIDEWALK. IF NO SIDEWALK EXISTS BETWEEN BACK OF CURB AND RIGHT OF WAY, THEN "A" SHALL BE SET TO 5' MIN.
- ** WHERE SLOPE RESTRICTIONS WILL NOT ALLOW MATCHING EXISTING DRIVEWAY AT THE R.O.W. LINE, INCREASE SLOPES OR EXTEND DRIVEWAY AS REQUIRED TO MATCH EXISTING. COORDINATION WITH PROPERTY OWNER IS CONTRACTOR'S RESPONSIBILITY (NO SEPARATE PAY).
- *** PROPOSED RADIUS SHALL MATCH EXISTING DRIVEWAY RADIUS OR A MINIMUM OF 5'. THE NEW DRIVEWAY SHALL BE EQUAL TO OR GREATER THAN THE SIZE OF THE EXISTING DRIVEWAY (MIN. 12' WIDTH).

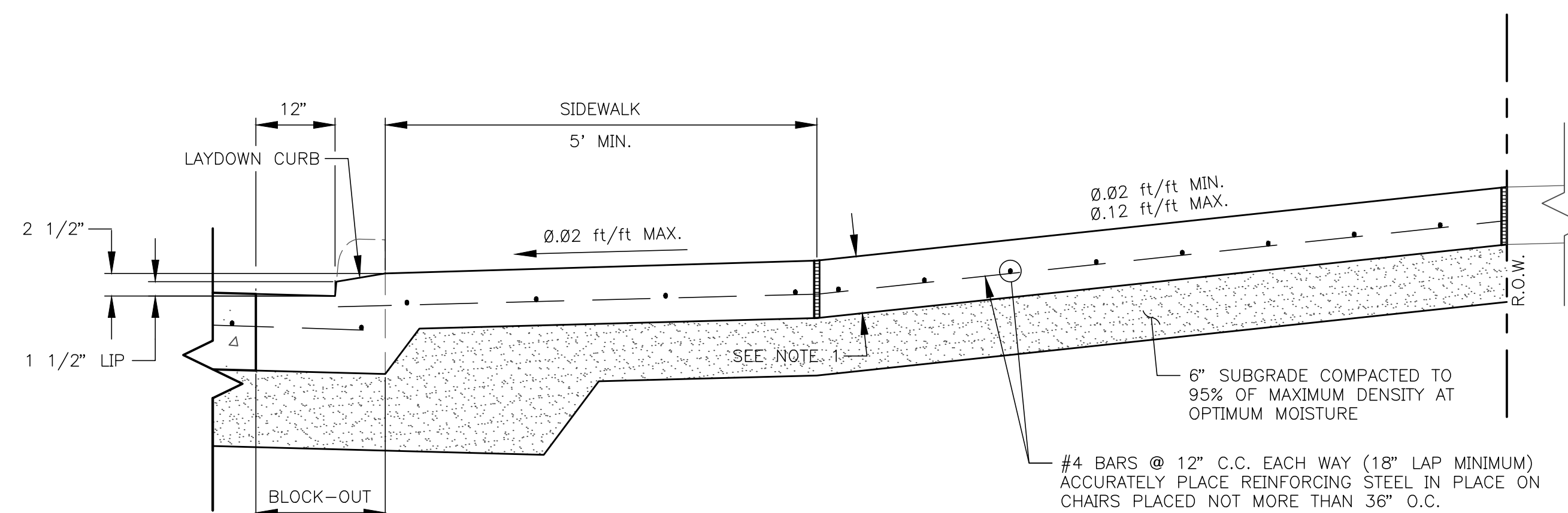
DRIVEWAY DETAIL
NOT TO SCALE



**DRIVEWAY DETAIL W/
SIDEWALK ADJACENT TO CURB**
NOT TO SCALE



SECTION A-A



SECTION B-B

MK.	DESCRIPTION	DATE	DWN.	CHK.

9-13-19

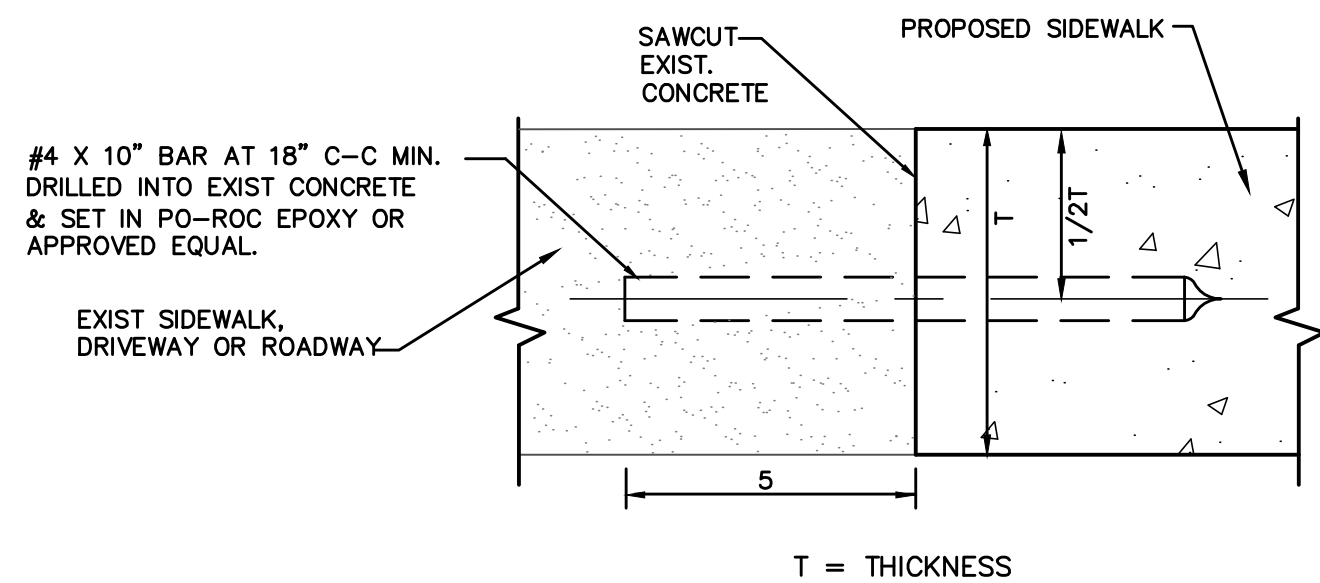
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Galveston County, Texas

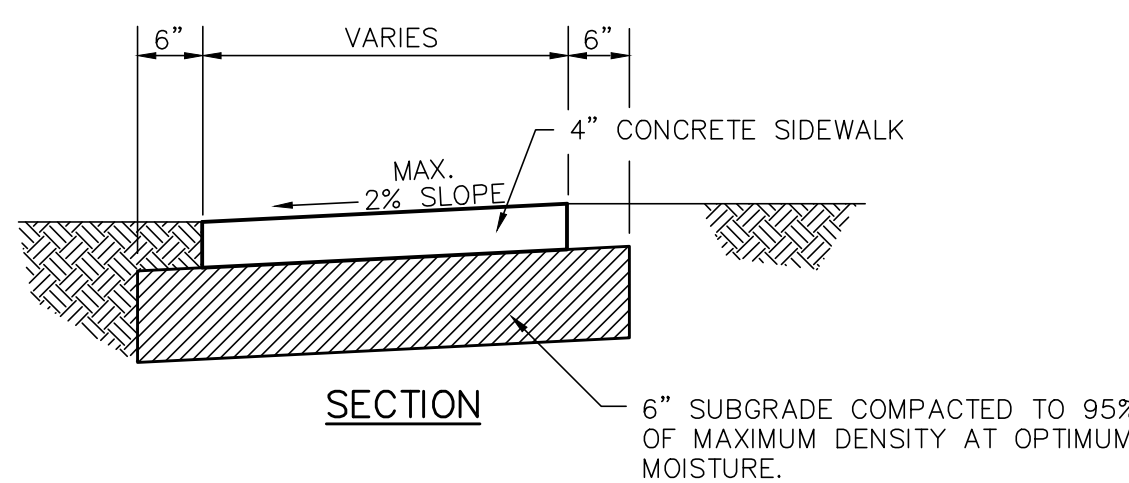
Texas Avenue Reconstruction

Paving Details II

Job No.: 18-015	Scale: N/A	SHEET
Date: September, 2019	HORZ: N/A	38
Dwn By: D. Fattig	VERT: N/A	OF 52
Chkd By: J. Rudloff		



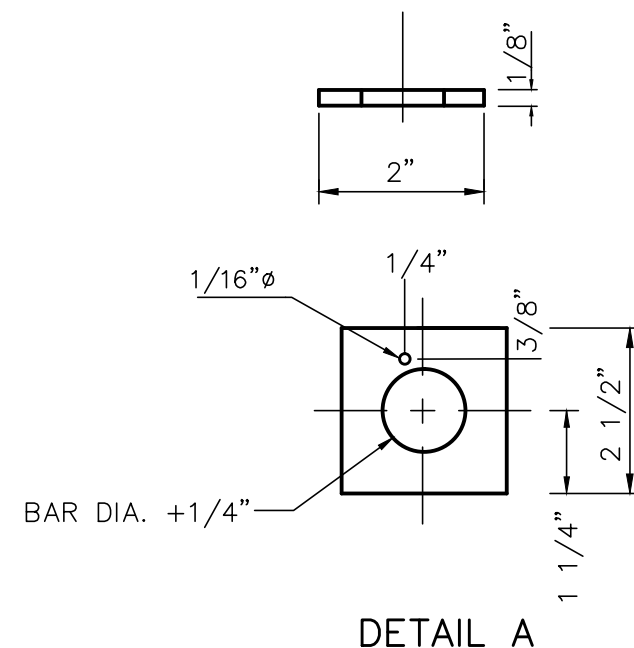
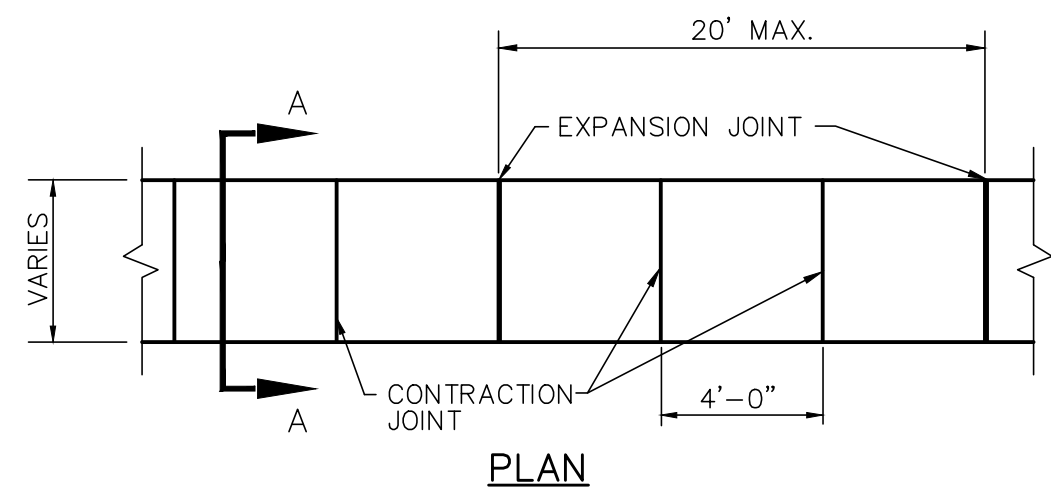
PROPOSED SIDEWALK AT EXISTING CONCRETE DETAIL
NOT TO SCALE



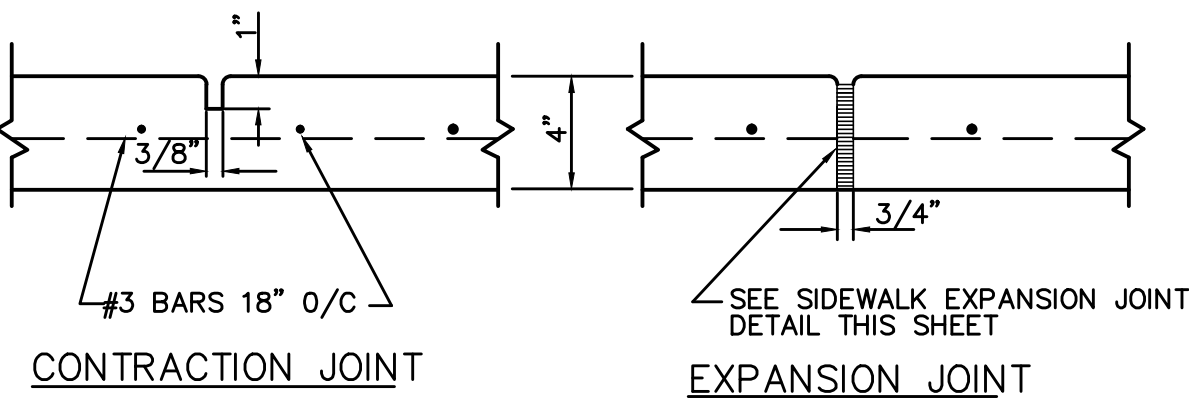
NOTES:

1. ALL EDGES SHALL BE ROUNDED WITH 1/4" RADIUS.
2. CONTRACTION JOINTS SHALL BE SPACED AT 4'-0" INTERVALS.
3. CONTRACTION JOINTS SHALL BE 1" DEEP AND EDGED WITH 1/4" RADIUS.
4. EXPANSION JOINTS SHALL BE SPACED AT 20 FT. INTERVALS. (MAXIMUM)
5. WHERE NEW SIDEWALK IS PLACED AGAINST EXISTING SIDEWALK, SAWCUT EXISTING SIDEWALK TO AN EVEN STRAIGHT LINE PRIOR TO INSTALLATION OF THE NEW SIDEWALK.

CONCRETE SIDEWALK DETAILS
NOT TO SCALE

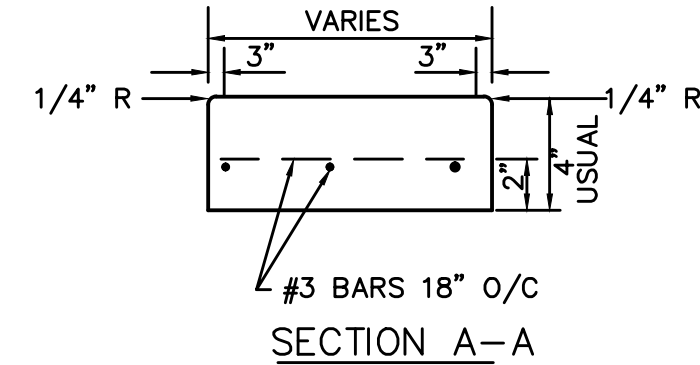


DETECTABLE WARNING PAVER

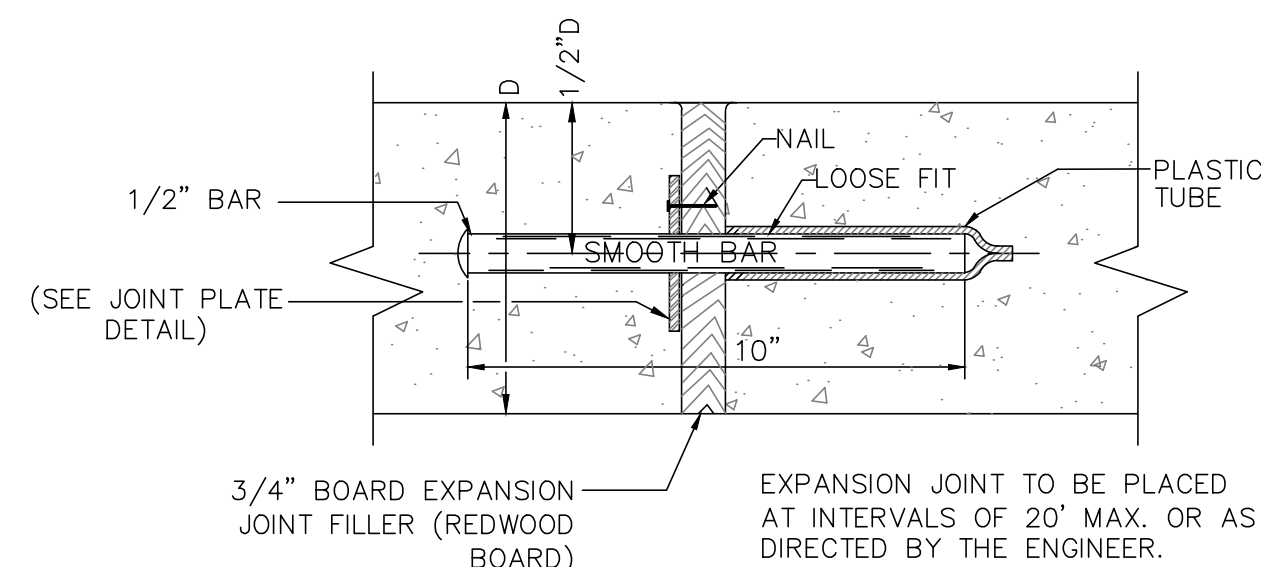


CONTRACTION JOINT

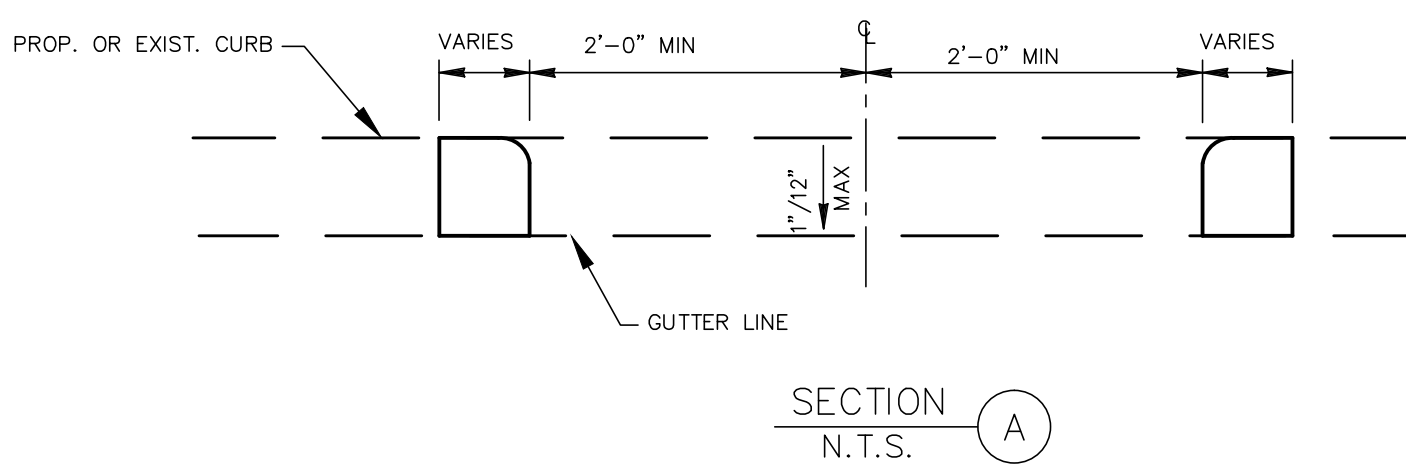
EXPANSION JOINT



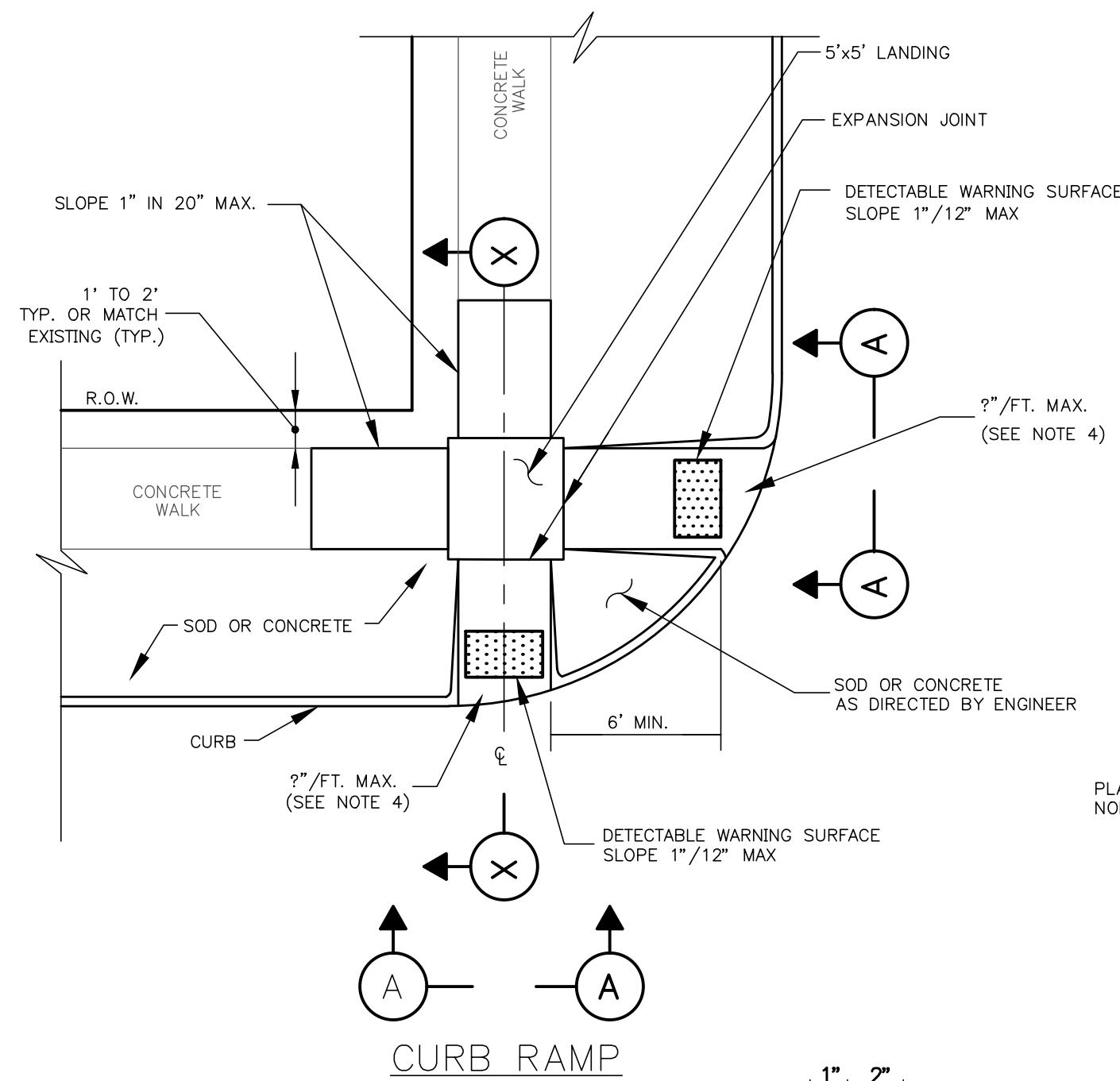
SECTION A-A



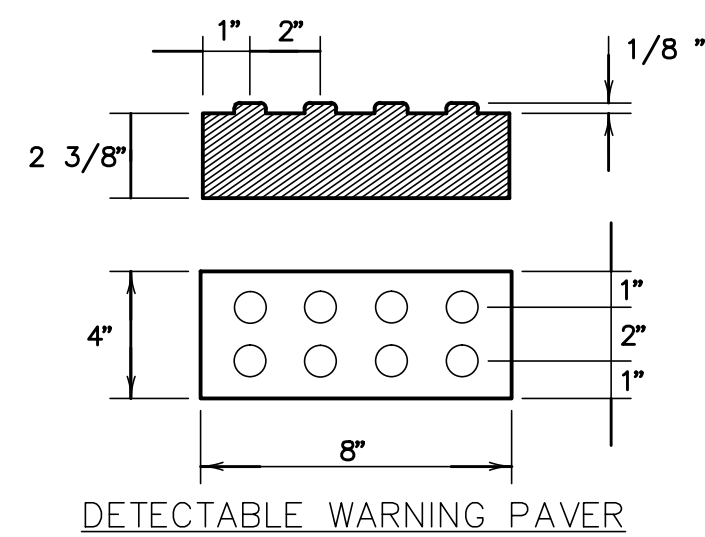
SIDEWALK EXPANSION JOINT DETAIL
NOT TO SCALE



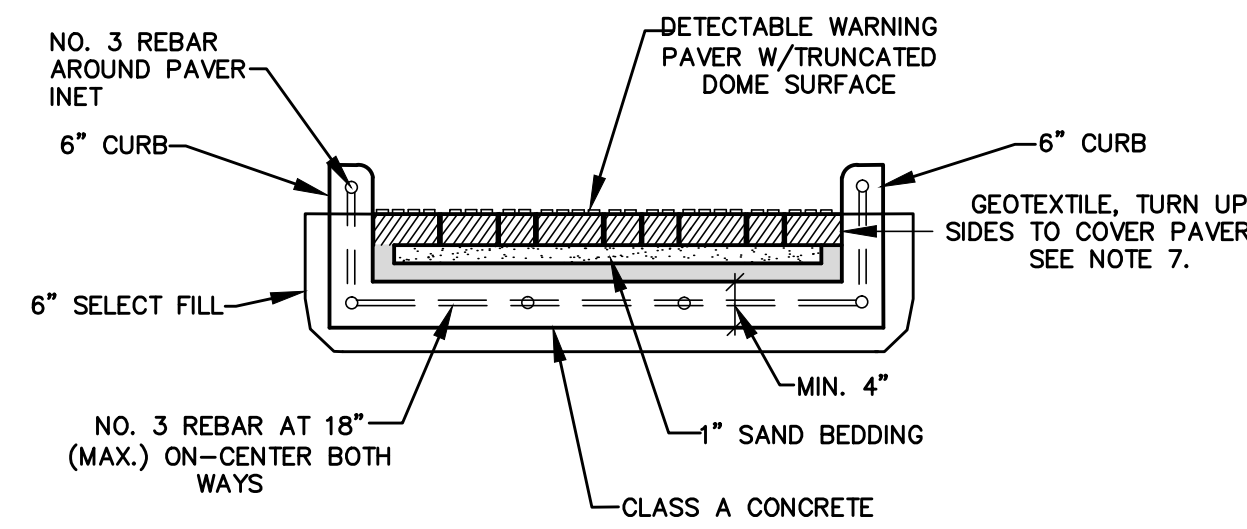
SECTION A
N.T.S.



CURB RAMP



TRUNCATED DOME PATTERN CURB RAMP



SECTION A-A

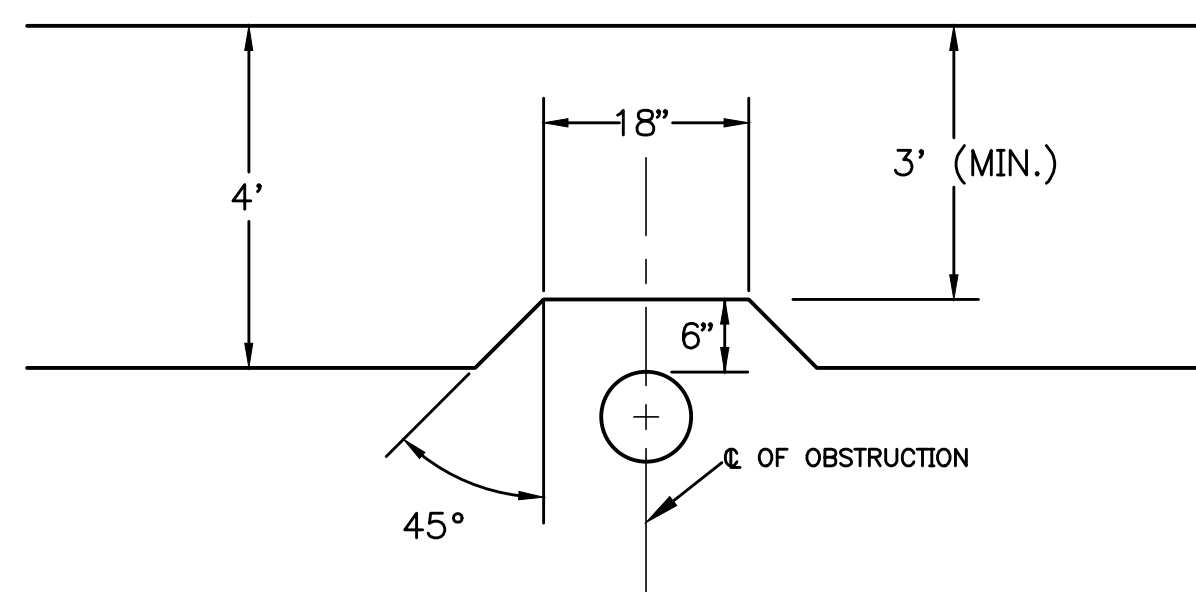
GENERAL NOTES (PAVERS):
FURNISH DETECTABLE WARNING PAVER UNITS MEETING ALL REQUIREMENTS OF ASTM C-936, C-33. LAY IN A TWO BY TWO UNIT BASKET WEAVE PATTERN OR AS DIRECTED.
LAY FULL-SIZE UNITS FIRST FOLLOWED BY CLOSURE UNITS CONSISTING OF AT LEAST 25 PERCENT OF A FULL UNIT. CUT DETECTABLE WARNING PAVER UNITS USING A POWER MASONRY SAW AND SHALL BE CUT FULL DEPTH.

DETECTABLE WARNING PAVER
NOT TO SCALE

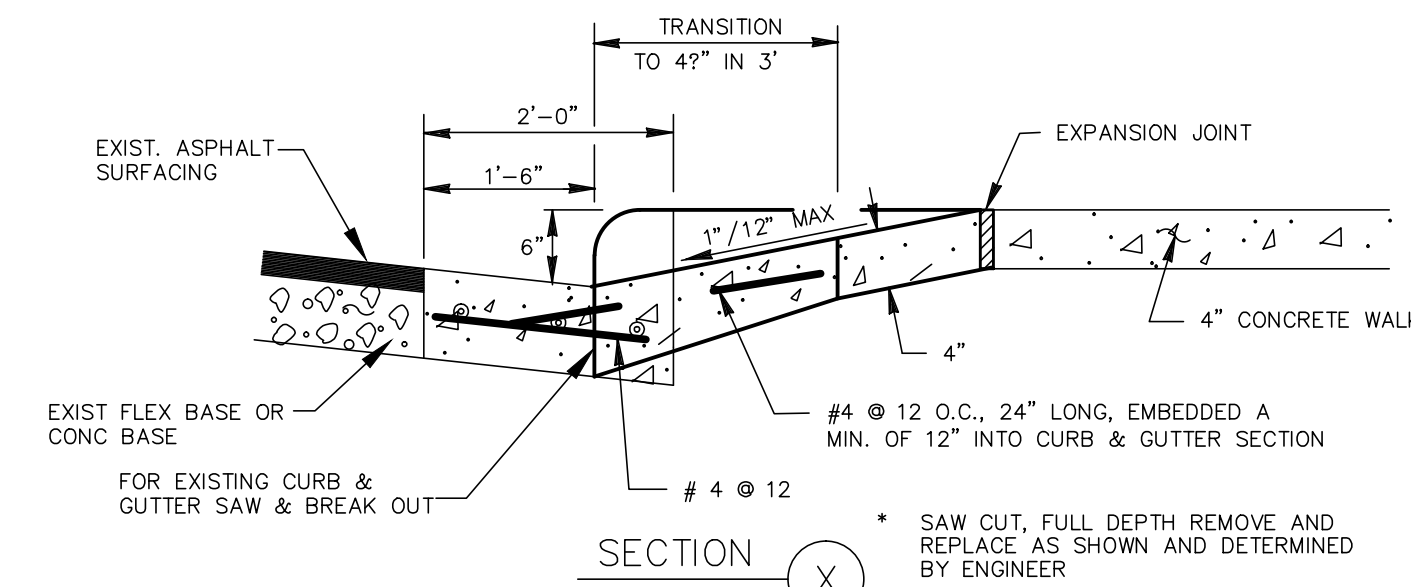
WHEEL CHAIR RAMP NOTES:

1. THE LOCATION OF A WHEELCHAIR RAMP MAY BE SHIFTED FROM THE PROPOSED LOCATION OF THE PLANS, BECAUSE OF UNFORESEEN EXISTING CONDITIONS AT THE TIME OF CONSTRUCTION. A CHANGE IN LOCATION WILL BE AS DIRECTED BY THE CITY OR ENGINEER.
2. ALL REINFORCING STEEL SHALL BE NEW BILLET STEEL AND MEET THE REQUIREMENTS OF ASTM DESIGNATION A-615. GRADE 60 DEFORMED BARS, FOR CONCRETE REINFORCEMENT.
3. MINIMUM CLEAR WIDTH OF WHEELCHAIR RAMP IS 3'-0".
4. IN AREAS WHERE CURB RAMP CONNECTS TO ROADWAY GUTTER WITHIN LIMITS OF A CURB ARC, A FLATTENED AREA (1/4" FT. MAX.) SHALL BE PROVIDED SUCH THAT THE APPROACH TO RAMP IS 90° TO THE RAMP TRAVEL DIRECTION. FLATTENED AREA SHALL BE SLOPED TOWARD GUTTER TO PROVIDE POSITIVE DRAINAGE.
5. CONTRACTOR SHALL ENSURE CONNECTION OF PROPOSED SIDEWALK TO EXISTING SIDEWALK IS EVEN. ANY CHANGE IN ELEVATION IN EXCESS OF 1/4" WILL REQUIRE REMOVAL AND REPLACEMENT OF PROPOSED SIDEWALK.
6. IN THE EVENT FIELD CONDITIONS PREVENT THE SIDEWALK TRANSITIONS FROM BEING CONSTRUCTED @ A 1:20 SLOPE OR LESS, CONTRACTOR SHALL INSTALL ADDITIONAL WHEELCHAIR RAMP. CONTRACTOR SHALL COORDINATE THE ADDITIONAL WHEELCHAIR RAMP LENGTH IN THE FIELD WITH THE OWNER'S REPRESENTATIVE.
7. ADDITIONAL INFORMATION ON WHEELCHAIR RAMP LOCATION, DESIGN VISIBILITY AND TEXTURE MAY BE FOUND IN THE CURRENT EDITION OF THE TEXAS ACCESSIBILITY STANDARDS (TAS) PREPARED AND ADMINISTERED BY THE TEXAS DEPARTMENT OF LICENSING AND REGULATION (TDLR).

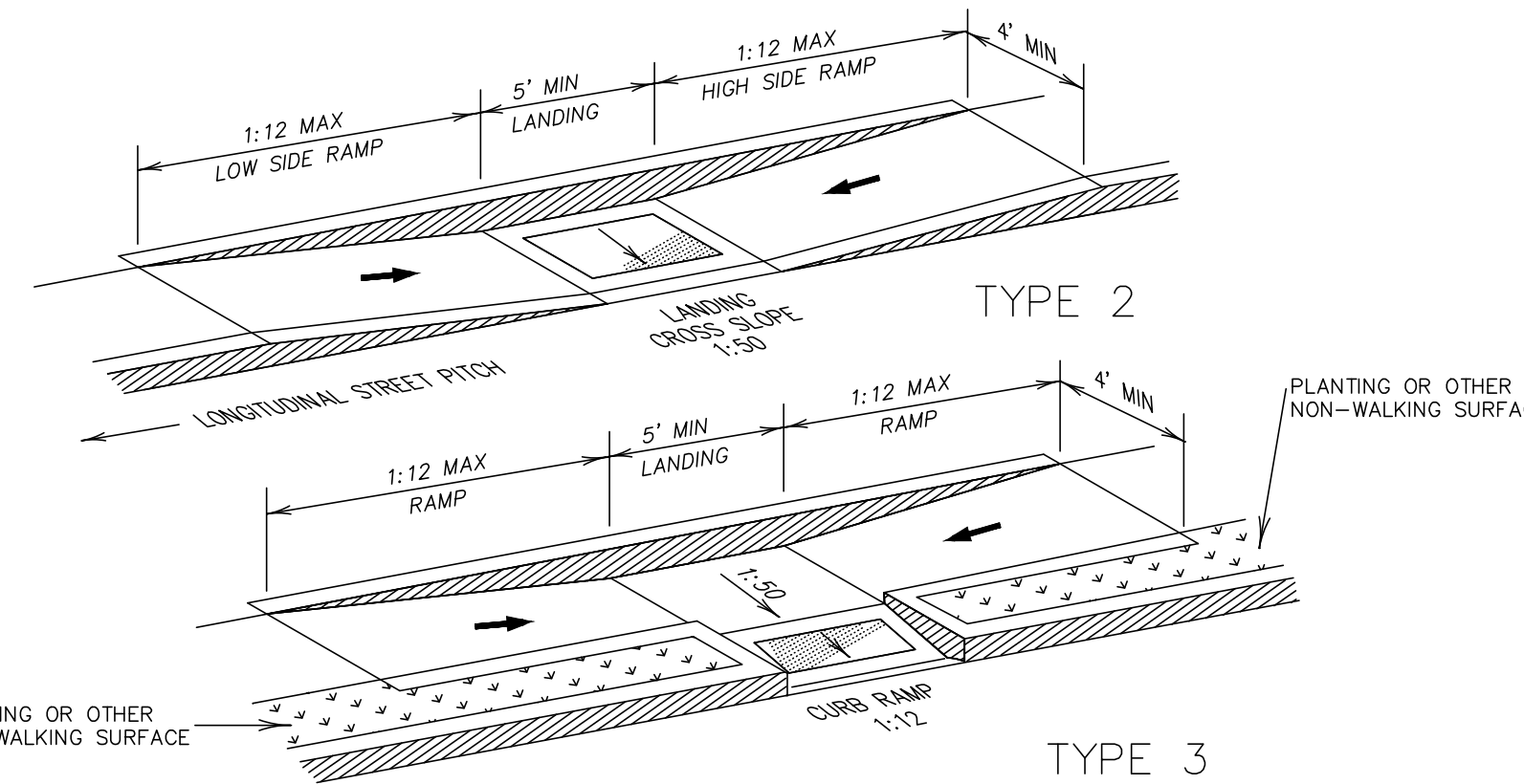
WHEELCHAIR RAMP DETAIL
NOT TO SCALE



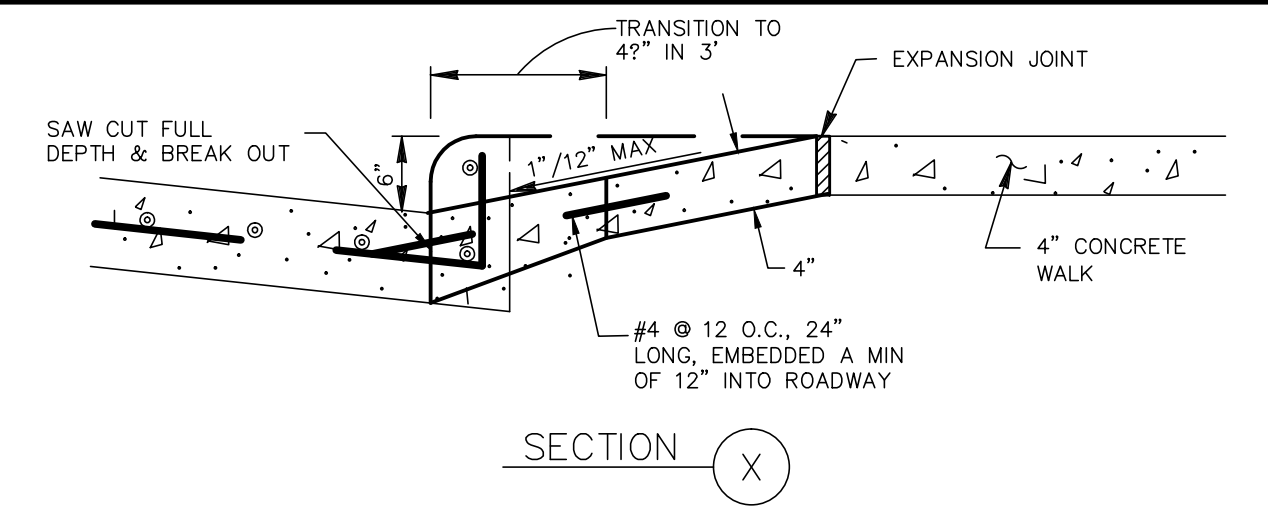
SIDEWALK AROUND OBSTRUCTION
NOT TO SCALE



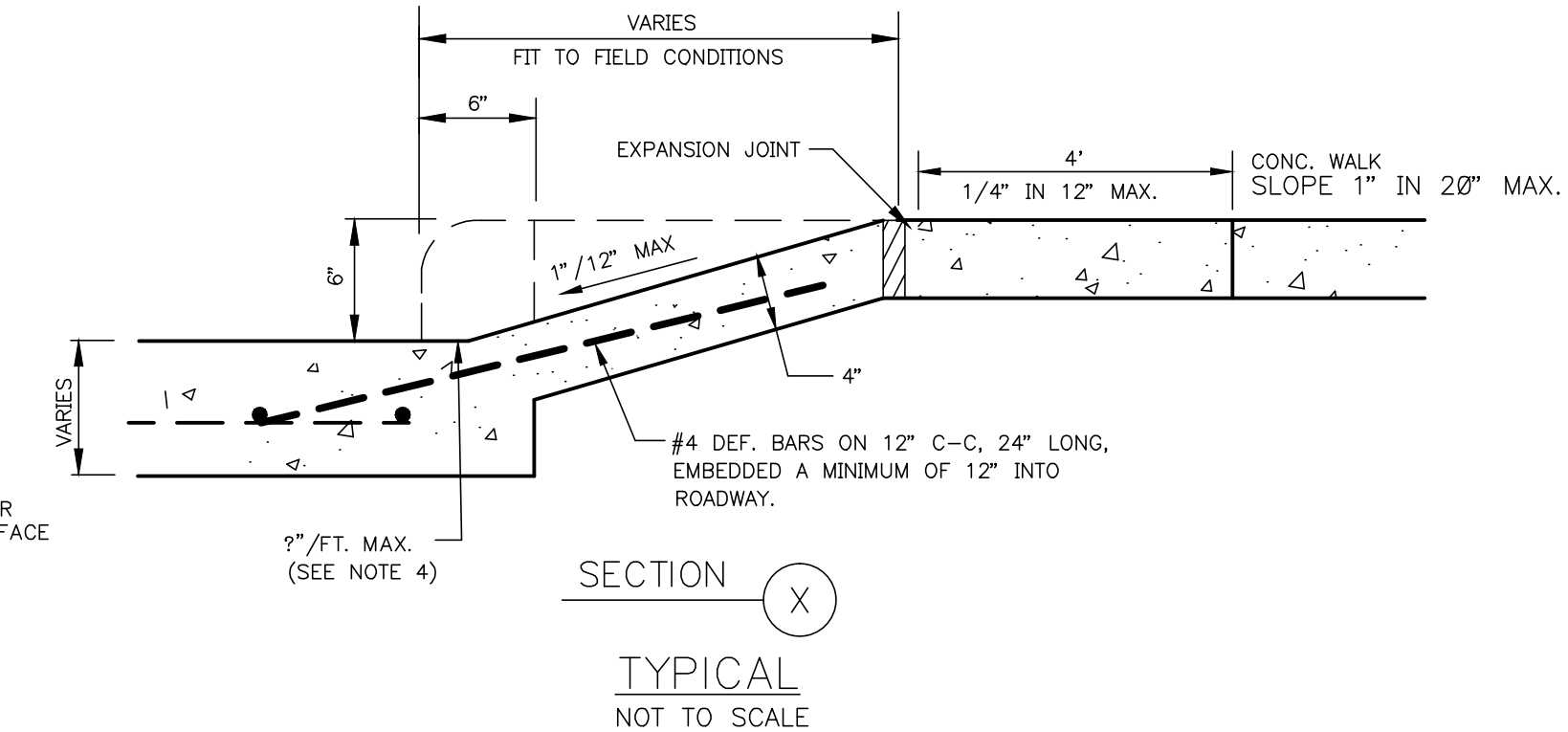
EXISTING CURB & GUTTER CONSTRUCTION
NOT TO SCALE



PARALLEL CURB RAMP



EXISTING CONCRETE PAVEMENT CONSTRUCTION
NOT TO SCALE

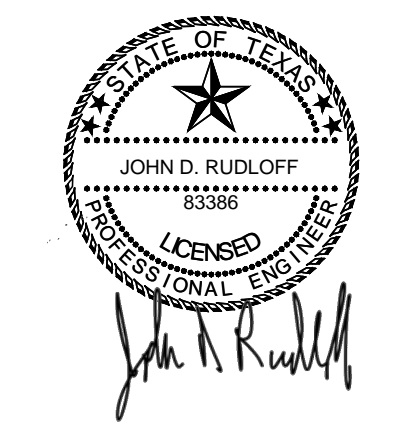


SECTION X
TYPICAL
NOT TO SCALE

NOTES FOR DETECTABLE WARNINGS:

1. CURB RAMP MUST CONTAIN A DETECTABLE WARNING SURFACE THAT CONSISTS OF RAISED TRUNCATED DOMES COMPLYING WITH SECTION 4.29 OF THE TEXAS ACCESSIBILITY STANDARDS (TAS). THE SURFACE MUST CONTRAST VISUALLY WITH ADJOINING SURFACES. THE CONTRACTOR SHALL COORDINATE WITH THE CITY TO OBTAIN APPROVAL OF THE COLOR PRIOR TO INSTALLING THE TRUNCATED DOME.
2. DETECTABLE WARNING SURFACES MUST BE SLIP RESISTANT AND NOT ALLOW WATER TO ACCUMULATE.
3. ALIGN TRUNCATED DOMES IN THE DIRECTION OF PEDESTRIAN TRAVEL WHEN ENTERING THE STREET.
4. SHADED AREAS ON THE CURB RAMP DETAILS INDICATE THE APPROXIMATE LOCATION FOR THE DETECTABLE WARNING SURFACE FOR THE CURB RAMP.
5. DETECTABLE WARNING SURFACES SHALL BE A MINIMUM OF 24" IN DEPTH IN THE DIRECTION OF PEDESTRIAN TRAVEL AND EXTEND THE FULL WIDTH OF THE RAMP OR LANDING WHERE THE PEDESTRIAN ACCESS ROUTE ENTERS THE STREET.
6. DETECTABLE WARNING SURFACE SHALL BE LOCATED SO THAT THE EDGE NEAREST THE CURB LINE IS A MINIMUM 6" AND A MAXIMUM 10" FROM THE EXTENSION OF THE FACE OF CURB. DETECTABLE WARNING SURFACES MAY BE CURVED ALONG THE CORNER RADIUS.
7. GEOTEXTILE SHALL BE INSTALLED AND CUT FLUSH WITH TOP OF PAVEMENT. ANY RAGGED EDGE EXPOSED AFTER PAVERS ARE IN PLACE, SHALL BE REMOVED BY HEAT.

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19



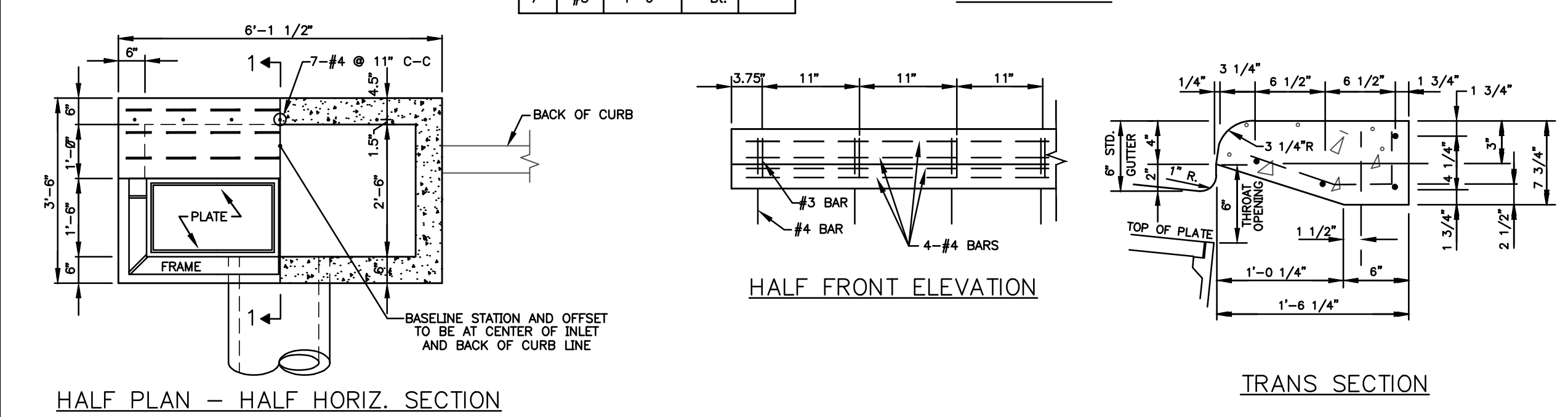
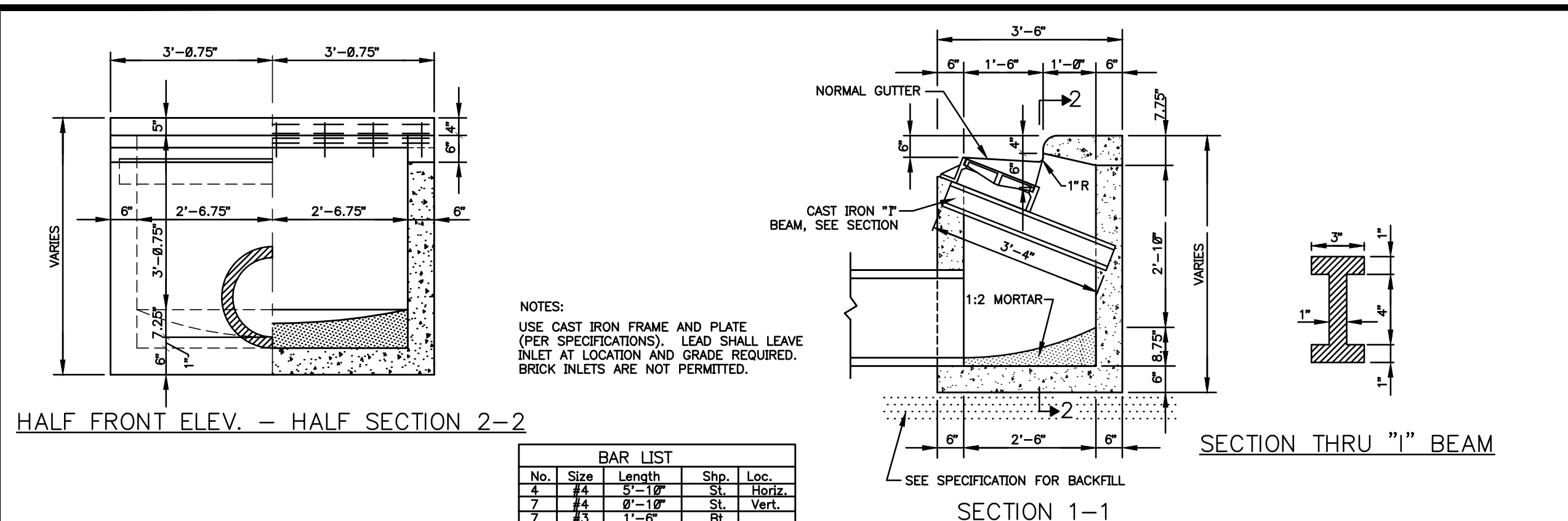
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Galveston County, Texas

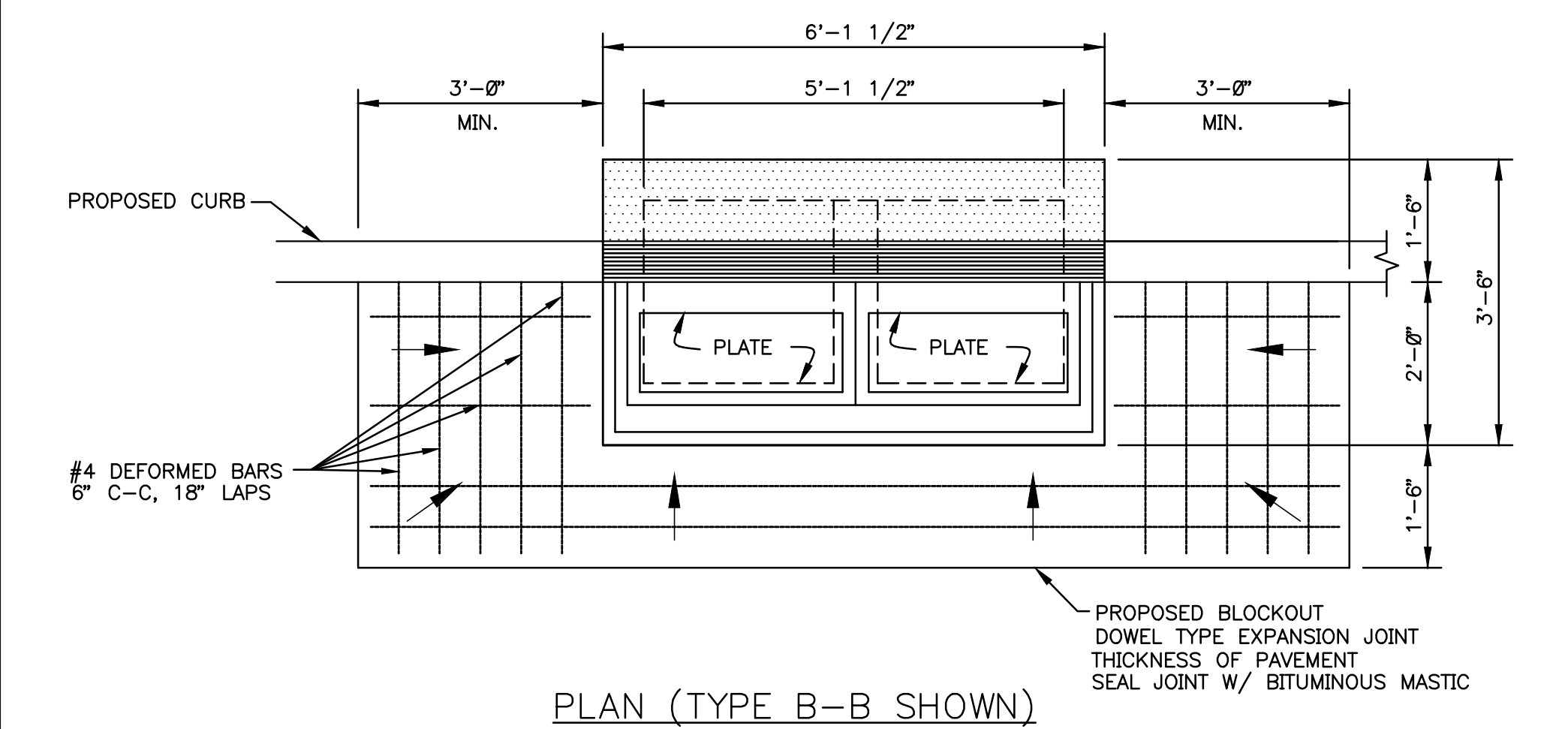
Texas Avenue Reconstruction

Paving Construction Details III

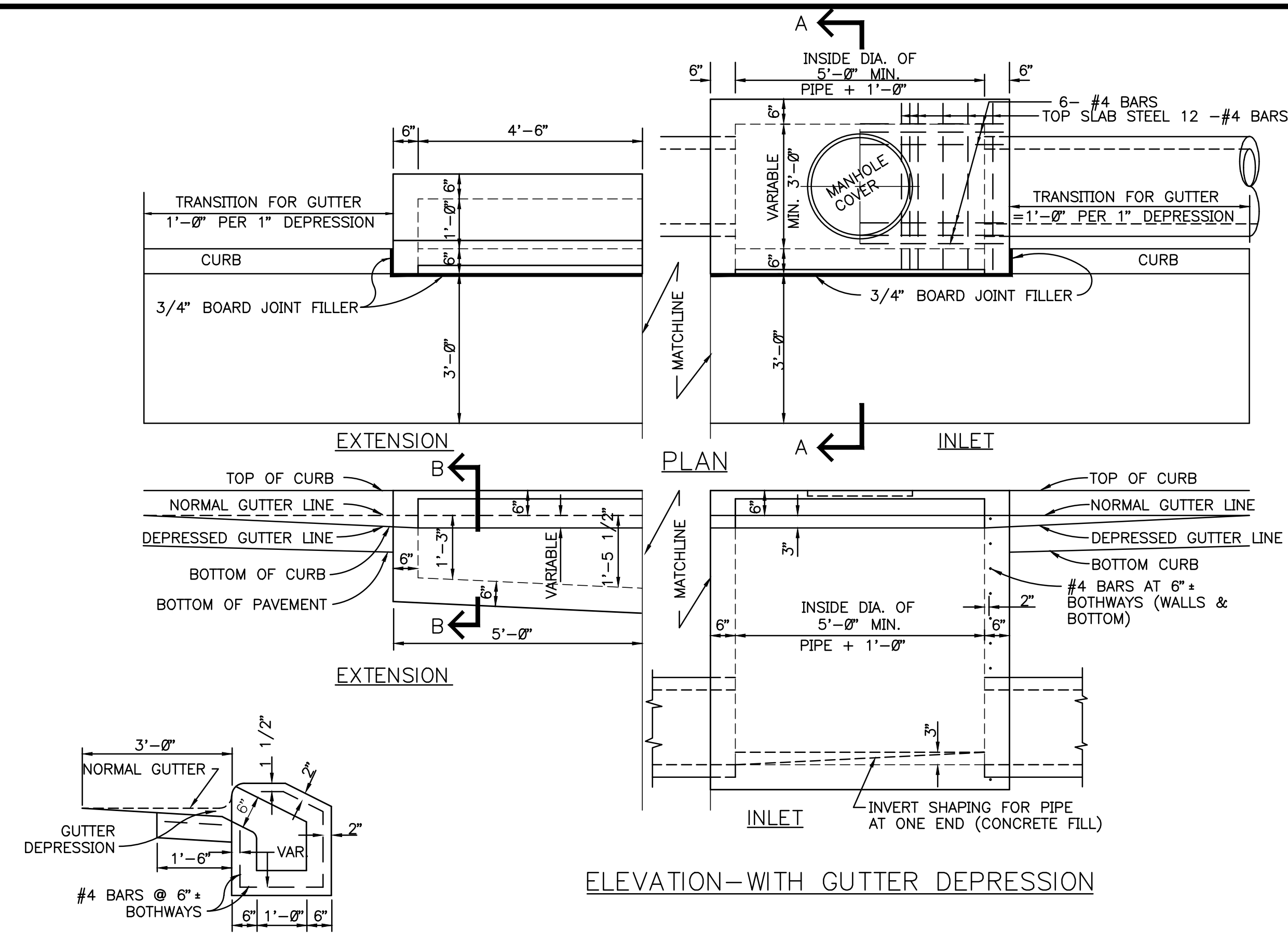
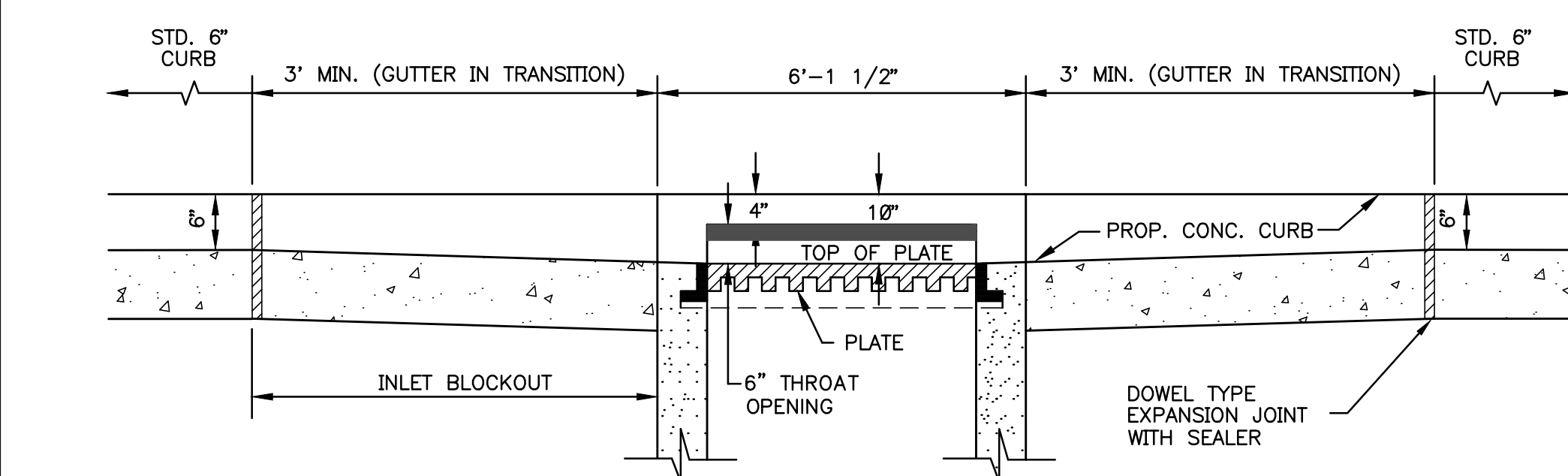
Job No.: 18-015	Scale: N/A	SHEET
Date: September, 2019	HORZ:	39
Dwn By: D. Fattig	VERT:	OF 52
Chk By: J Rudloff		



TYPE B-B' INLET
NOT TO SCALE



GUTTER DEPRESSIONS FOR INLETS
NOT TO SCALE



SECTION B-B

GENERAL NOTES:

All concrete shall be Class A. All exposed corners shall be chamfered 3/4". Pipes shall enter inlets as shown elsewhere on plans. Slope top of inlets as directed to match graded section.

All materials used in casting manhole covers and ladder rung shall conform to A.S.T.M. Specifications. Payment of curb inlets and extensions thereto as shown on the plans will be made at the unit prices bid for the "Inlets" and "Inlet Extensions".

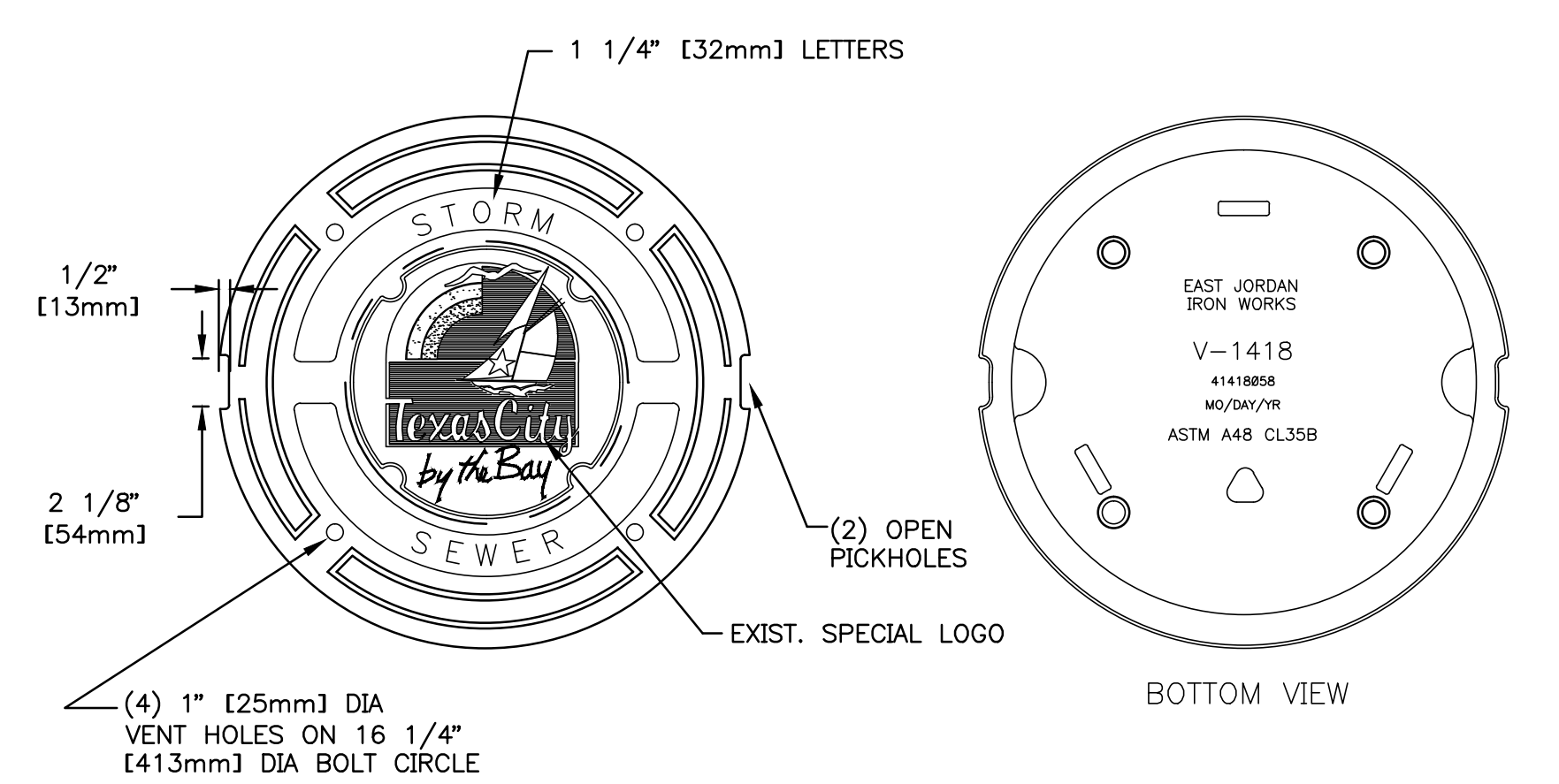
A permissible construction joint may be placed in the inlet wall with the approval of the Engineer. Where shown elsewhere on plans a 6"x24" opening shall be placed in the backwall of the inlet as directed by the Engineer.

Manhole ring and cover shall be 23" unless otherwise specified in the plans. Precasting of Stage I Construction will be permitted with the approval of the Engineer. Connection of pipes to precast units shall be mortared as directed by the Engineer.

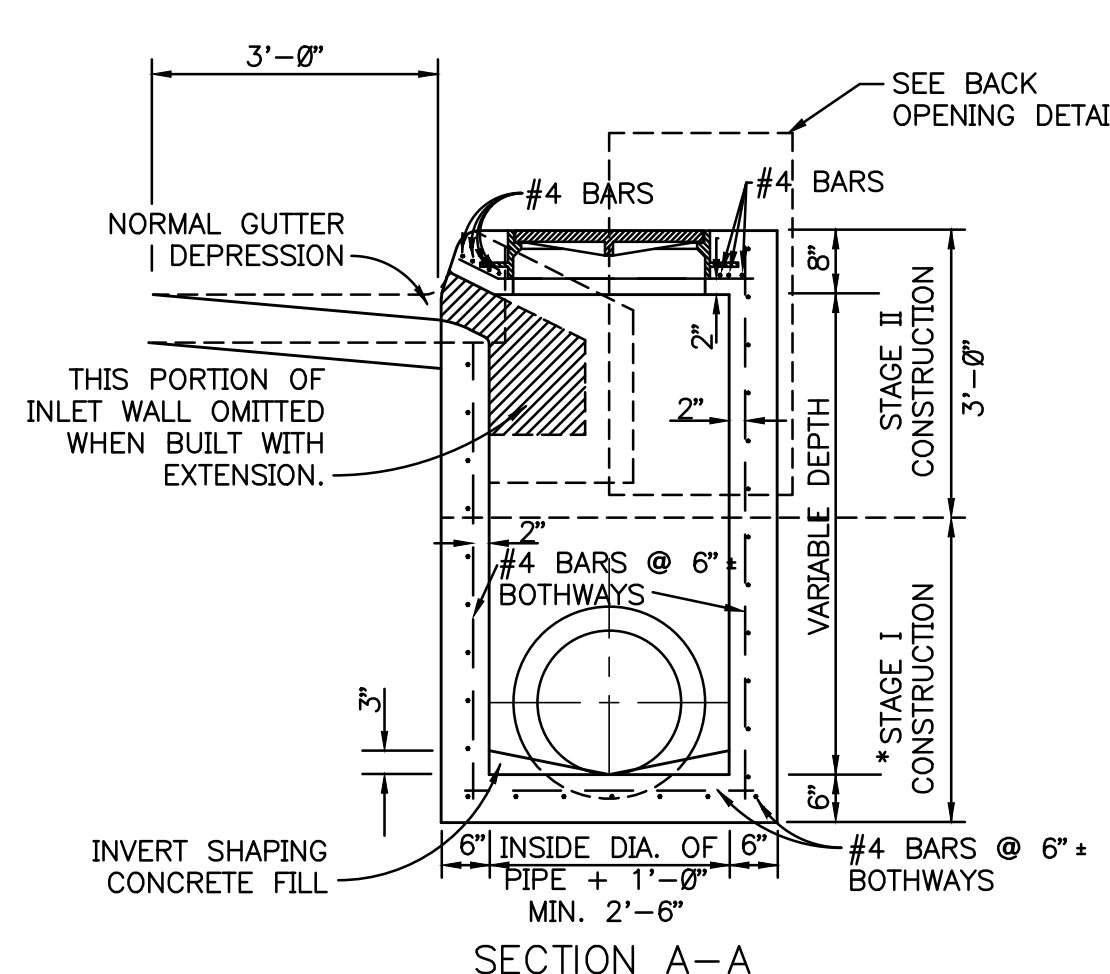
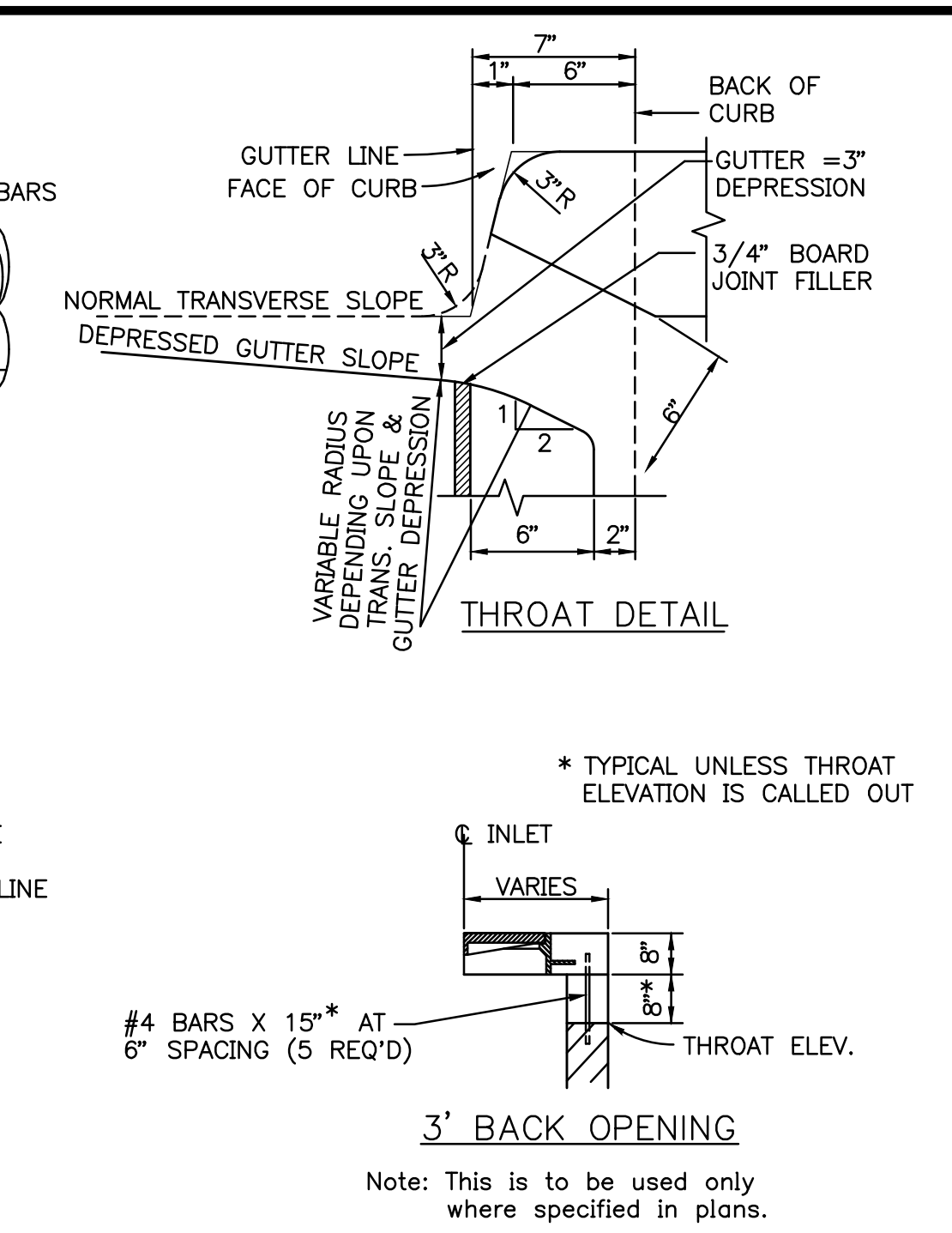
* But not less than six inches over highest pipe.

Control points for horizontal layout of "c" inlets, all types, is the lateral center of the inlet, without regard for extensions, at the back of curb line.

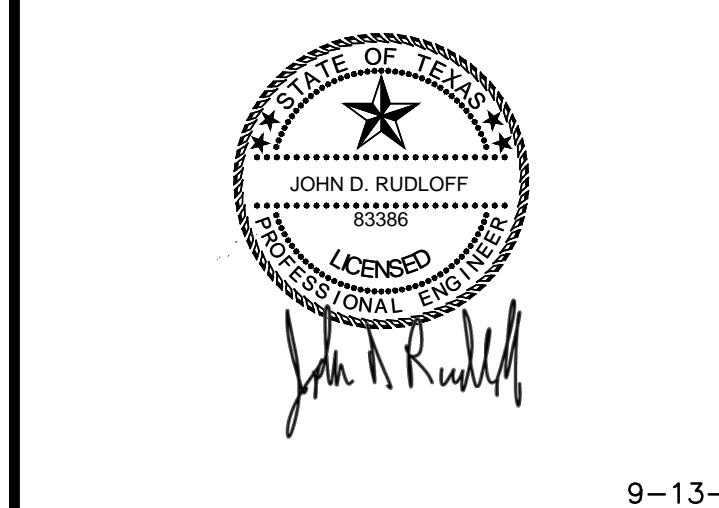
TYPE "C" INLET DETAILS
NOT TO SCALE



TYPE "C"/"C-1"/"C-2"/"C-2A" INLET MANHOLE COVER DETAIL
NOT TO SCALE



MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19

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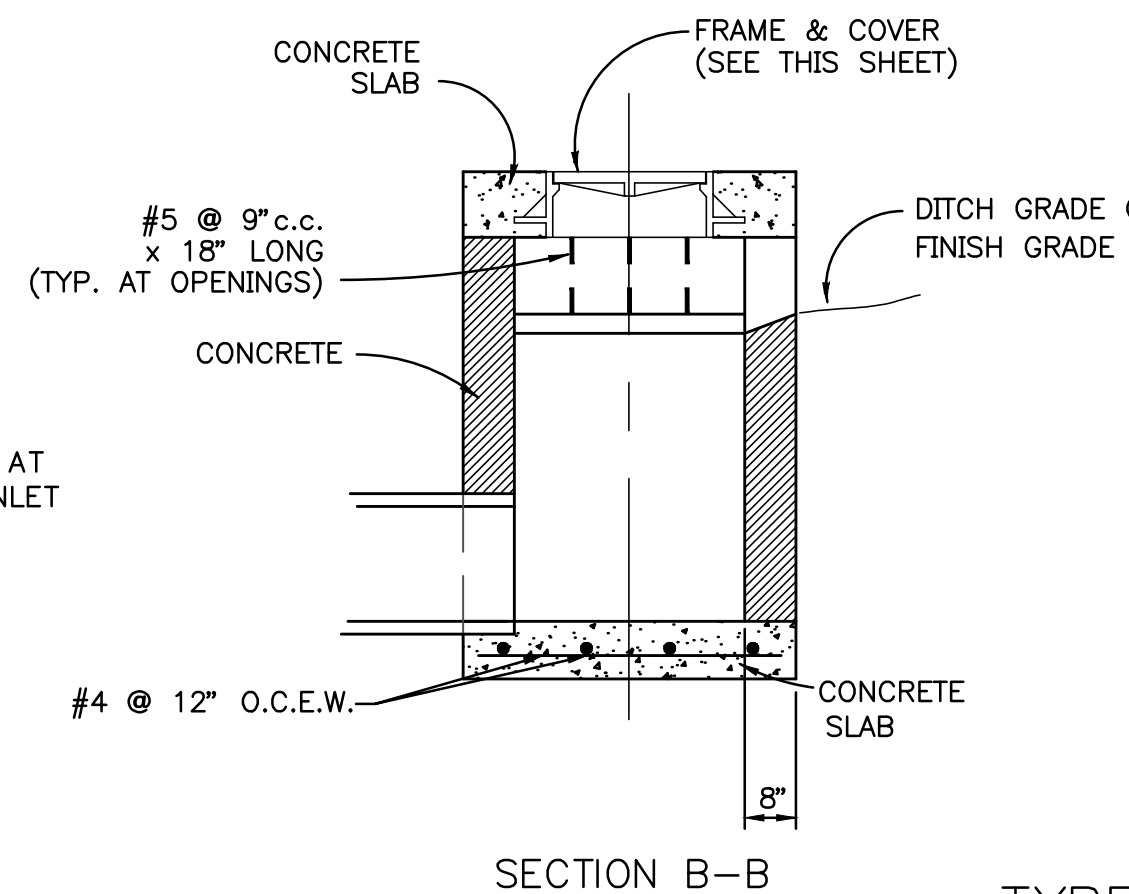
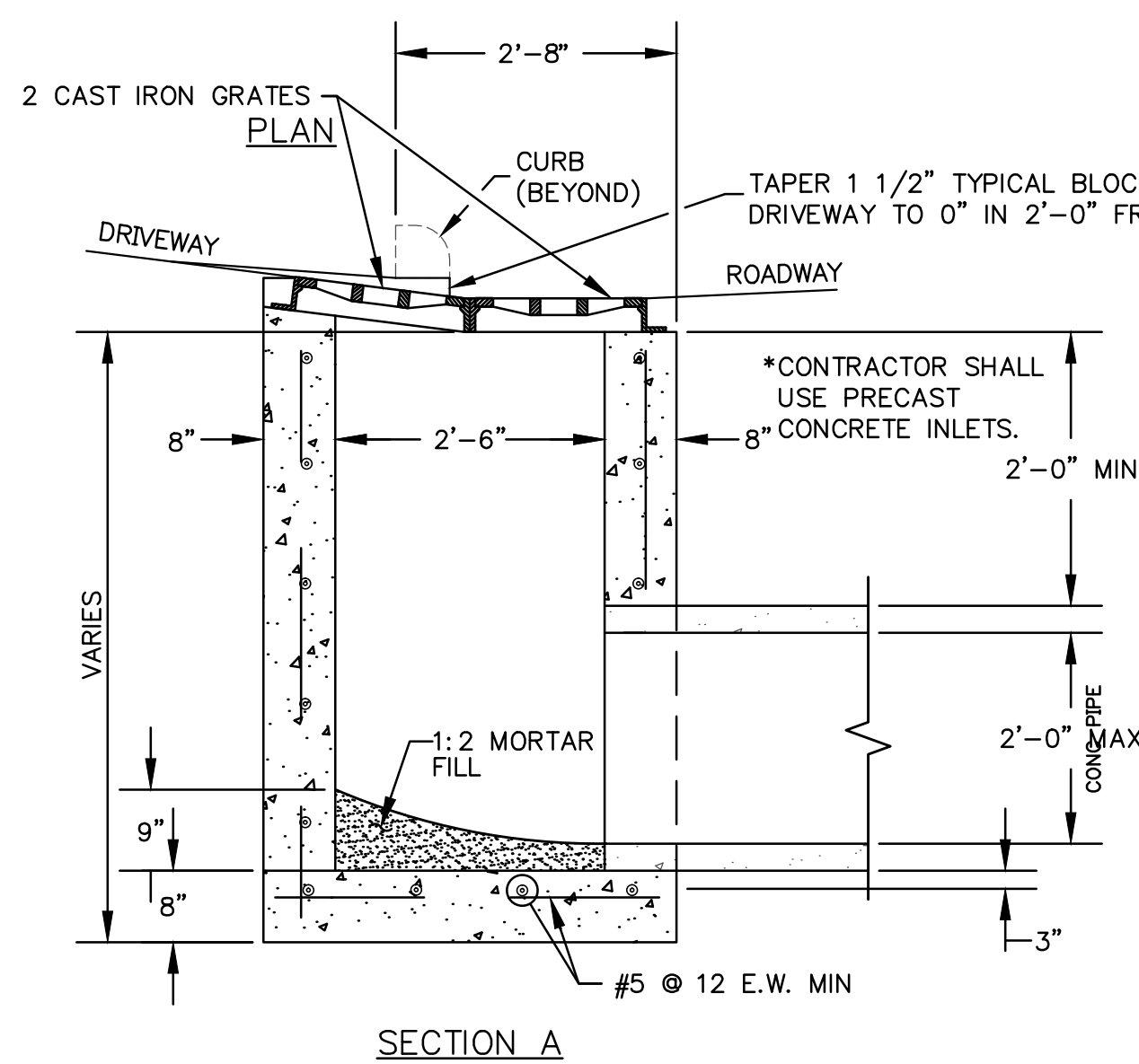
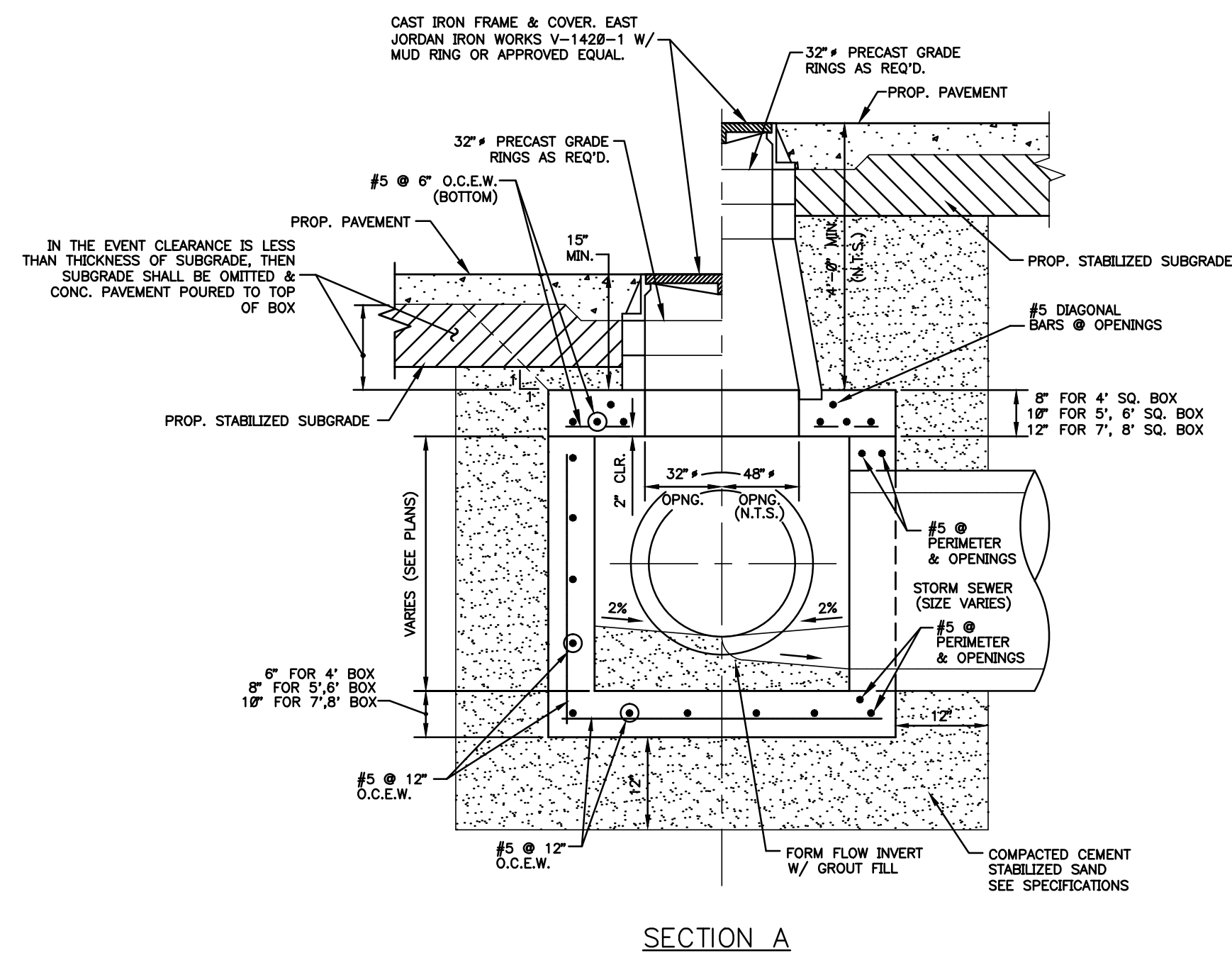
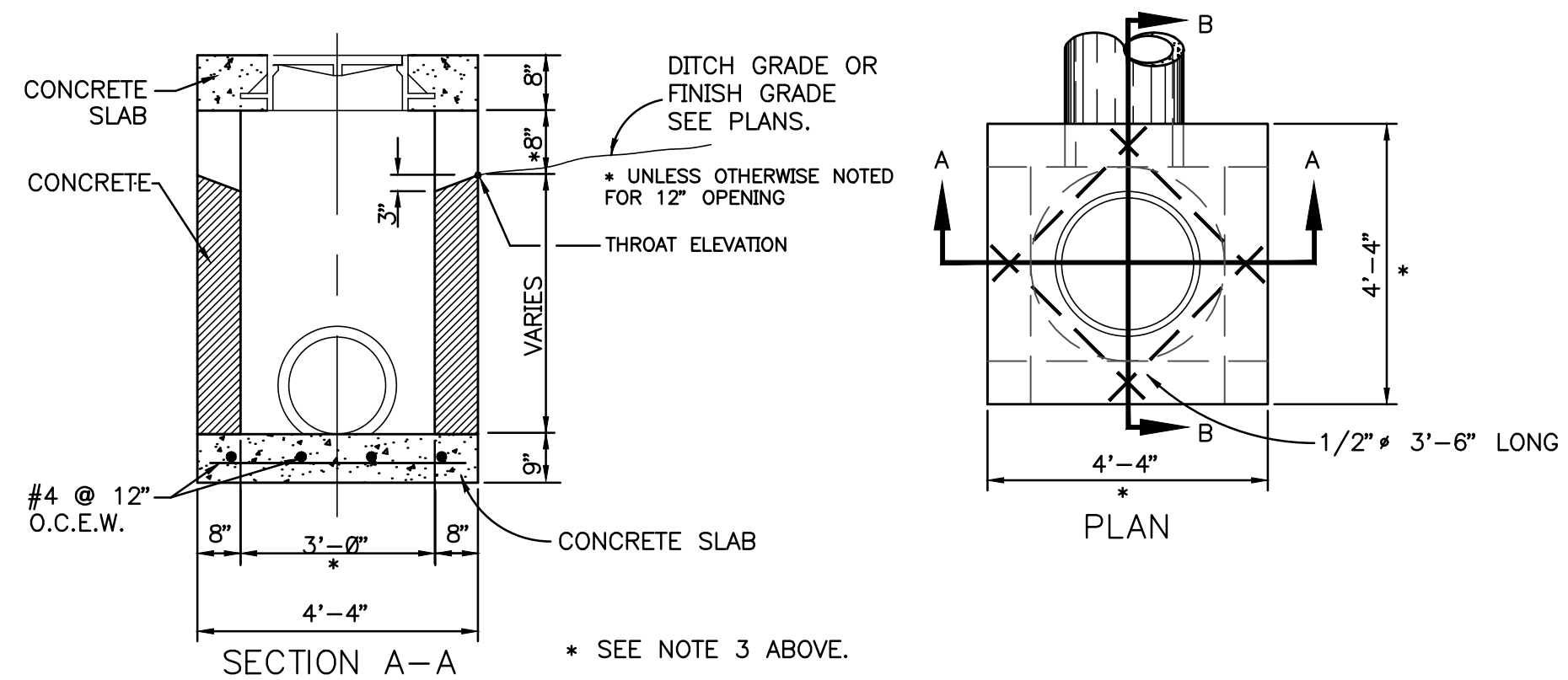
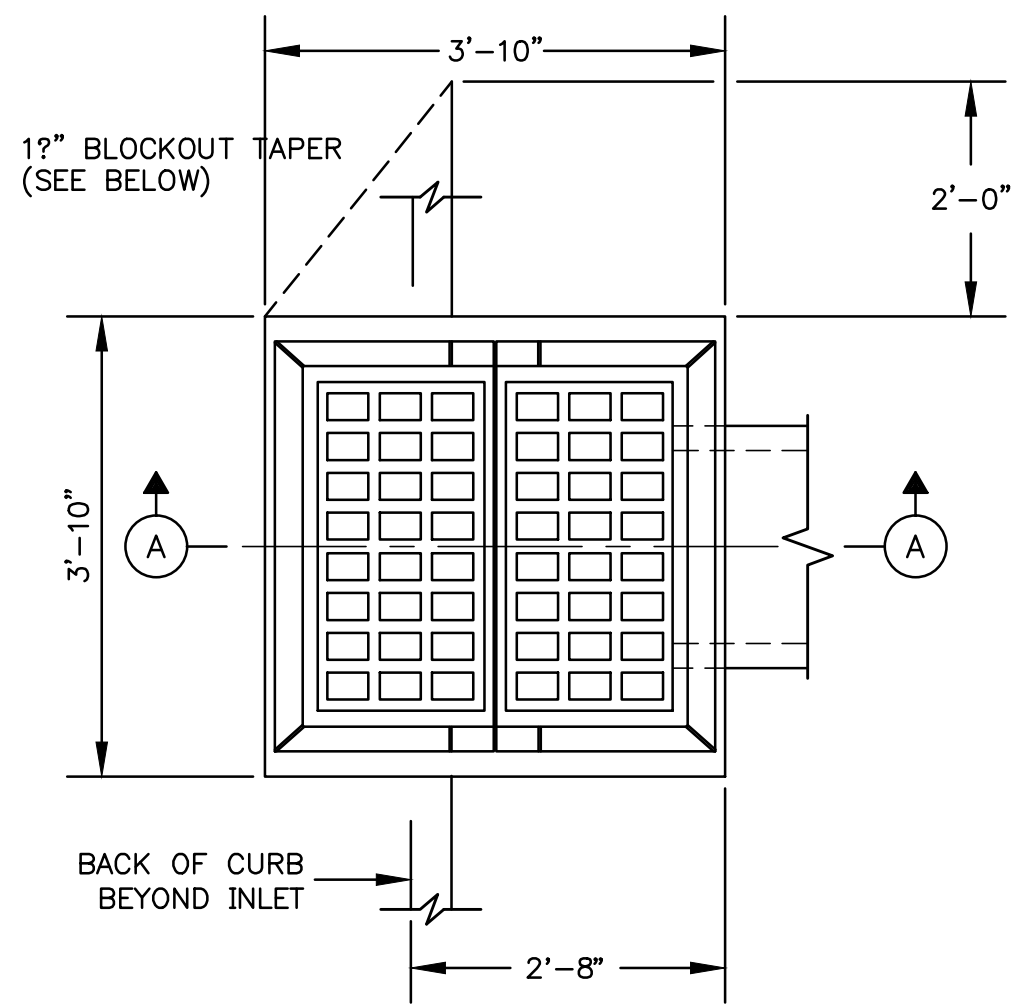
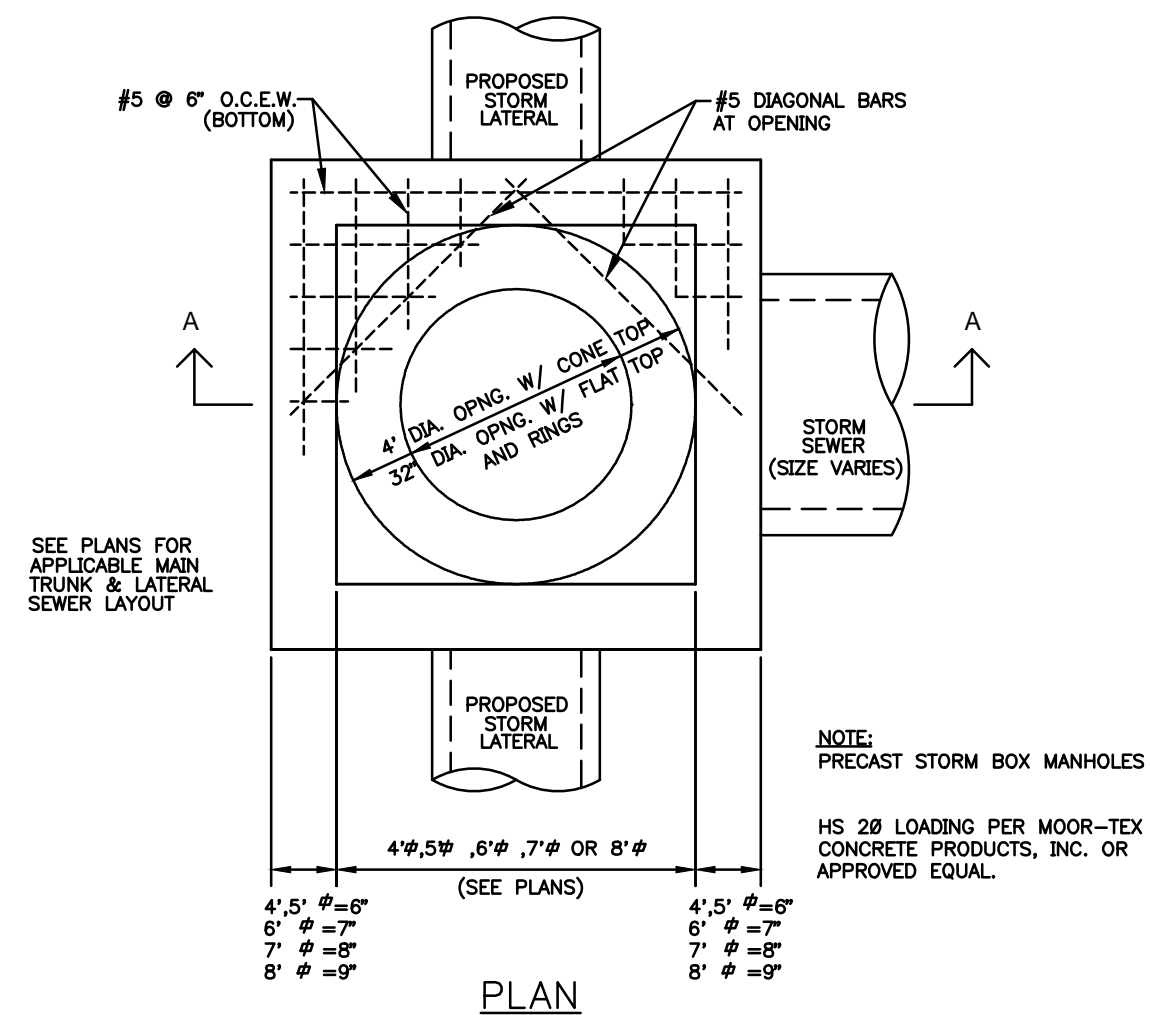
Texas Avenue Reconstruction

Drainage Details I

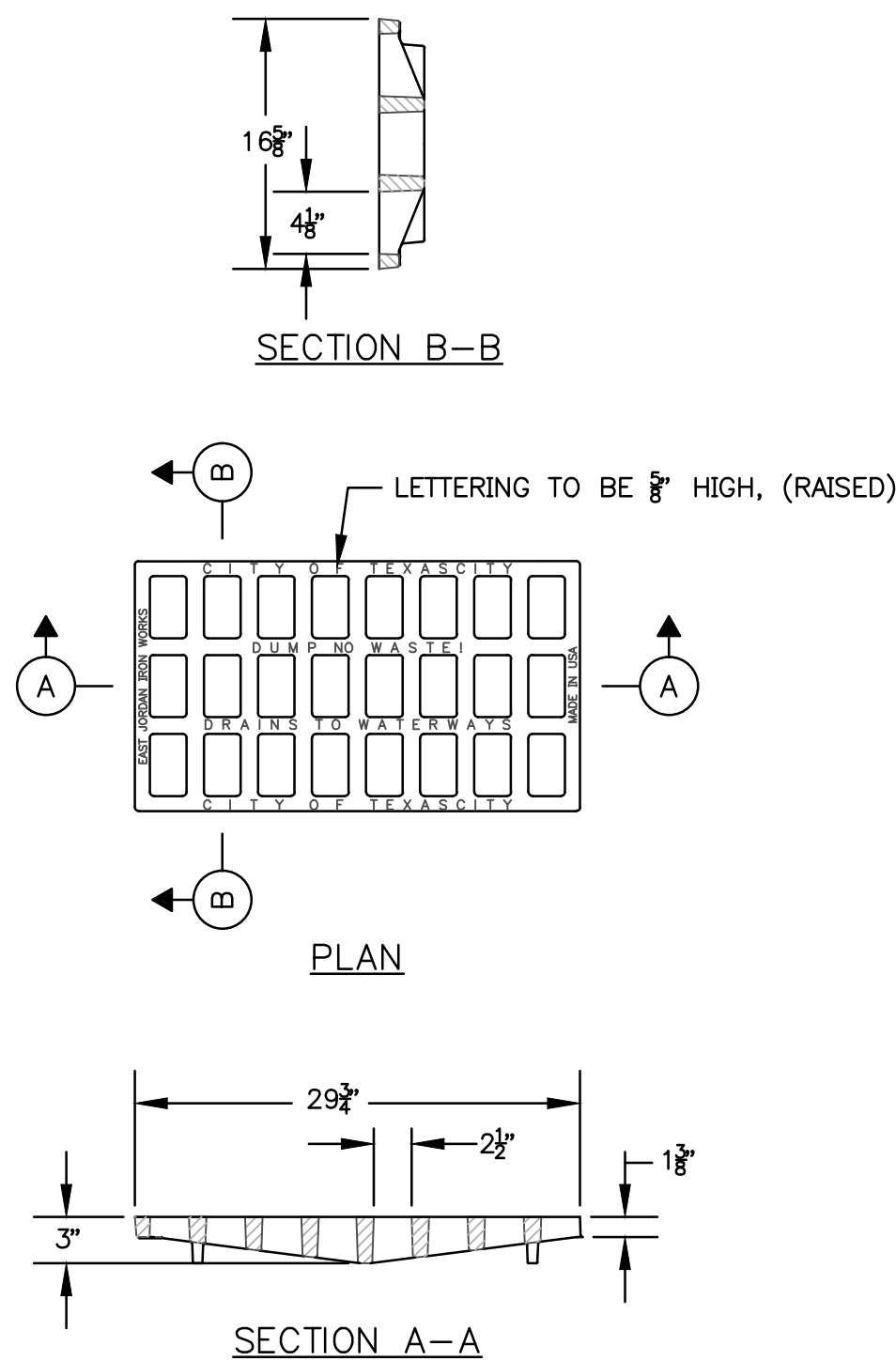
Job No.: 18-015
Date: September, 2019
Dwn By: D. Fattig
Chk By: J Rudloff

Scale: HORZ: N/A
VERT: N/A

SHEET **40** OF 52



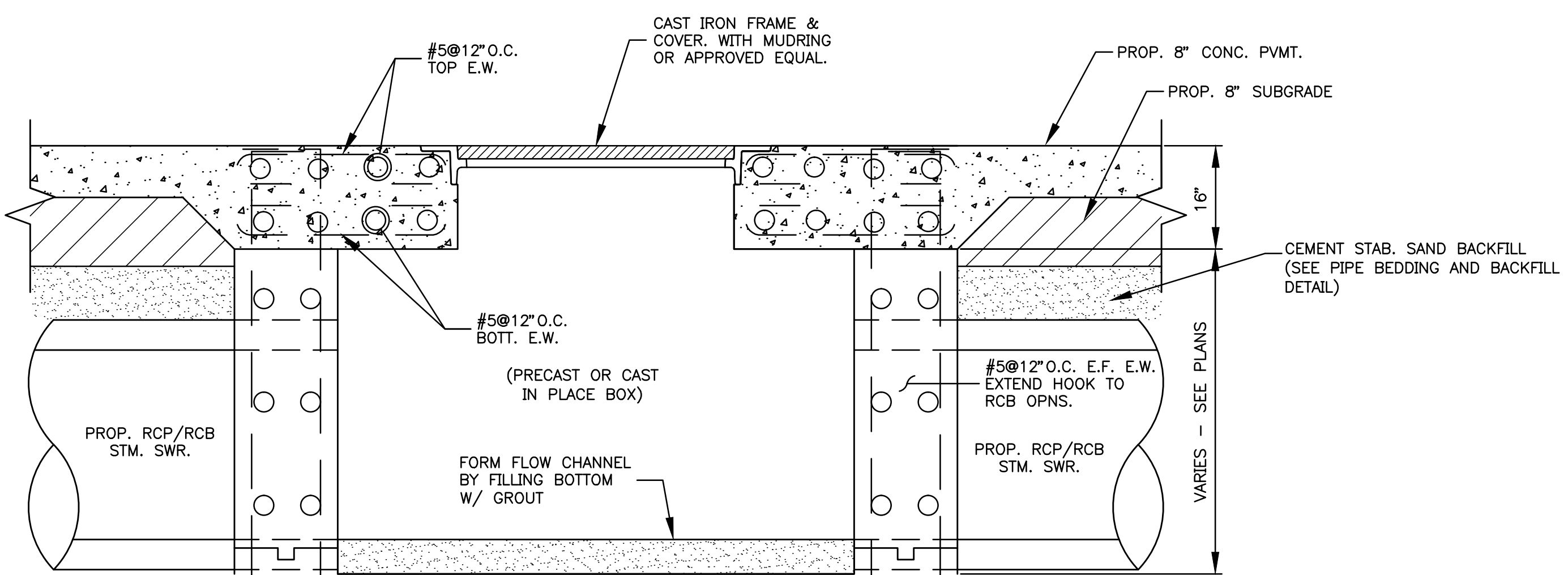
TYPE "E" INLET
NOT TO SCALE



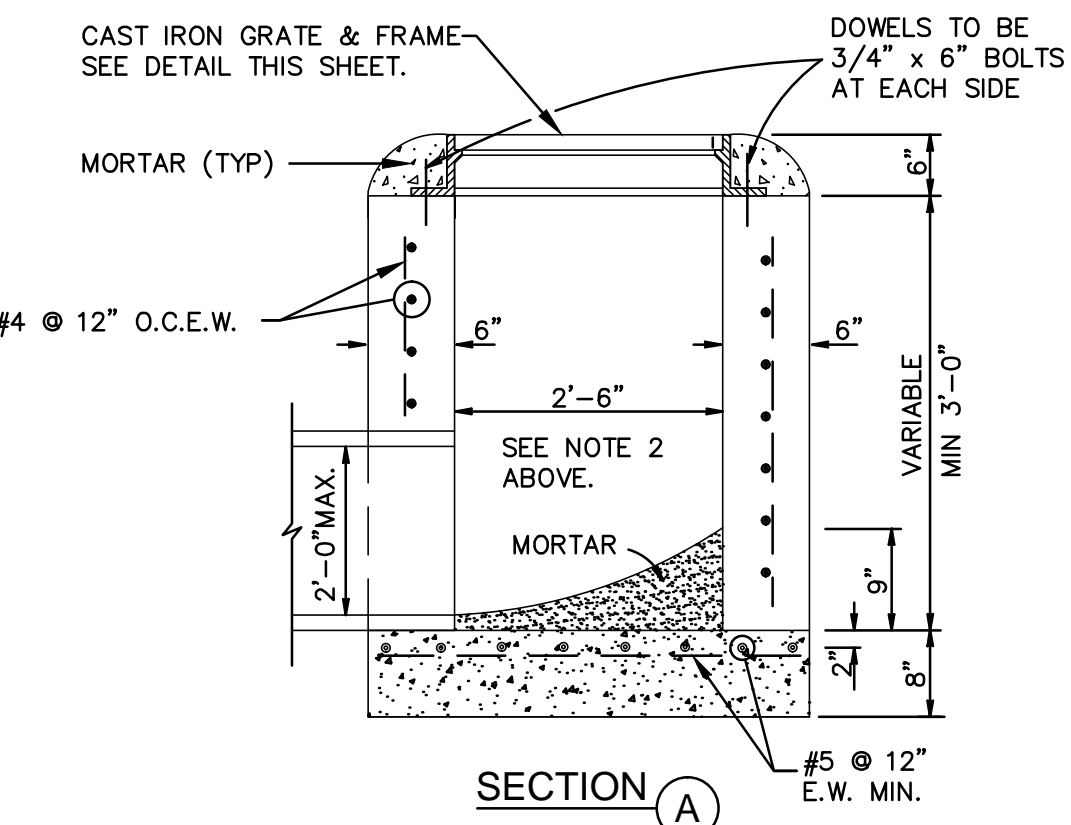
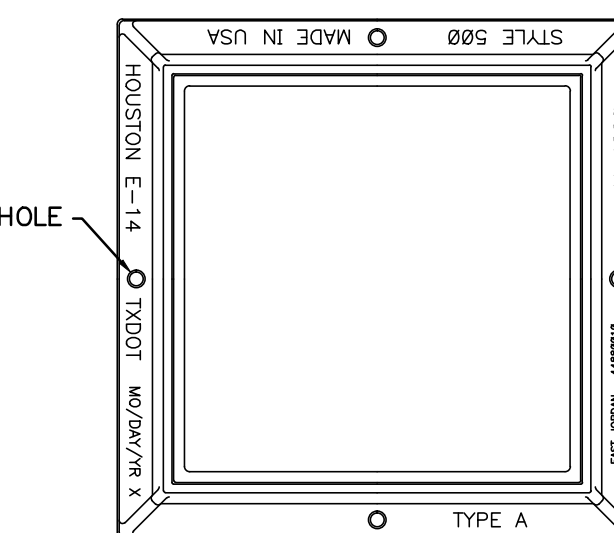
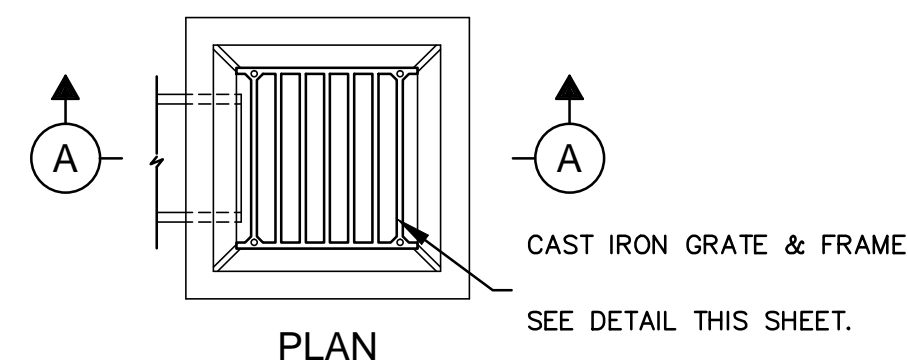
GRATE FRAME & COVER DETAILS
NOT TO SCALE

PRECAST STORM SEWER BOX MANHOLE
NOT TO SCALE

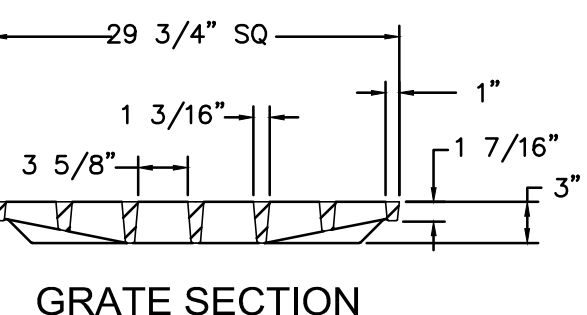
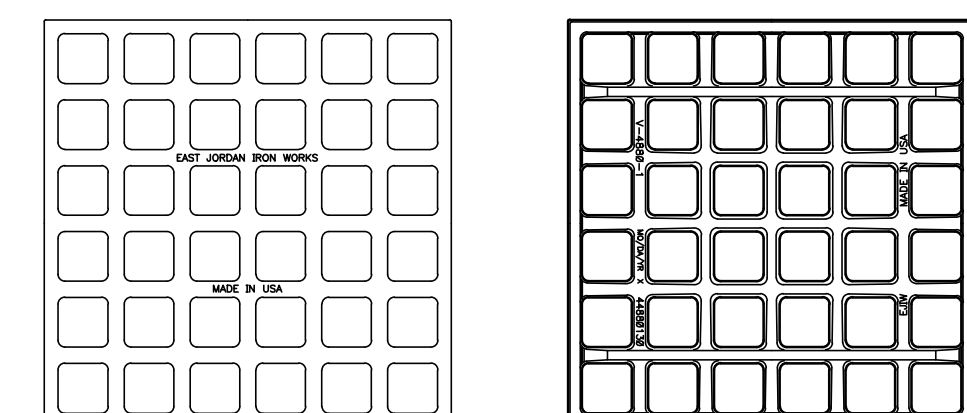
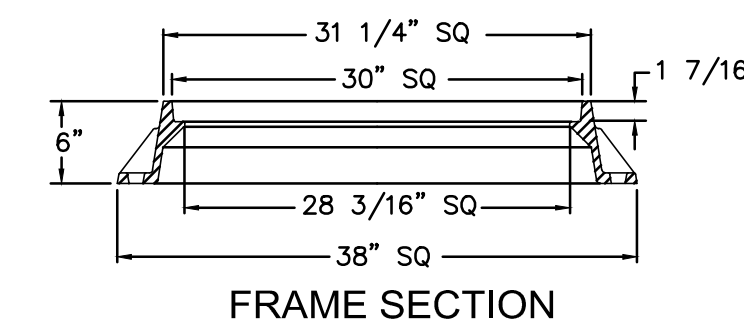
ALTERNATE TYPE B-B INLET WITH GRATE TOP
NOT TO SCALE



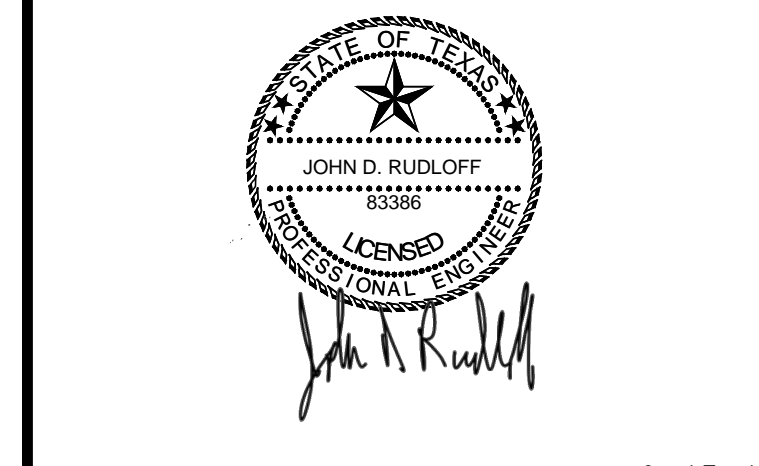
SHALLOW BOX MANHOLE CAST IN PLACE TOP DETAIL
NOT TO SCALE



TYPE "A" GRATE INLET DETAIL



MK.	DESCRIPTION	DATE	DWN.	CHK.

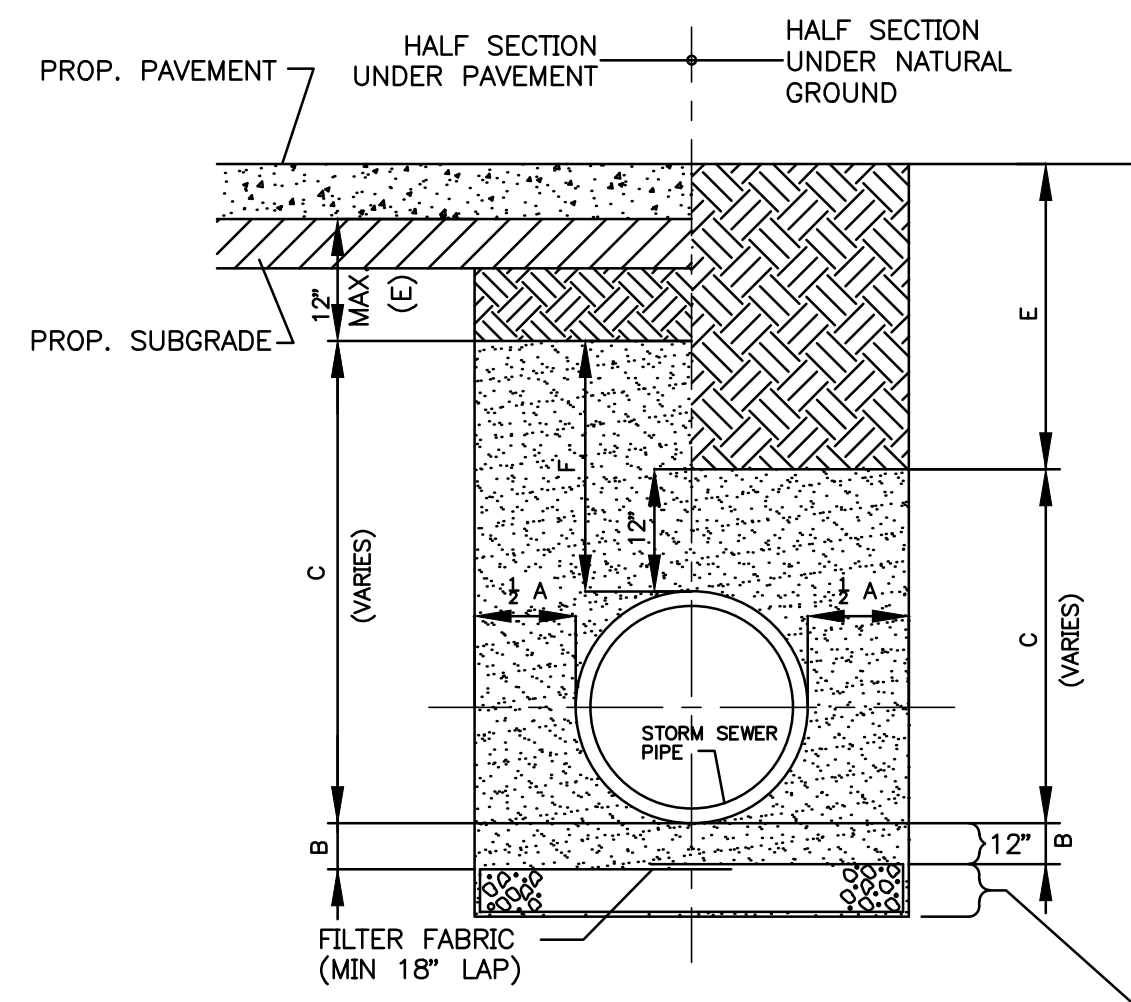


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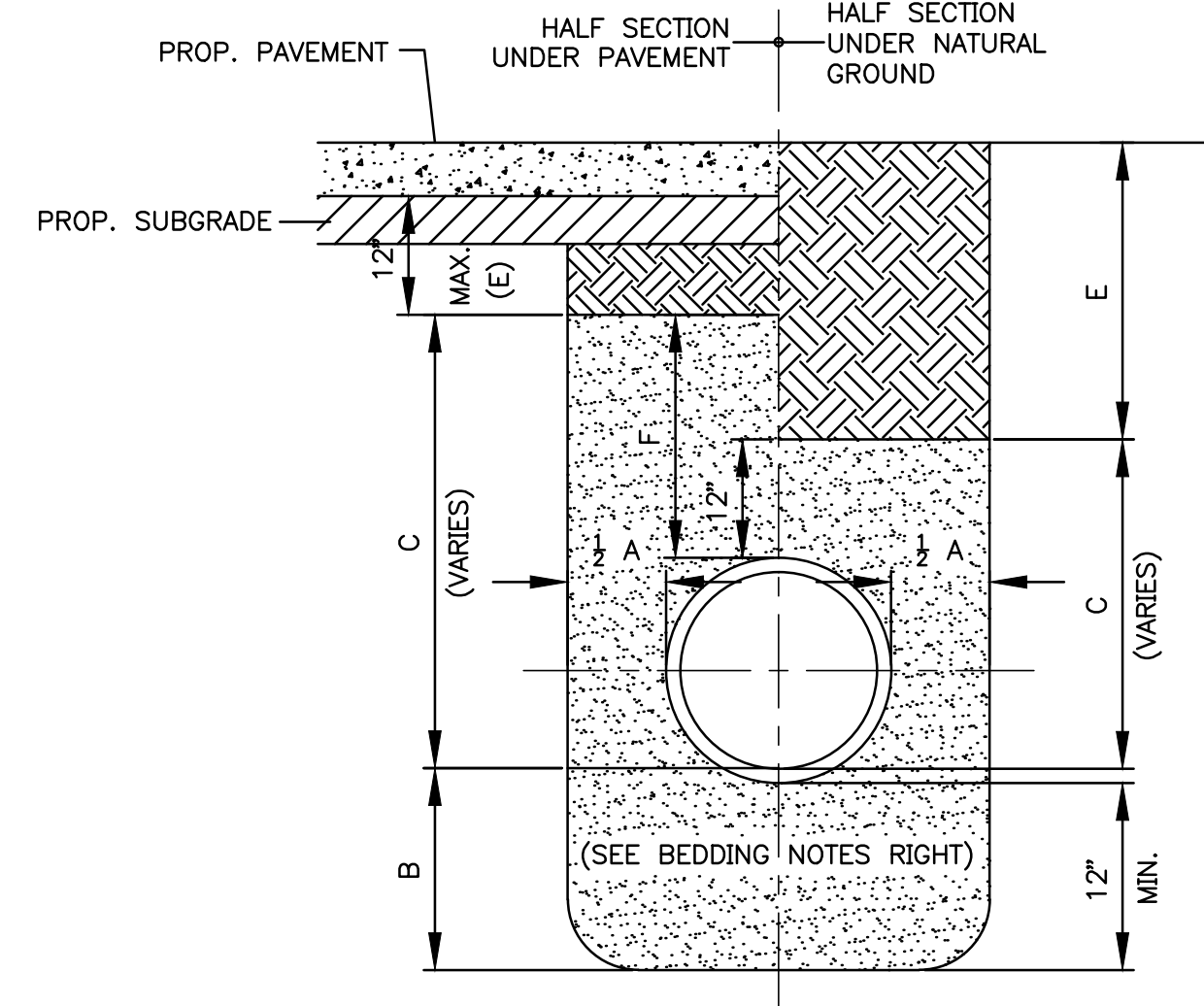
Galveston County, Texas
Texas Avenue Reconstruction

Drainage Details II

Job No.: 18-015	Scale: HORZ: VERT: N/A	SHEET
Date: September, 2019		41
Dwn By: D. Fattig		OF 52
Chk By: J Rudloff		



WET CONDITION BEDDING
NOT TO SCALE



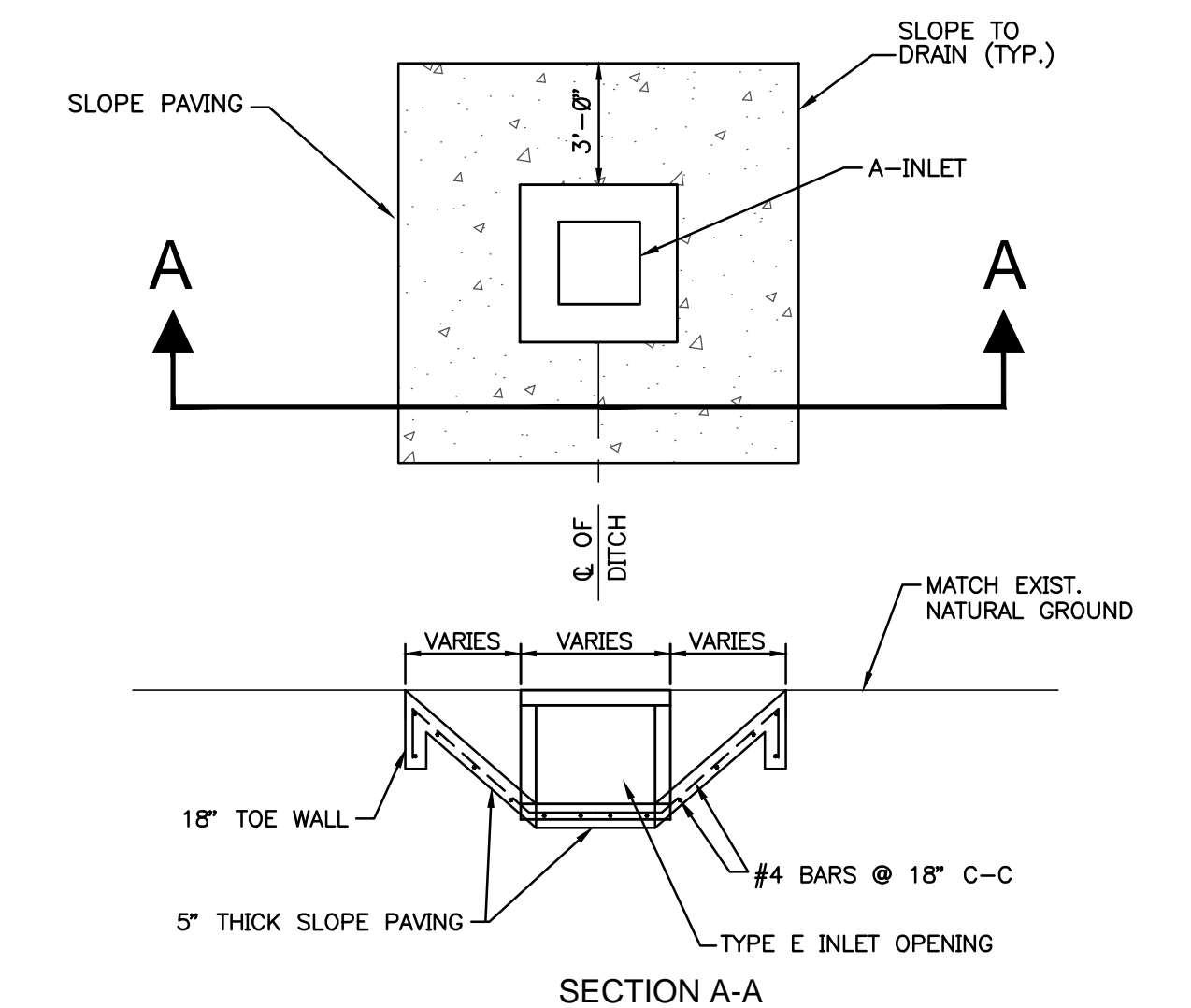
BEDDING AND BACKFILL DETAIL FOR STORM SEWER PIPES
NOT TO SCALE

BEDDING AND BACKFILL NOTES (APPLICABLE TO ALL DETAILS THIS SHEET):

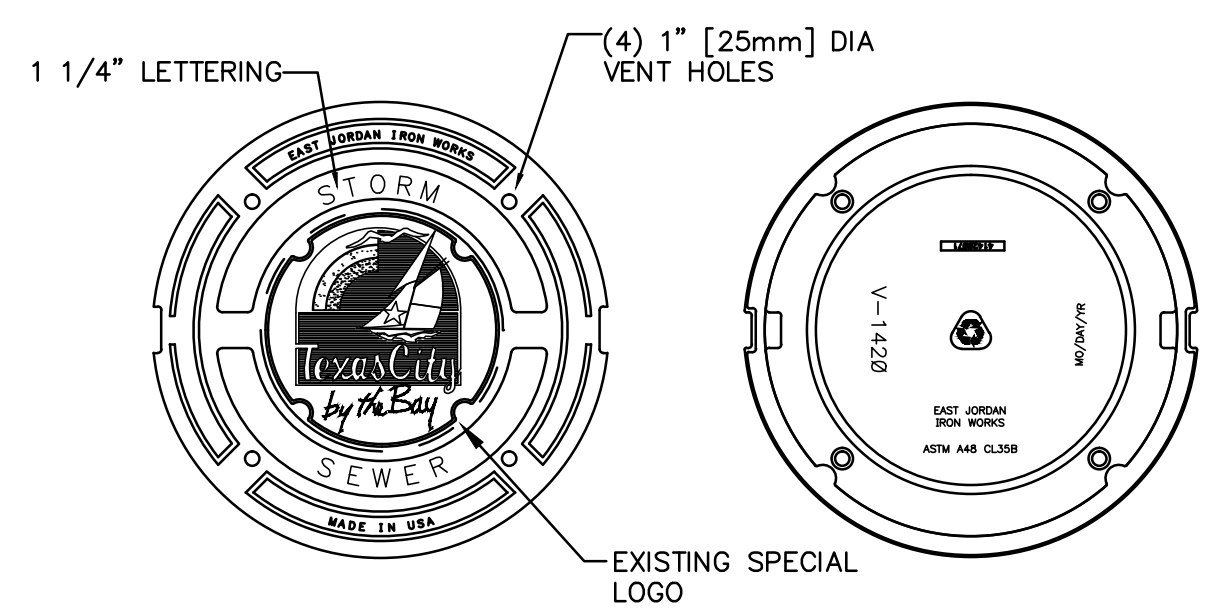
- A. MIN. TRENCH WIDTH SHALL BE PIPE O.D. PLUS AN ALLOWANCE "A" FOR THE NOMINAL PIPE SIZE:

NOMINAL PIPE SIZE	"A"
<18"	18"
18" TO 30"	24"
>30"	36"

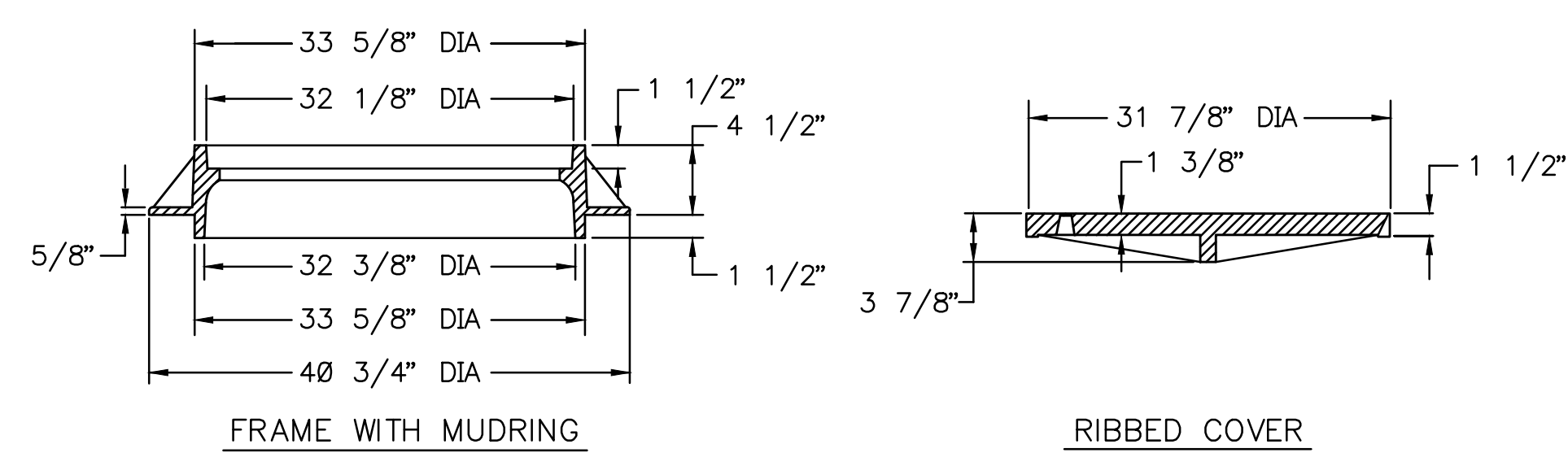
MAX TRENCH WIDTH SHALL NOT BE GREATER THAN MIN TRENCH WIDTH PLUS 24". UNLESS OTHERWISE NOTED.
 IF OUTSIDE EDGE OF PIPE IS WITHIN 2' OF BACK OF CURB, BACKFILL SHALL BE PERFORMED AS UNDER PAVEMENT.
- B. CEMENT STABILIZED SAND (1.5 SACKS OF CEMENT PER CUBIC YARD, COMPACTED TO 95% OF MAX. STD. PROCTOR) PLACED BEFORE PIPE IS LAID UP TO FLOW LINE OF PIPE OR ABOVE—MINIMUM DEPTH = 12".
- C. CEMENT STABILIZED SAND (AS SPECIFIED ABOVE) PLACED AFTER PIPE IS LAID IN 8" LIFTS.
- D. COMPACTED BANK SAND BACKFILL, COMPACTED AS PER SPECIFICATIONS.
- E. SELECT EARTH BACKFILL WITH MAX LIQUID LIMIT OF 40, MIN. P.I. OF 7, MAX P.I. OF 20 CONTAINING NO ROCKS OR OTHER DEBRIS NOR CONTAINING ANY DIRT CLOUDS EXCEEDING 6" IN ANY DIMENSION. PLACED IN 6" LAYERS, MOISTENED IF NECESSARY AND THOROUGHLY COMPACTED TO 95% DENSITY AS DETERMINED BY ASTM D698, UNLESS OTHERWISE NOTED.



SLOPE PAVING W/ WINGWALL AT E-INLET
NOT TO SCALE



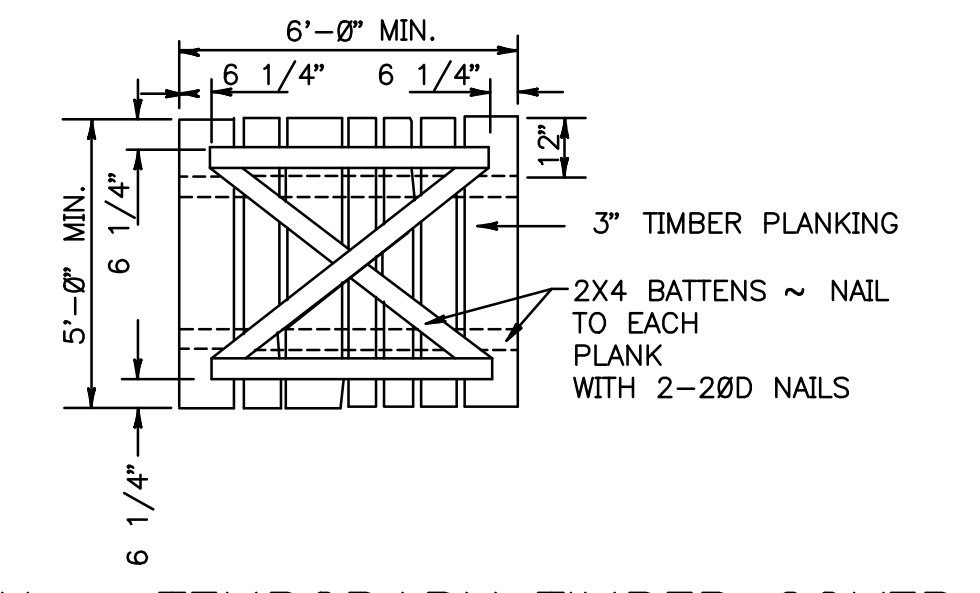
BOTTOM VIEW OF COVER



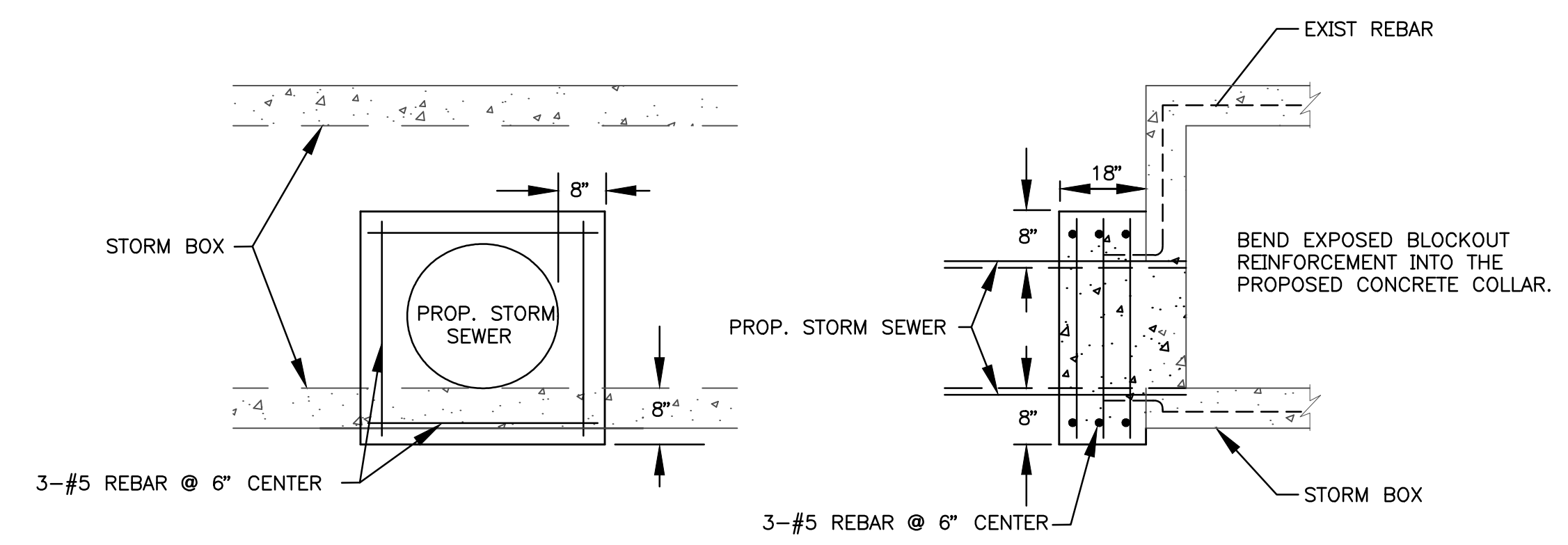
STORM MANHOLE FRAME & COVER
NOT TO SCALE

GENERAL NOTES:

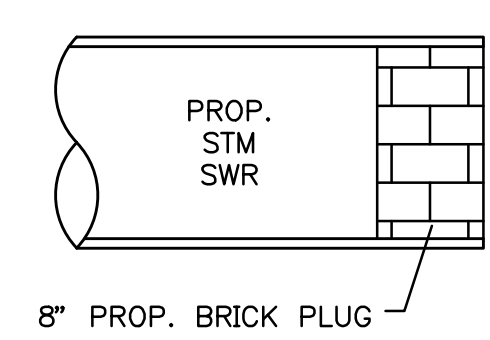
- 1. ALL CONCRETE SHALL BE CLASS A. ALL EXPOSED CORNERS SHALL BE CHAMFERED 3/4". PIPES SHALL ENTER INLETS AS SHOWN ELSEWHERE ON PLANS. SLOPE TOP OF INLETS AS DIRECTED TO MATCH GRADED SECTION.
- 2. ALL MATERIALS USED IN CASTING MANHOLE COVERS AND LADDER RUNG SHALL CONFORM TO A.S.T.M. SPECIFICATIONS.
- 3. A PERMISSIBLE CONSTRUCTION JOINT MAY BE PLACED IN THE INLET WALL WITH THE APPROVAL OF THE ENGINEER.
- 4. MANHOLE RING AND COVER SHALL BE 32" UNLESS OTHERWISE SPECIFIED IN THE PLANS. CONNECTION OF PIPES TO PRECAST UNITS SHALL BE MORTARED AS DIRECTED BY THE ENGINEER.



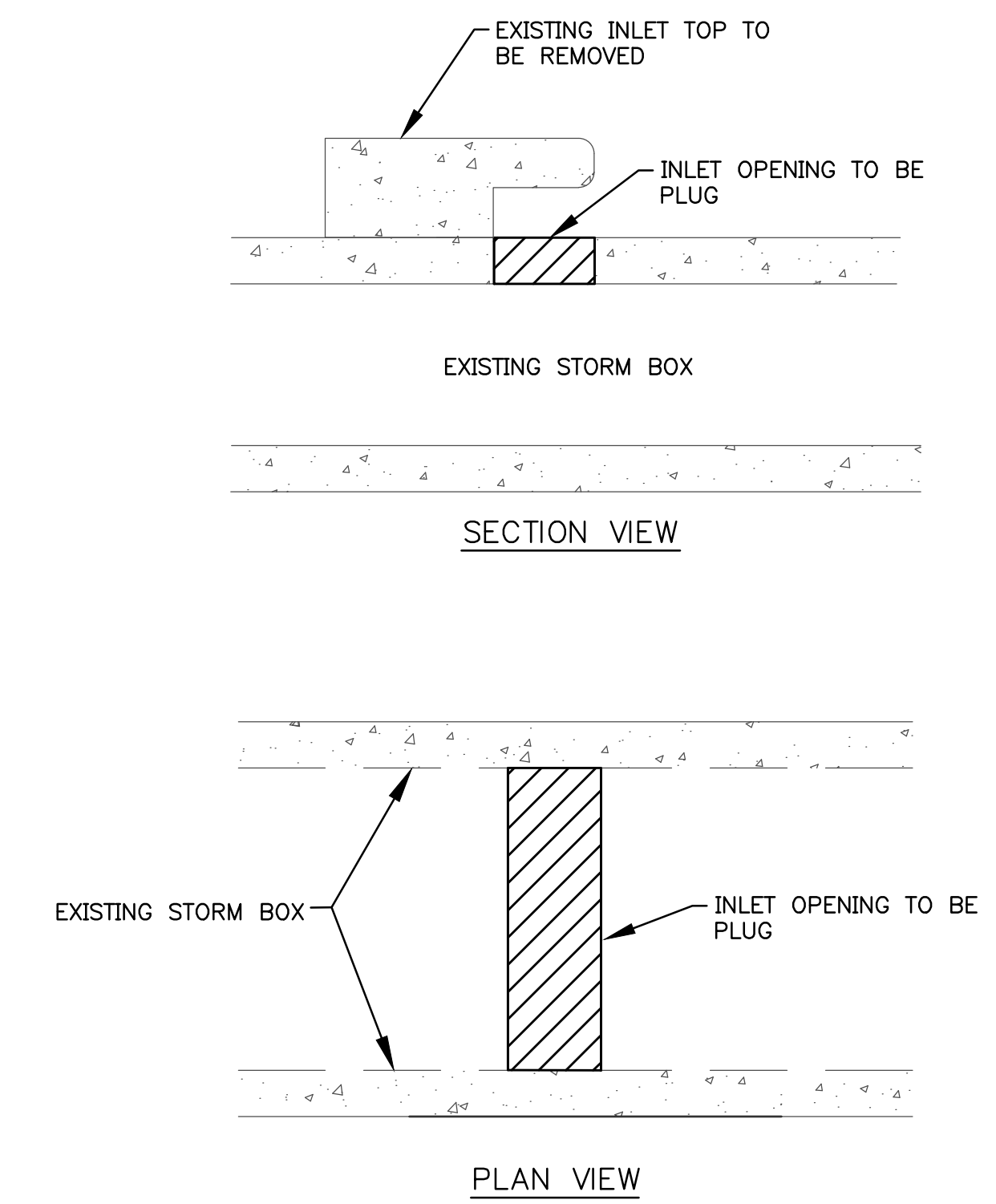
PLAN ~ TEMPORARY TIMBER COVER
NOT TO SCALE



PIPE TO BOX CONNECTION DETAIL
NOT TO SCALE



PLUG PROPOSED STORM SEWER
NOT TO SCALE



PLUG PROPOSED INLET OPENING
NOT TO SCALE

MK.	DESCRIPTION	DATE	DWN.	CHK.

9-13-19

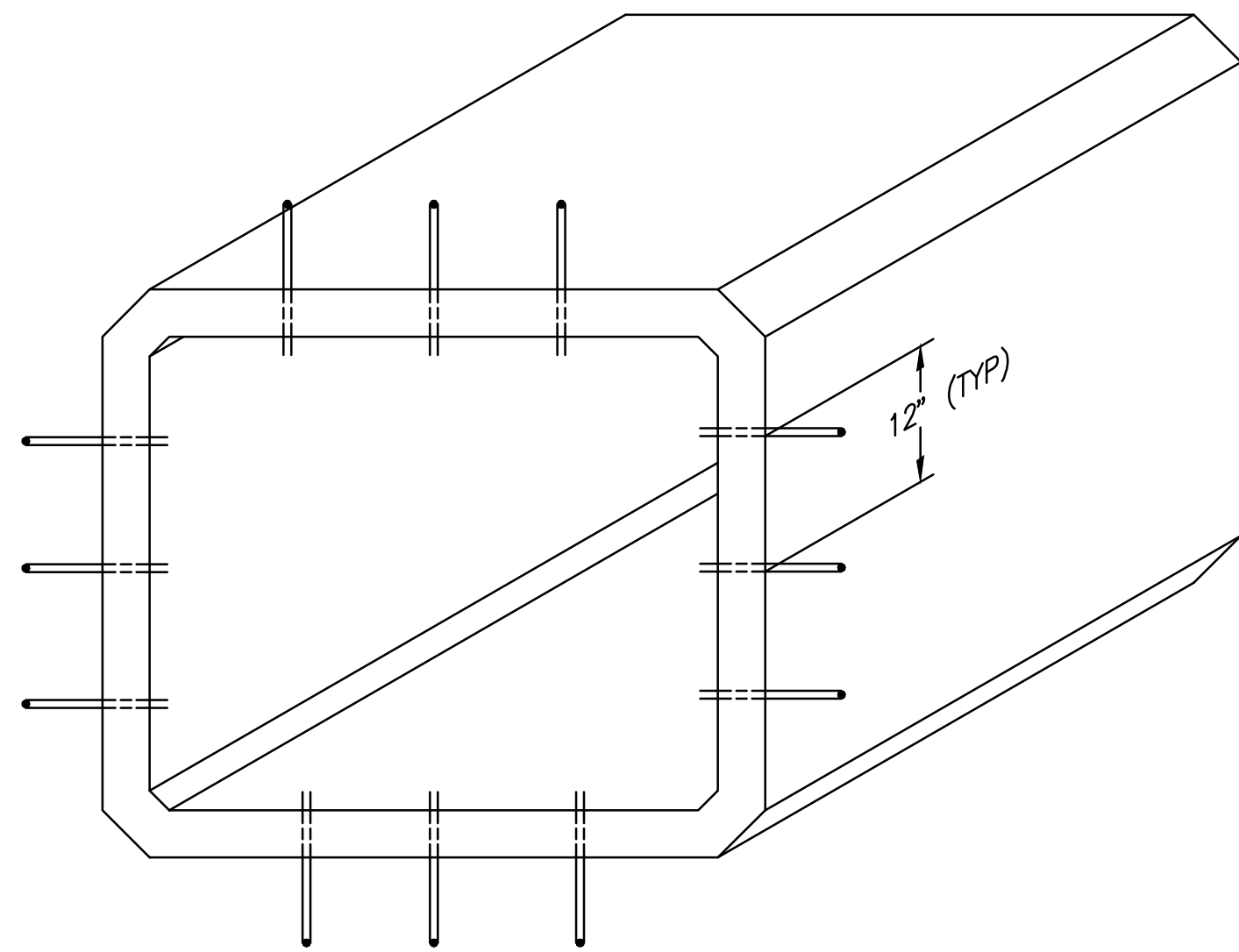
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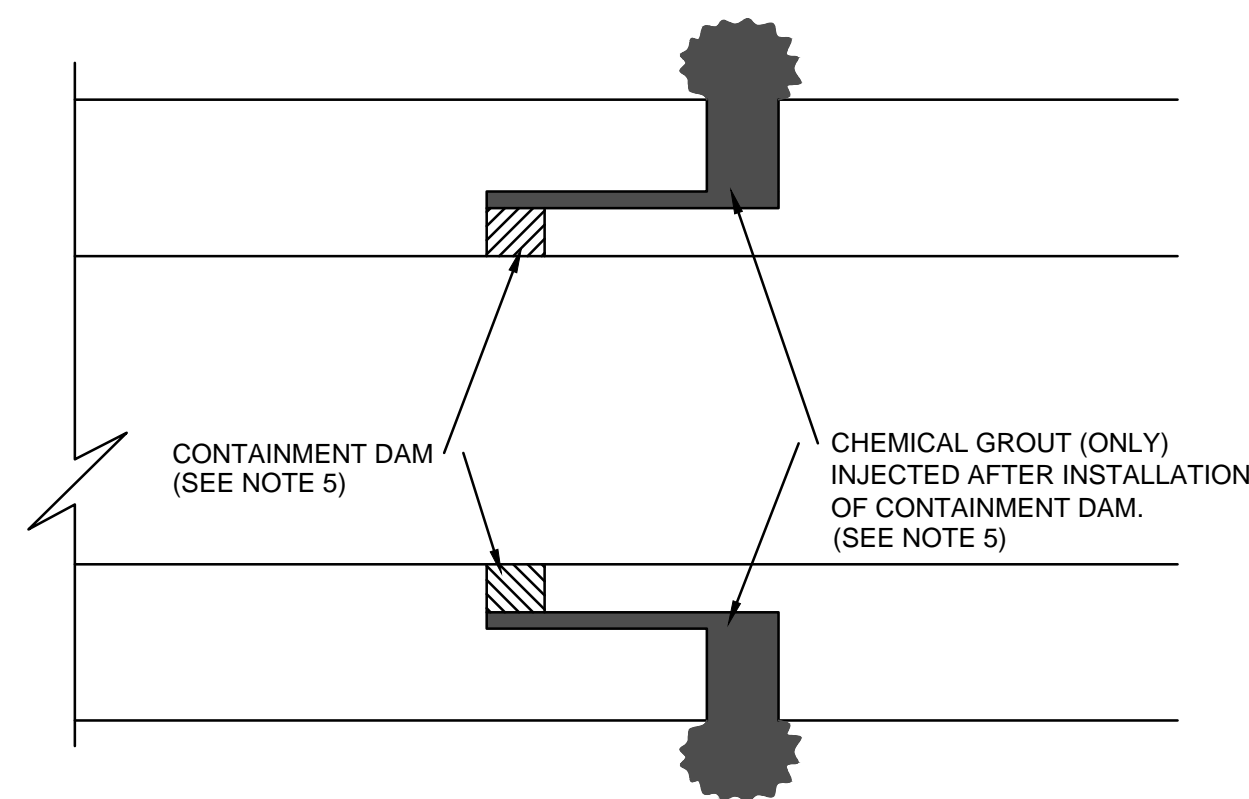
Texas Avenue Reconstruction

Drainage Details III

Job No.: 18-015	Scale: HORZ: N/A	SHEET 42 OF 52
Date: September, 2019	VERT: N/A	
Dwn By: D. Fattig		
Chkd By: J Rudloff		



JOINT REPAIR SPACING



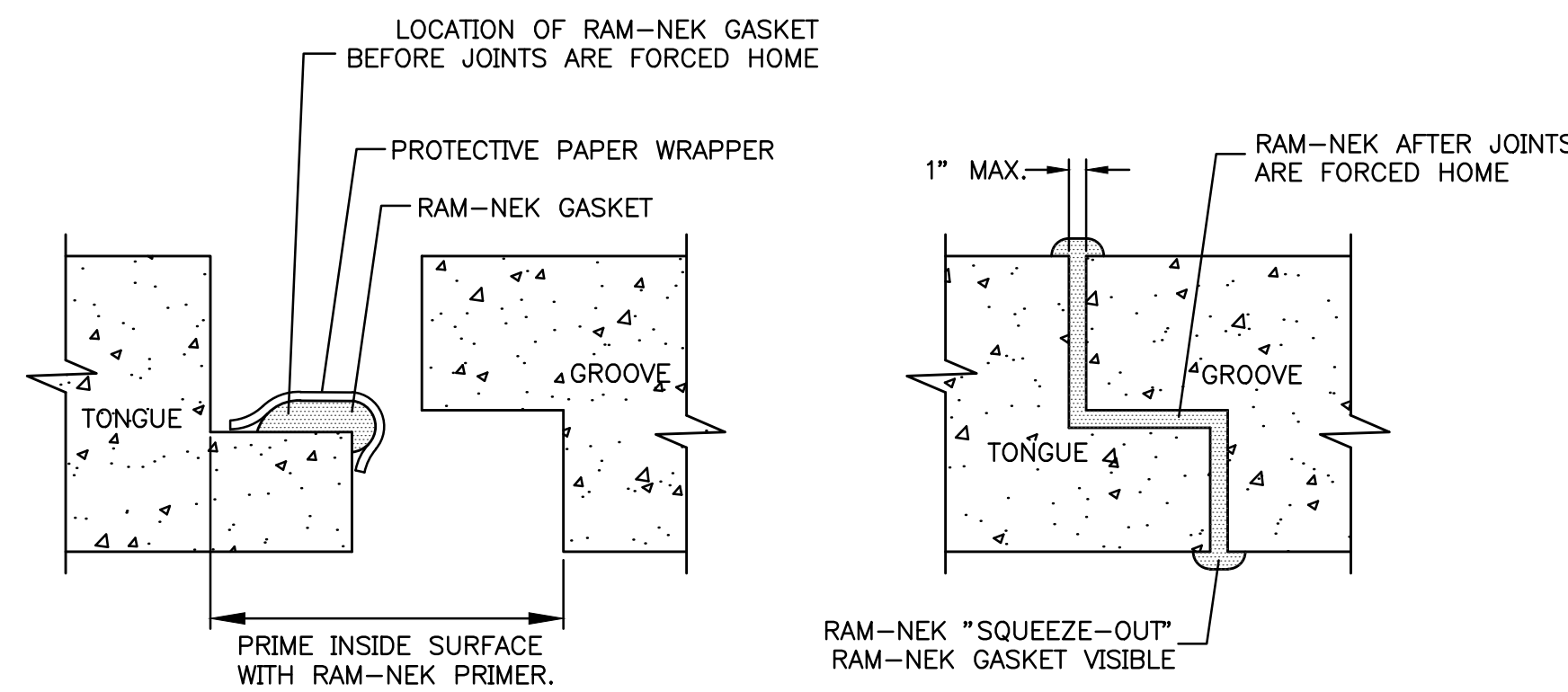
JOINT REPAIR DETAIL

NOTES:

1. JOINT REPAIR SHALL BE PERFORMED FROM THE INSIDE OF THE STORM SEWER SYSTEM AND SHALL BE PERFORMED IN STRICT ACCORDANCE TO ALL LOCAL, STATE, AND FEDERAL LAWS. THE CONTRACTOR SHALL PROVIDE A SAFETY PLAN THAT SHALL INCLUDE BUT NOT LIMITED TO, GAS DETECTOR, TRIPOD AND WRENCH, HARNESS, VENTILATION DEVICES, ETC.
2. CONTRACTOR SHALL REMOVE ALL EXISTING FILL AND DEBRIS FROM ALL AREAS AROUND THE JOINTS TO A WIDTH OF 12" FROM CENTERLINE OF JOINT. THE FILL AND DEBRIS CAN BE TEMPORARILY PLACED ADJACENT TO THE JOINT AND BE REPLACED IN THE SAME LOCATION AT THE SAME HEIGHT AFTER REPAIR OF JOINT. FILL WILL NOT BE ALLOWED TO REMAIN IN A PILE AFTER REPAIR OF THE JOINT.
3. COFFERDAMS, SANDBAGS, PUMPS AND OTHER MEANS OF DEWATERING SHALL BE USED TO MAINTAIN THE WATER AT A LOW LEVEL. IT IS NOT NECESSARY FOR THE JOINT TO BE DRY, BUT WATER LEVEL SHALL BE MAINTAINED AT AS LOW A LEVEL AS IS PRACTICAL. FLOW IN BOX CULVERTS MUST BE CONTROLLED TO AN EXTENT THAT JOINT BEGINNING REPAIRED IS NOT INUNDATED BY WATER.
4. ALL EXISTING BITUMINOUS JOINT SEALANT MATERIAL SHALL BE REMOVED FROM JOINTS PRIOR TO WORK. THE JOINTS SHALL BE CLEANED BY PRESSURIZED WATER BLASTERS TO REMOVE LOOSE DEBRIS.
5. THE JOINTS SHALL HAVE A "CONTAINMENT DAM" USED TO PROVIDE CONTAINMENT FOR THE GROUT THAT IS INJECTED BEHIND THE BOX CULVERT. THE "CONTAINMENT DAM" SHALL BE AN APPROVED CEMENTITIOUS GROUT OR SATURATED JUTE OAKUM WITH AN APPROVED CHEMICAL GROUT, AS INDICATED IN SPECIFICATIONS. CEMENTITIOUS GROUT MAY ONLY BE USED IN SECTIONS OF NON-SUBMERGED JOINTS ONLY. SATURATED JUTE OAKUM SHALL BE USED IN SUBMERGED AREAS AND MAY BE USED IN NON-SUBMERGED AREAS AS WELL. NON-SUBMERGED AREAS ARE DEFINED AS SECTIONS IN THE JOINT THAT ARE A MINIMUM OF ONE (1) FOOT ABOVE THE STANDING WATER LEVEL OF THE BOX CULVERT, AT EITHER PRE-CONSTRUCTION OR CONSTRUCTION PHASE, WHICHEVER IS HIGHER. ALL OTHER AREAS OF THE JOINT ARE CONSIDERED SUBMERGED.
6. AFTER THE INSTALLATION OF THE CONTAINMENT DAM, CHEMICAL GROUT SHALL BE PUMPED BEHIND CULVERT @ 12" SPACING STARTING AT THE MIDDLE OF THE BOTTOM JOINT UNTIL OUTCROPPING IS SEEN OR GROUT ACHIEVES A PRESSURE OF 125 PSI OR AS PER MANUFACTURERS SUGGESTED PRESSURE CRITERIA.
7. OUTCROPPED CHEMICAL GROUT MATERIAL SHALL BE REMOVED, FLUSHED TO JOINT, AND DISPOSED OF PROPERLY.
8. CLEANUP MUST BE DONE WITHOUT INORDINATE USE OF FLAMMABLE OR HAZARDOUS CHEMICALS.
9. THE CONTRACTOR IS RESPONSIBLE FOR REMOVING ANY IMPEDANCE TO FLOW, SUCH AS TEMPORARY COFFERDAMS, SANDBAGS, AND EQUIPMENT FROM THE BOX CULVERTS IN THE EVENT OF RAIN.

HORIZONTAL NOTES:

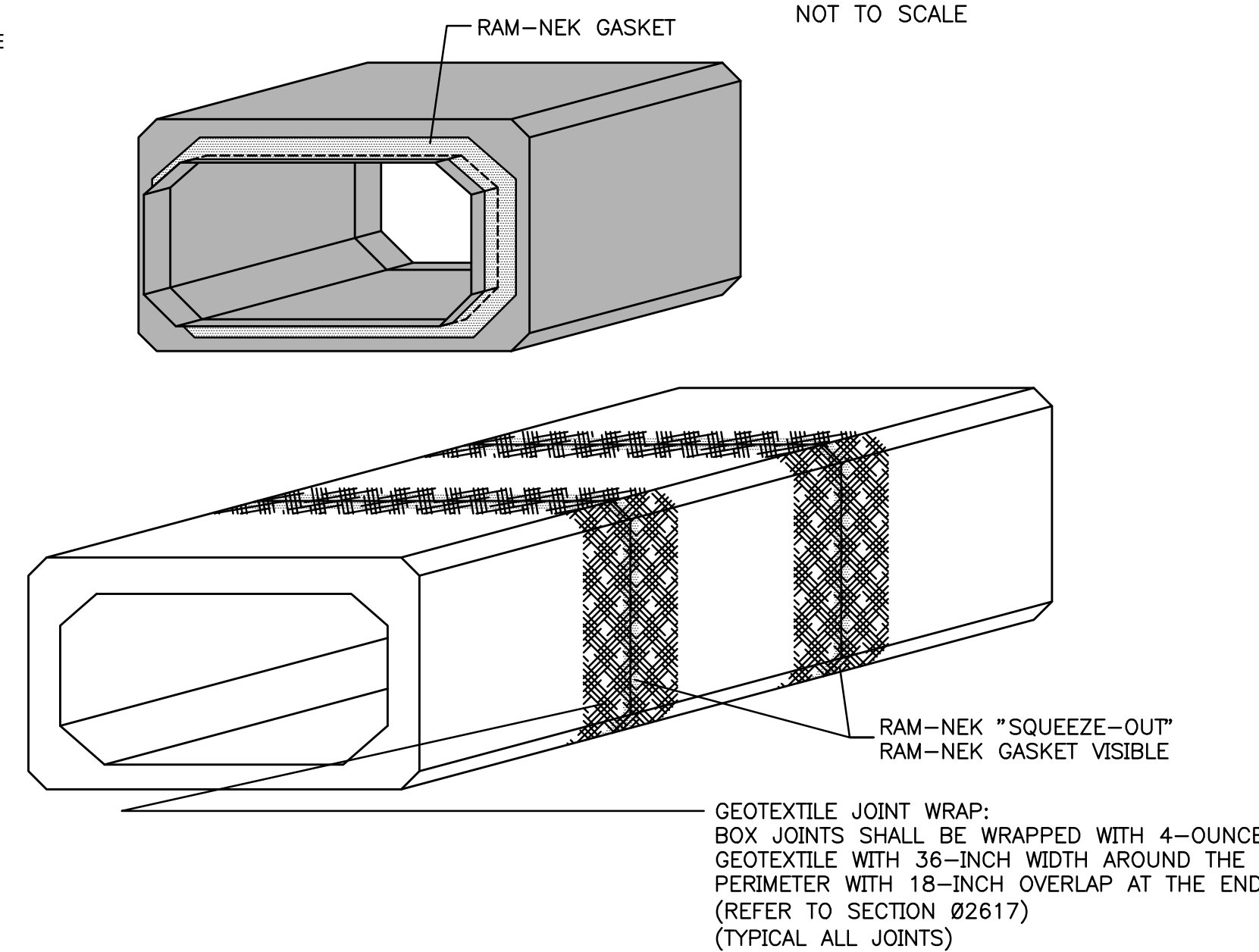
1. TRENCH CONDITIONS SHALL BE SUCH THAT PIPE JOINTING CAN BE ACCOMPLISHED WITHOUT GETTING MUD, SILT, GRAVEL OR OTHER FOREIGN MATERIALS INTO THE JOINT. GENERALLY THE TRENCH SHOULD BE DEWATERED AND HAVE A FIRM BOTTOM FREE OF MUCK.
2. PRIME JOINT AS PER MANUFACTURER'S RECOMMENDATIONS. REMOVE PROTECTIVE WRAPPER ON ONE SIDE OF PREFORMED RAM-NEK STRIP OR COIL AND PRESS FIRMLY TO DRY, CLEAN JOINT SURFACE. BEFORE LAYING THE PIPE IN THE TRENCH, ATTACH THE GASKETS END-TO-END TO THE LEADING EDGE OF THE TONGUE OR GROOVE OF EACH PIPE JOINT, FORMING A CONTINUOUS GASKET AROUND THE CIRCUMFERENCE. REMOVE PROTECTIVE WRAPPER BEFORE JOINING PIPE SECTIONS.
3. AFTER THE GASKET IS APPLIED, THE PIPE SHOULD BE HANDLED CAREFULLY TO AVOID DISPLACING OR SOILING OF GASKET. ANY GASKET SO DISTURBED SHOULD BE REPLACED.
4. THE PIPE SHOULD BE PROPERLY ALIGNED BEFORE JOINTS ARE FORCED HOME. FOR TONGUE AND GROOVE PIPE, THE PIPE SHOULD BE PARTIALLY SUPPORTED TO MAINTAIN CONCENTRICITY UNTIL THE GASKET IS PROPERLY COMPRESSED IN THE JOINT SPACE AND SUFFICIENT PRESSURE APPLIED TO MAKE SURE THAT THE JOINT IS PROPERLY MADE.
5. LIFT HOLE PLUG SHALL BE GROUTED IN PLACE PRIOR TO BACKFILLING.
6. BACKFILLING AND COMPACTION CAN BEGIN WHEN JOINTING & GROUTING ARE COMPLETED.
7. CONTRACTOR SHALL FOLLOW APPLICATION INSTRUCTIONS PROVIDED BY THE MANUFACTURER. THE GAP BETWEEN THE FACE OF THE TONGUE AND GROOVE SHALL NOT EXCEED 1" AFTER JOINTS ARE FORCED HOME. IF JOINT GAP EXCEEDS 1" THEN JOINT SHALL BE REPAIRED AS PER JOINT REPAIR DETAIL AND SPECIFICATION. THIS IS NOT CONSIDERED A 1" AVERAGE. JOINT REPAIR SHALL BE PERFORMED ON SECTIONS OF THE JOINT THAT EXCEED 1". IF MORE THAN HALF THE JOINT EXCEEDS 1", THEN THE WHOLE JOINT SHALL BE REPAIRED (NO SEPARATE PAY SHALL BE MADE FOR JOINT REPAIR).



HORIZONTAL APPLICATION

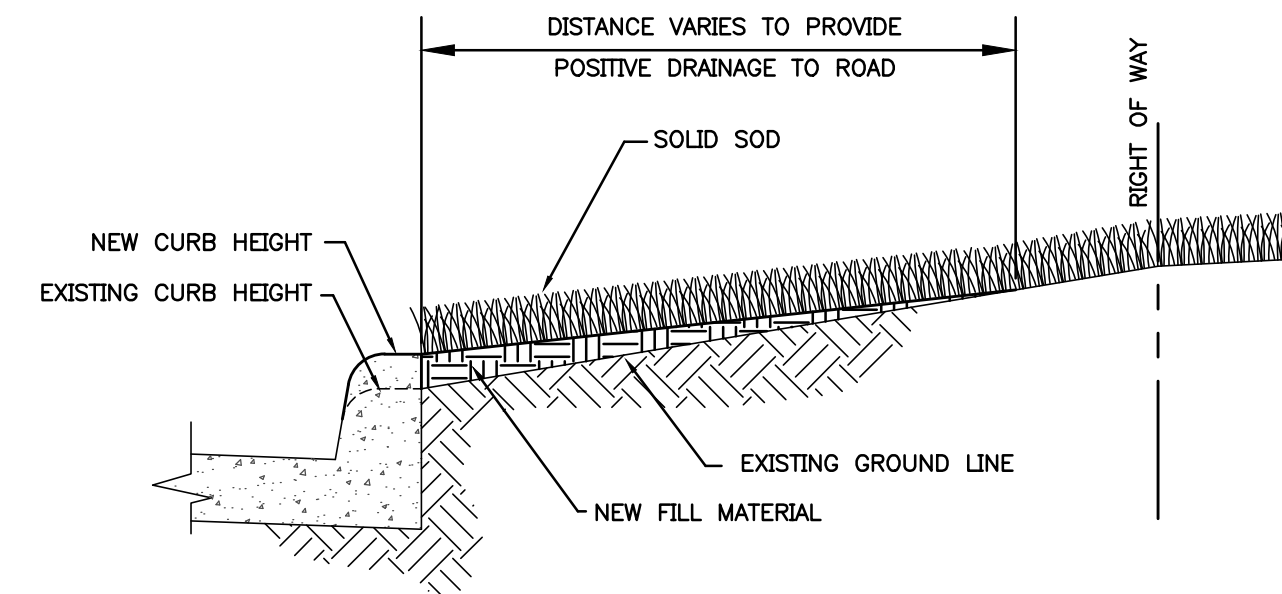
RAM-NEK GASKET INSTALLATION DETAIL

NOT TO SCALE



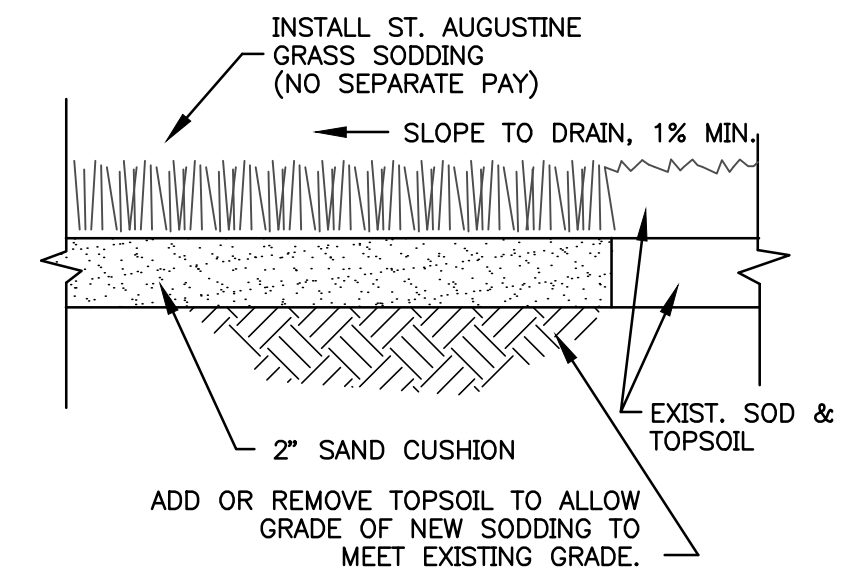
RAM-NEK DETAIL

NOT TO SCALE



FILL BEHIND BACK OF CURB DETAIL

NOT TO SCALE



NOTES:

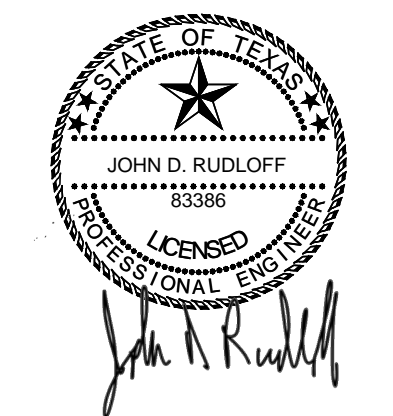
1. SODDING SHALL BE ON AREAS DISTURBED BY CONSTRUCTION.
2. SODDING SHALL BE ON AREAS DISTURBED BY CONSTRUCTION.
3. SODDING SHALL BE ON AREAS DISTURBED BY CONSTRUCTION.
4. IN THE EVENT EXISTING LANDSCAPING OTHER THAN GRASS IS WITHIN THESE AREAS, THE CONTRACTOR SHALL REBUILD OR REINSTALL THE LANDSCAPING OF THE AREA AFTER CONSTRUCTION IN AN EQUAL OR BETTER CONDITION.

TYPICAL GRASS SODDING DETAILS

NOT TO SCALE

NO.	DATE	BY	CHK.

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19



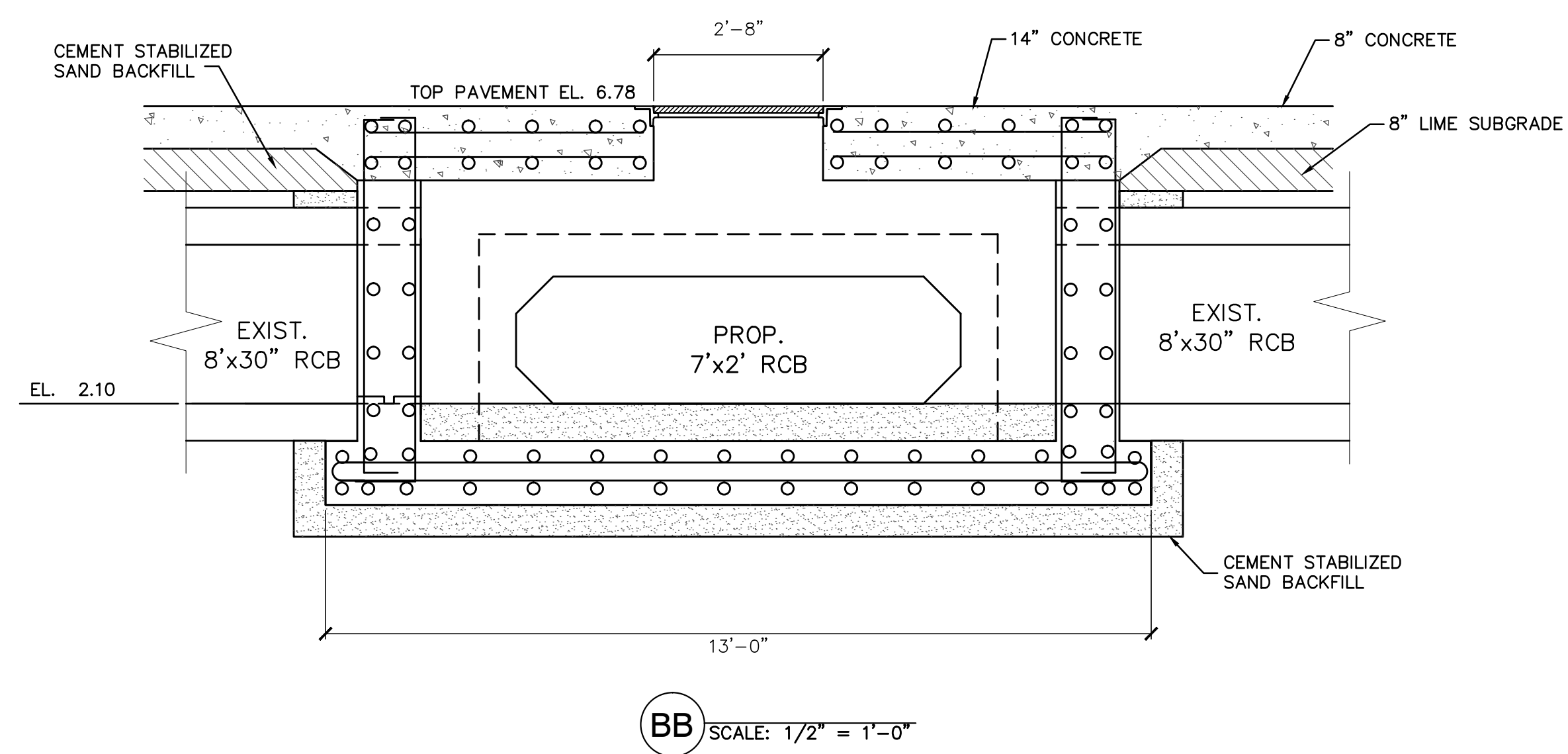
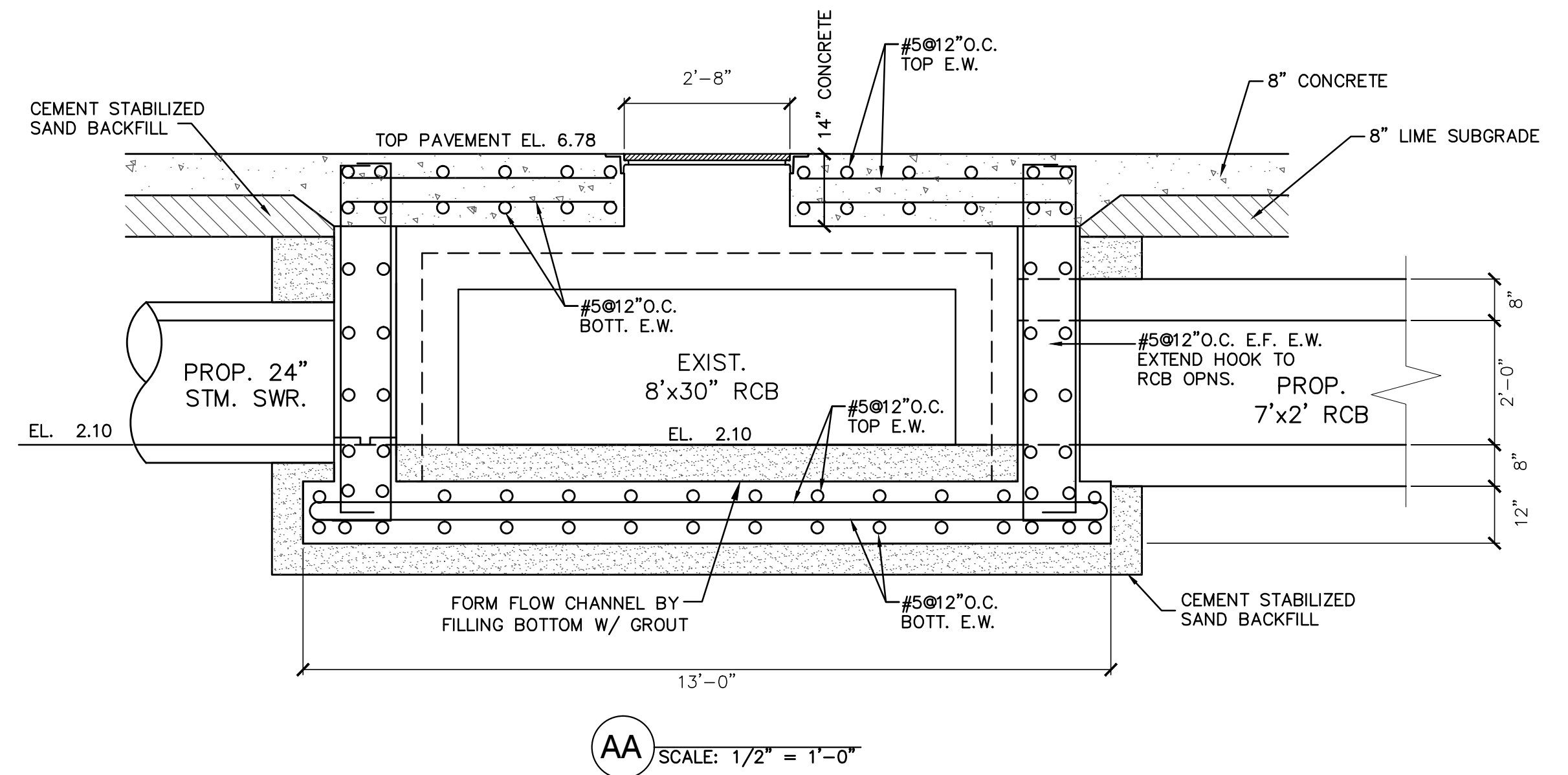
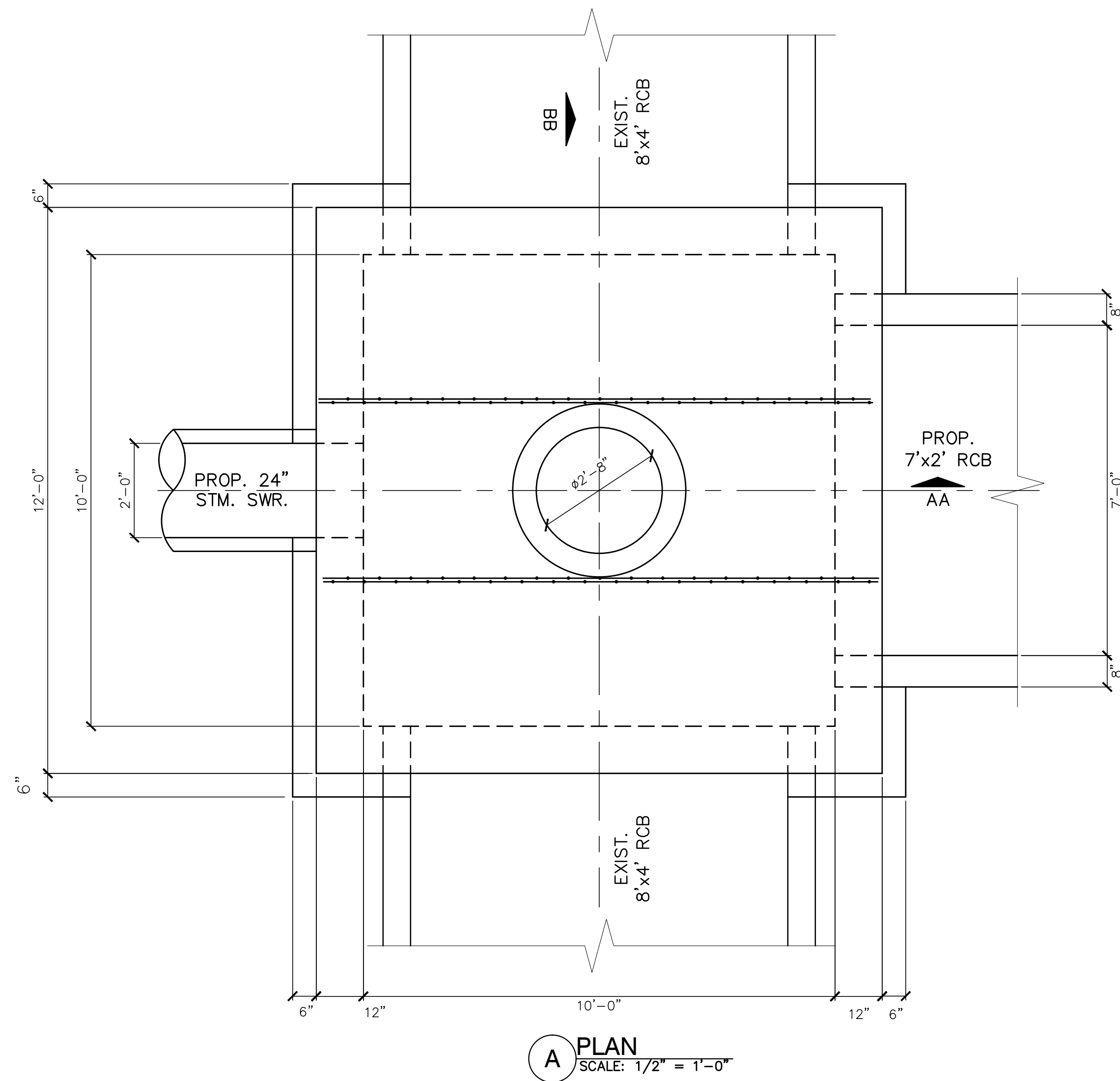
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Galveston County, Texas

Texas Avenue Reconstruction

Drainage Details IV

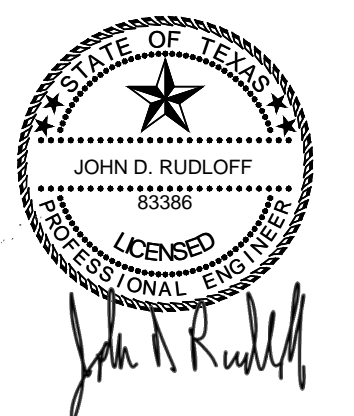
Job No.: 18-015	Scale:	SHEET
Date: September, 2019	HORZ:	43
Dwn By: D. Fattig	VERT: N/A	
Chkd By: J Rudloff		OF 52



NOTES:

1. REFER SHEET 50 FOR GENERAL NOTES.
2. REFER SHEET 51 FOR TYPICAL DETAILS.
3. PROVIDE ADDITIONAL REINFORCING IN WALLS OF THE JUNCTION BOX RECEIVING PIPES PER DETAIL 6/51.
4. PROVIDE ADDITIONAL REINFORCING AT TOP & BOTTOM BEAM/SLAB OF JUNCTION BOX ABOVE AND BELOW THE TOP AND BOTTOM SLAB OR PRECAST BOX PER DETAILS 8/51 & 9/51.
5. REFER DETAIL 13/51 FOR WALLS RECEIVING PRECAST BOX.

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19



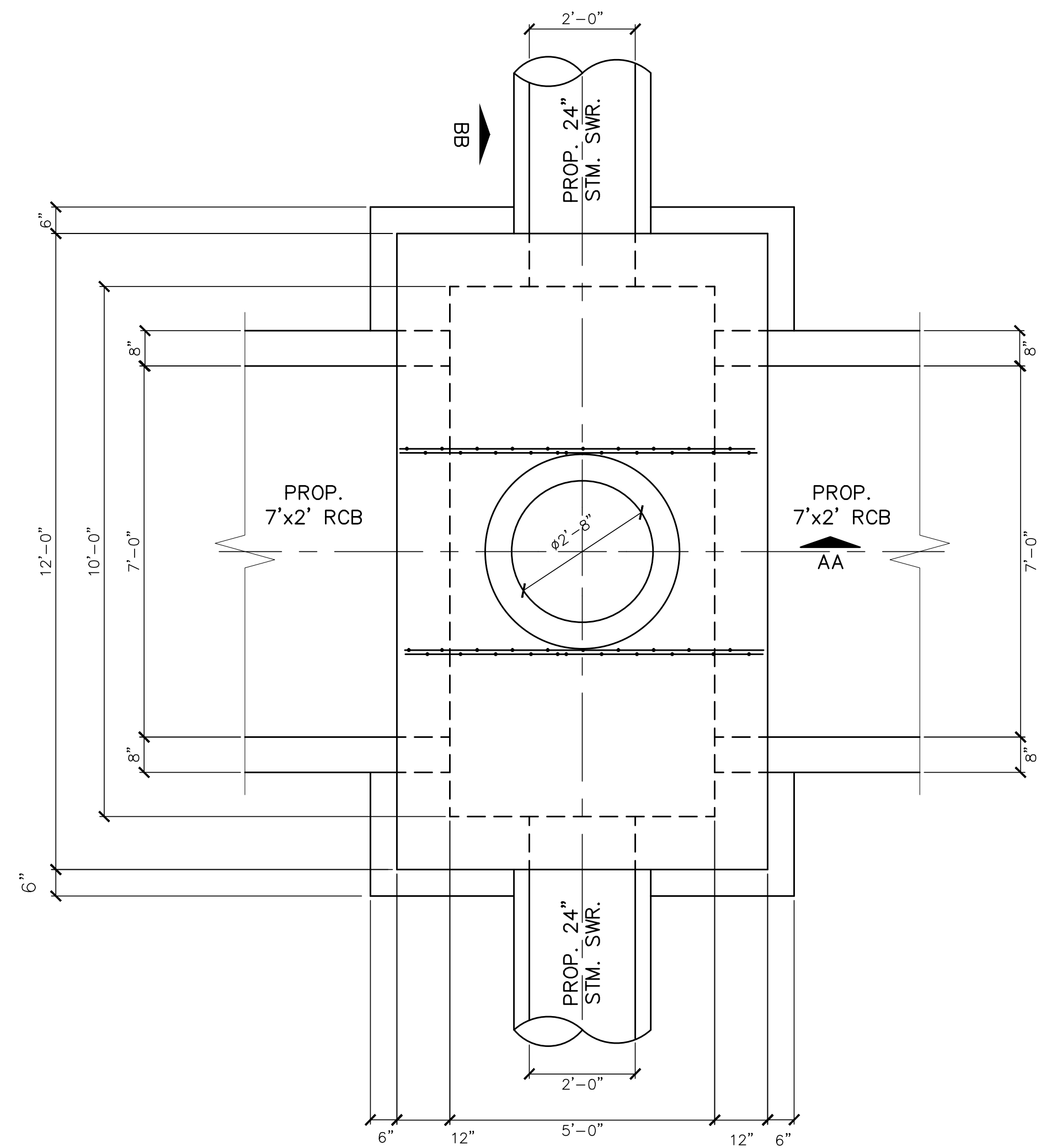
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Galveston County, Texas

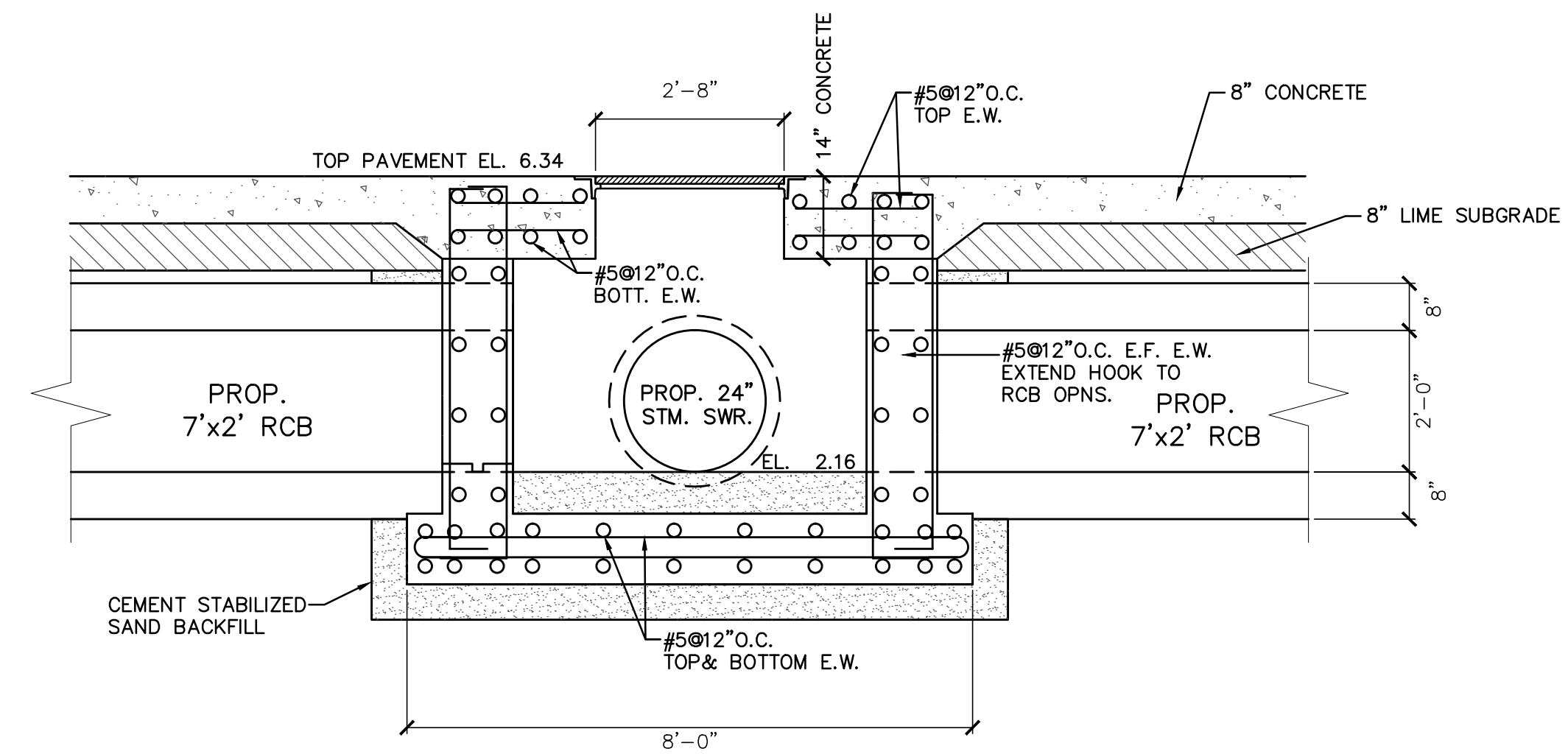
Texas Avenue Reconstruction

Junction Box A1 - Sta. 4+19.10

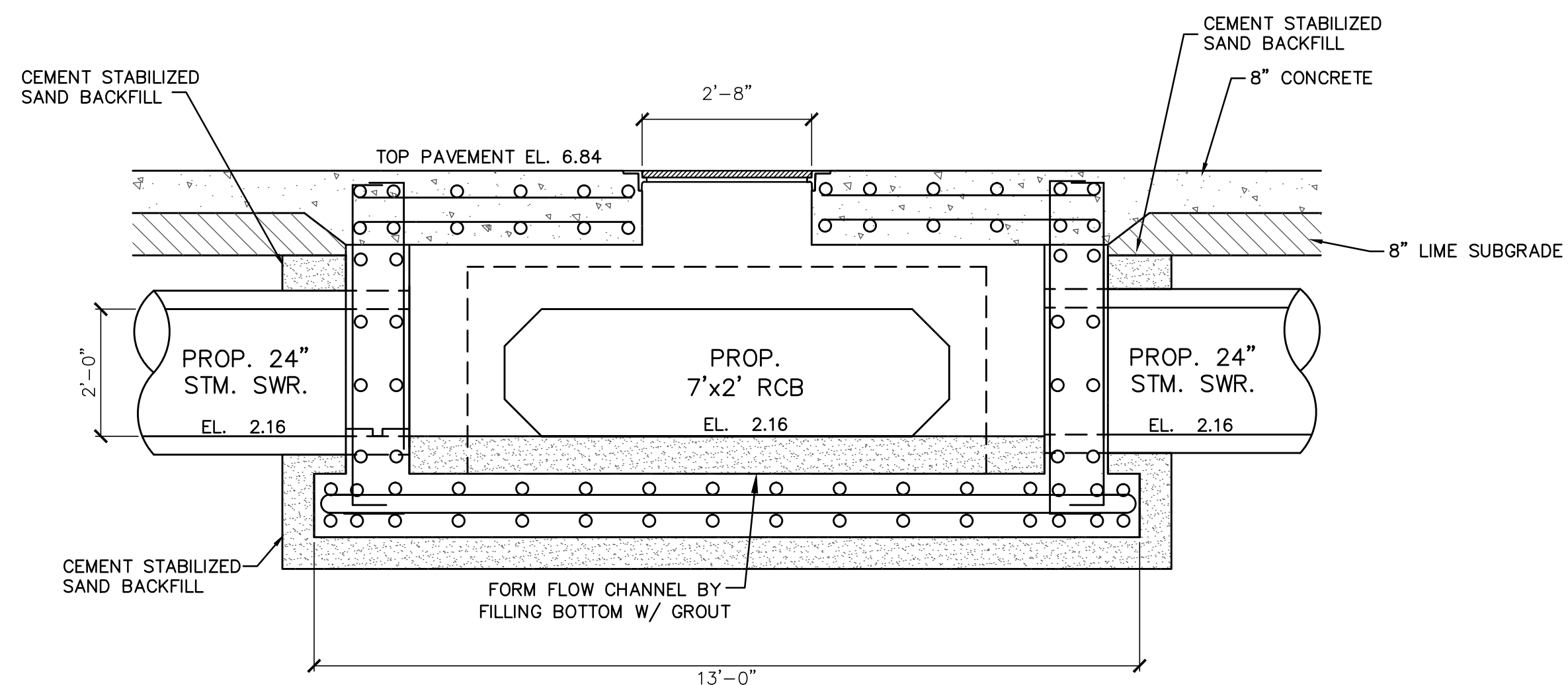
Job No.: 18-015	Scale: HORZ 1/2" = 1'-0"	SHEET
Date: September, 2019	VERT: 1/2" = 1'-0"	44
Dwn By: D. Fattig		
Chkd By: J Rudloff		OF 52



A PLAN
SCALE: 1/2" = 1'-0"



AA SCALE: 1/2" = 1'-0"

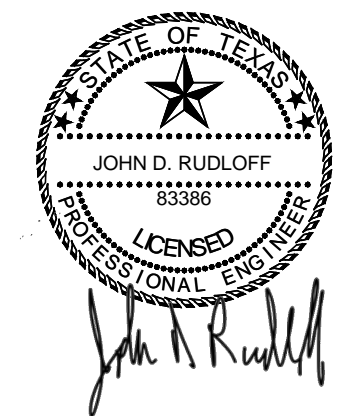


BB SCALE: 1/2" = 1'-0"

NOTES:

1. REFER SHEET 50 FOR GENERAL NOTES.
2. REFER SHEET 51 FOR TYPICAL DETAILS.
3. PROVIDE ADDITIONAL REINFORCING IN WALLS OF THE JUNCTION BOX RECEIVING PIPES PER DETAIL 6/51.
4. PROVIDE ADDITIONAL REINFORCING AT TOP & BOTTOM BEAM/SLAB OF JUNCTION BOX ABOVE AND BELOW THE TOP AND BOTTOM SLAB OR PRECAST BOX PER DETAILS 8/51 & 9/51.
5. REFER DETAIL 13/51 FOR WALLS RECEIVING PRECAST BOX.

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19



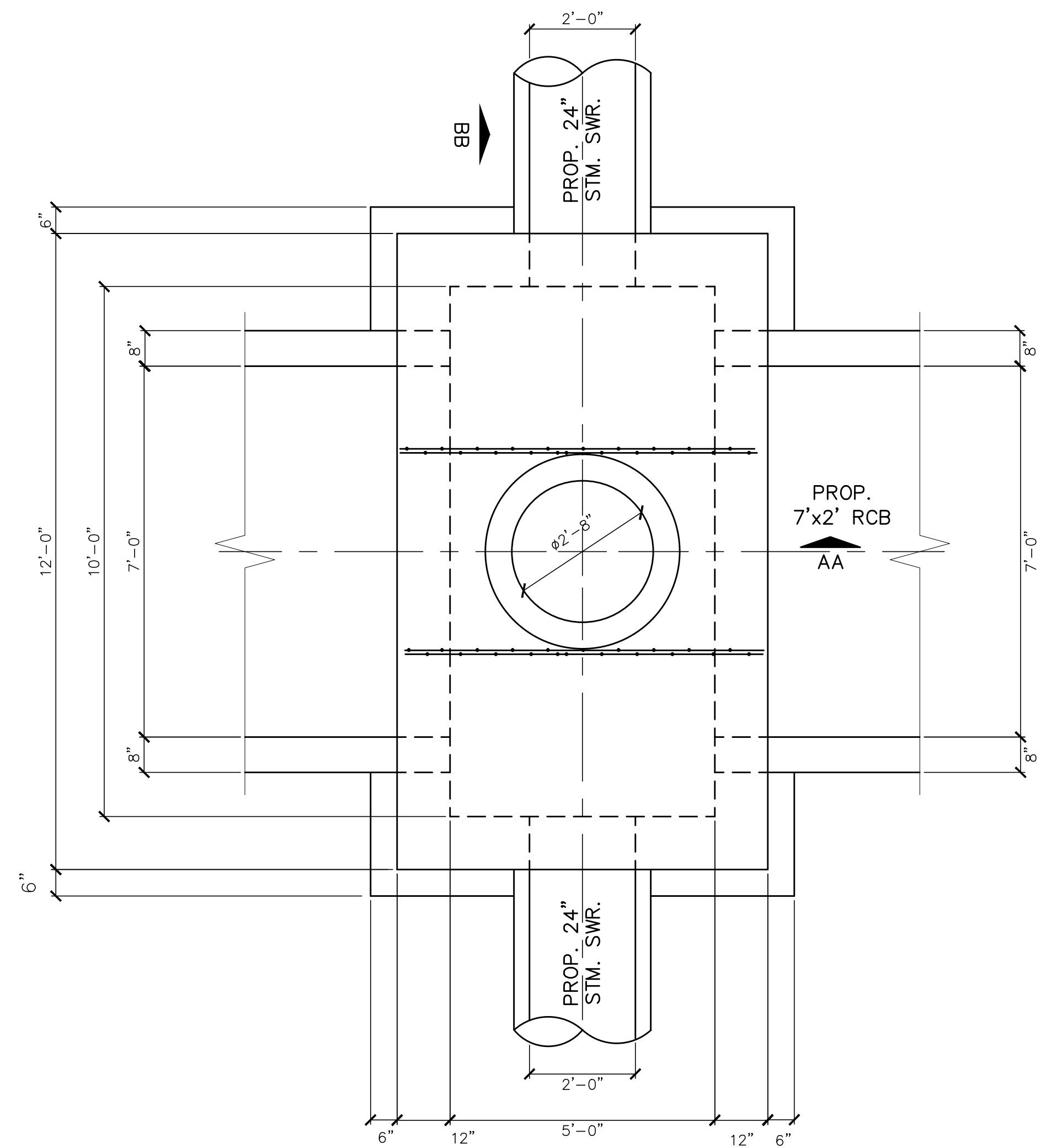
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(713) 400-2755 • www.arkkengineers.com • TX PE Firm No. 13872

Galveston County, Texas

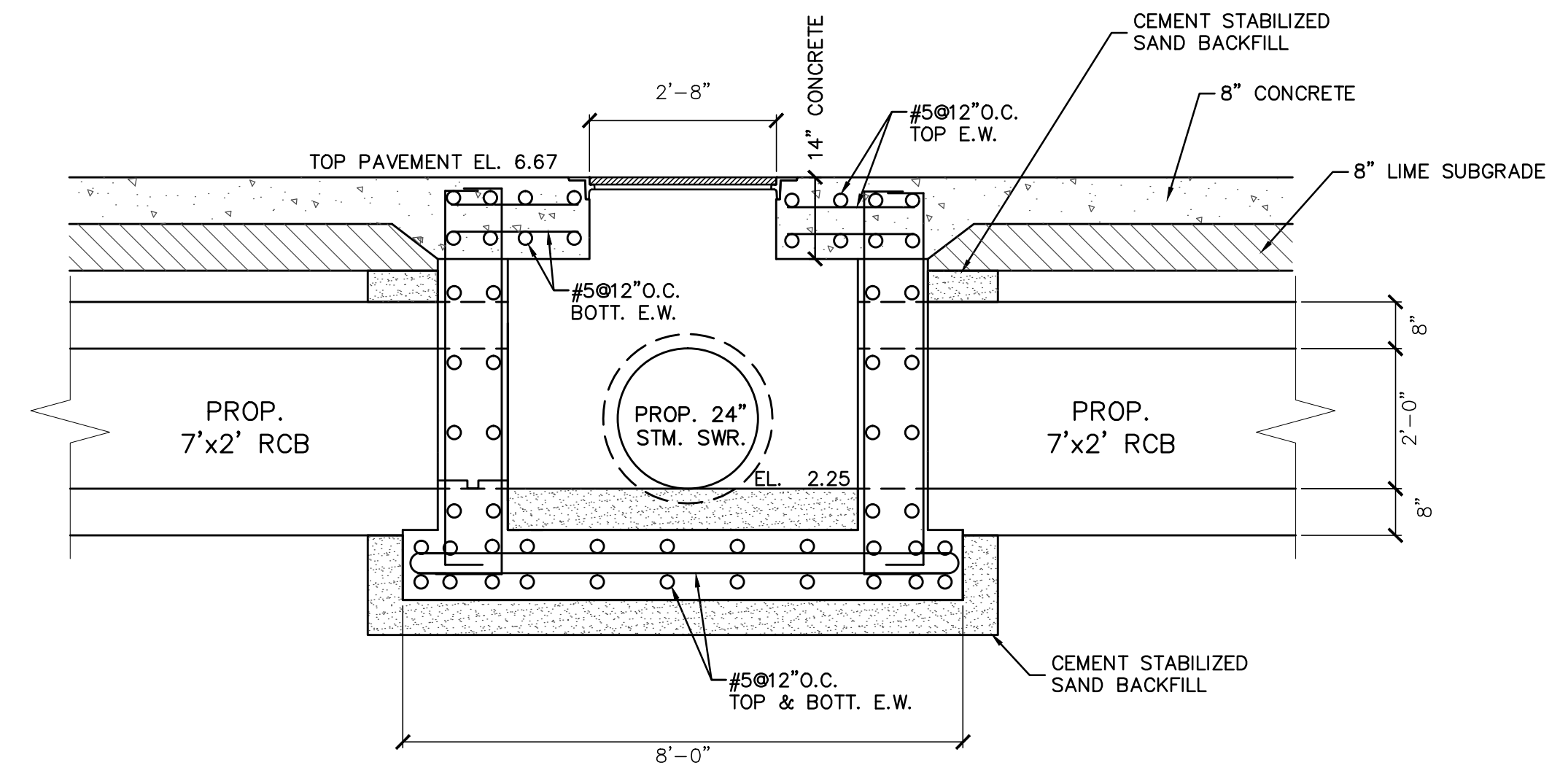
Texas Avenue Reconstruction

Junction Box A2 - Sta. 5+45.00

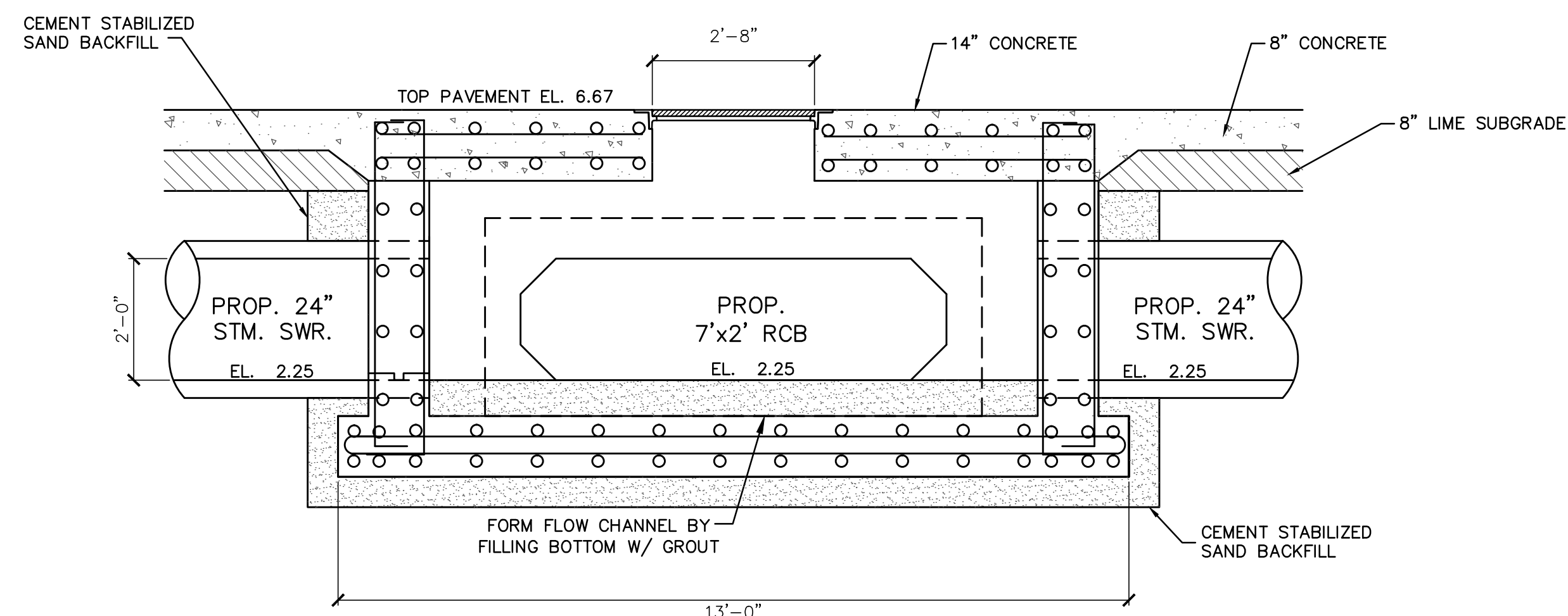
Job No.: 18-015	Scale: HORZ 1/2" = 1'-0"	SHEET
Date: September, 2019	VERT: 1/2" = 1'-0"	45
Dwn By: D. Fattig		OF 52
Chkd By: J Rudloff		



A PLAN
SCALE: 1/2" = 1'-0"



AA SCALE: 1/2" = 1'-0"

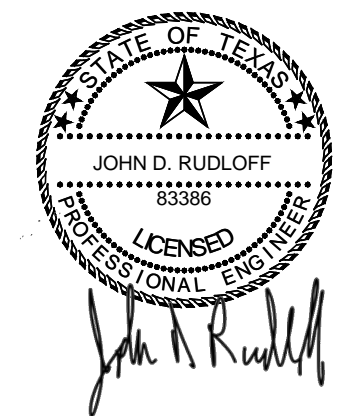


BB SCALE: 1/2" = 1'-0"

NOTES:

1. REFER SHEET 50 FOR GENERAL NOTES.
2. REFER SHEET 51 FOR TYPICAL DETAILS.
3. PROVIDE ADDITIONAL REINFORCING IN WALLS OF THE JUNCTION BOX RECEIVING PIPES PER DETAIL 6/51.
4. PROVIDE ADDITIONAL REINFORCING AT TOP & BOTTOM BEAM/SLAB OF JUNCTION BOX ABOVE AND BELOW THE TOP AND BOTTOM SLAB OR PRECAST BOX PER DETAILS 8/51 & 9/51.
5. REFER DETAIL 13/51 FOR WALLS RECEIVING PRECAST BOX.

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19



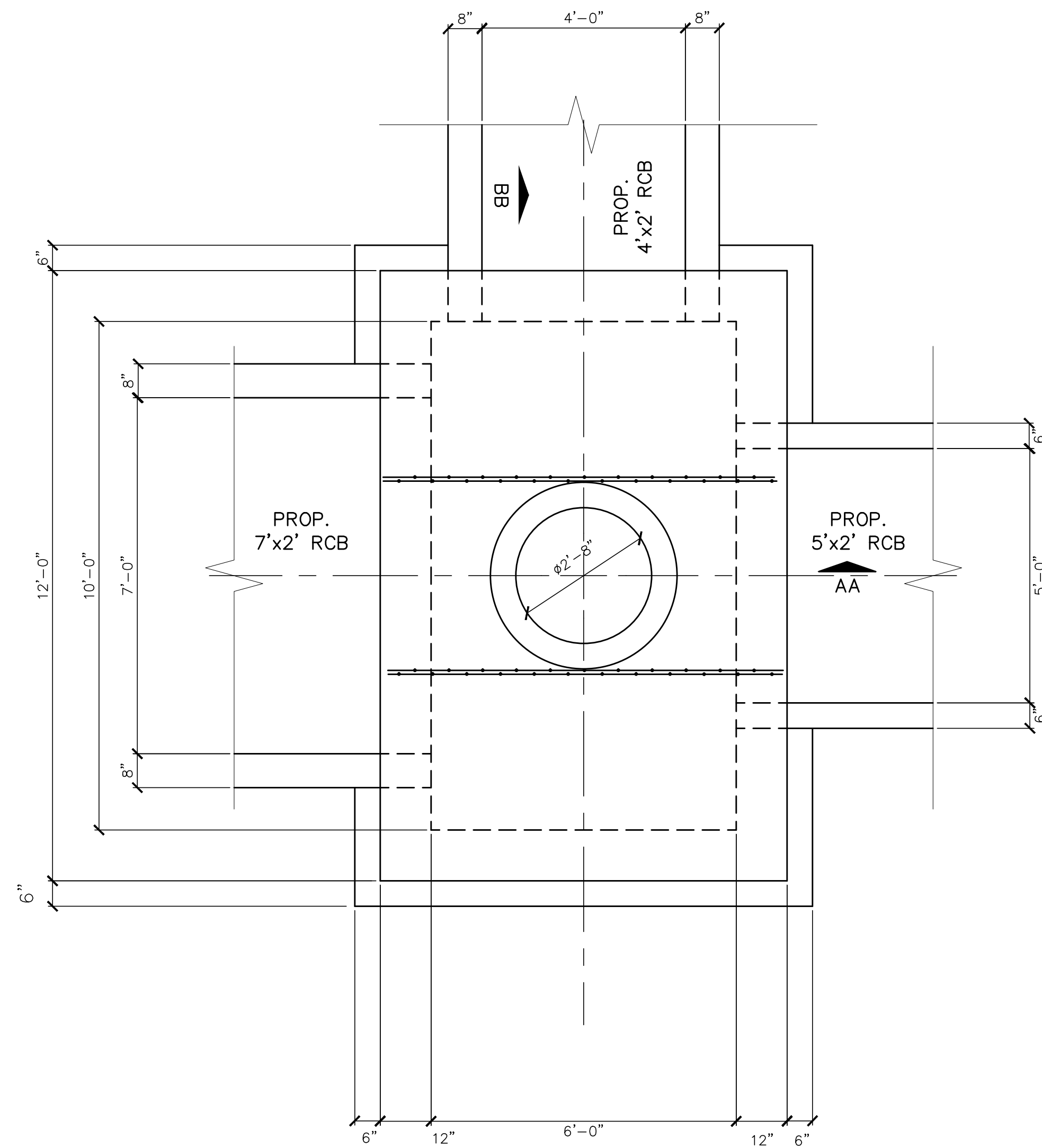
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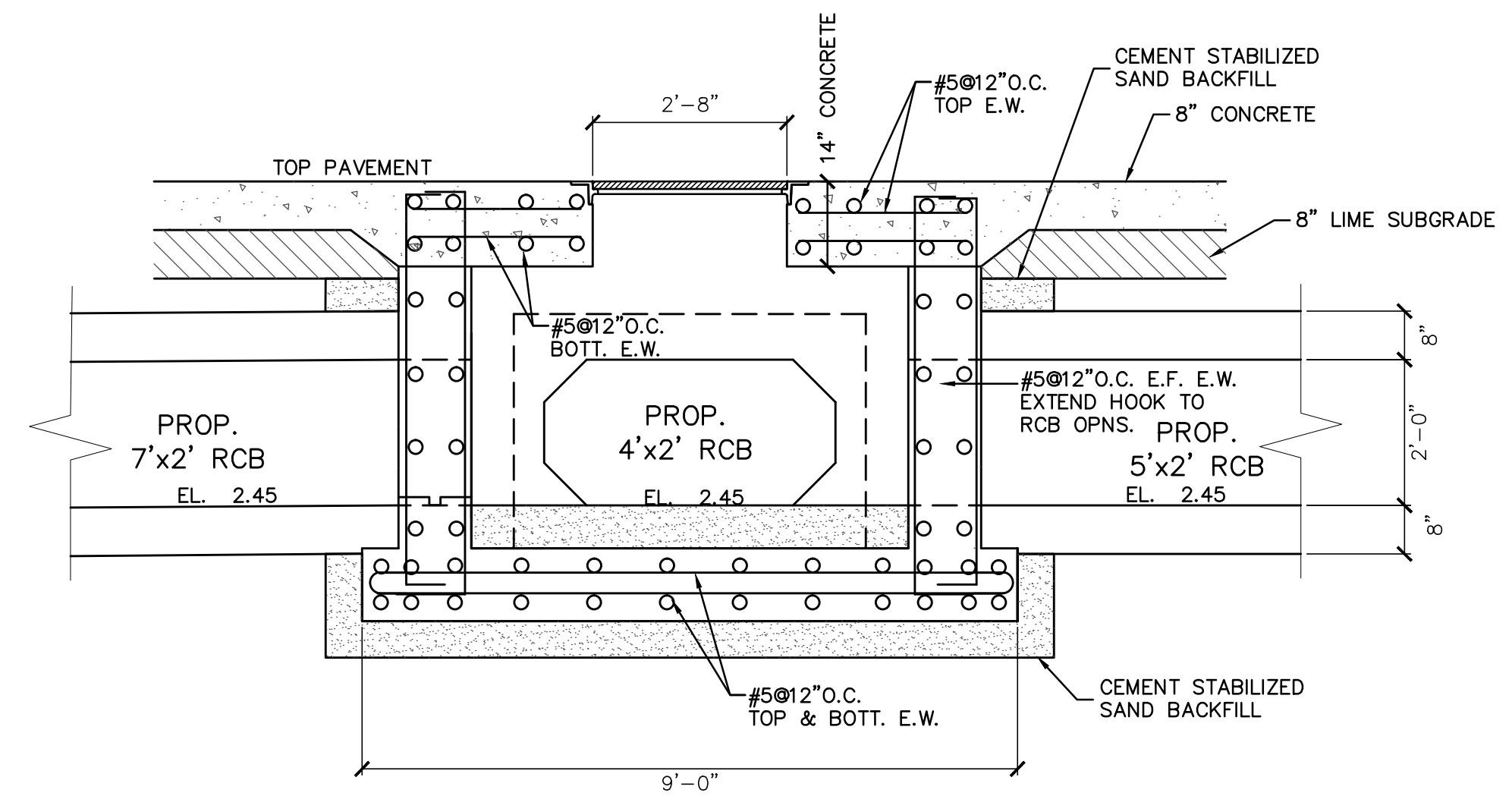
Texas Avenue Reconstruction

Junction Box #A3 - Sta. 7+26.00

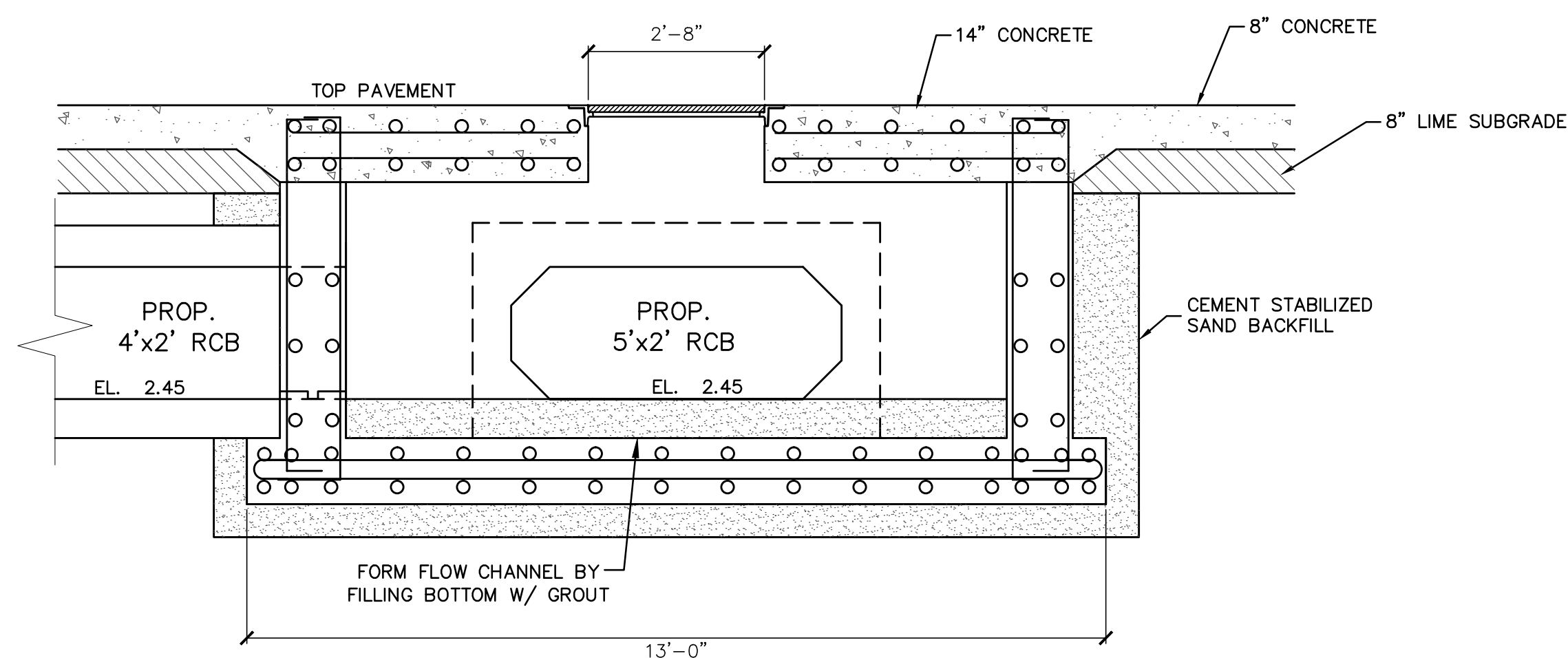
Job No.: 18-015	Scale: HORZ 1/2" = 1'-0"	SHEET
Date: September, 2019	VERT: 1/2" = 1'-0"	46
Dwn By: D. Fattig		OF 52
Chkd By: J Rudloff		



A PLAN
SCALE: 1/2" = 1'-0"



AA SCALE: 1/2" = 1'-0"

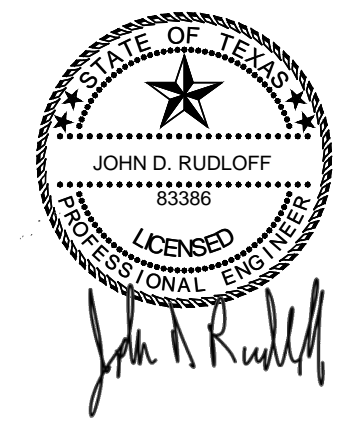


BB SCALE: 1/2" = 1'-0"

NOTES:

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2. REFER SHEET 51 FOR TYPICAL DETAILS.
3. PROVIDE ADDITIONAL REINFORCING IN WALLS OF THE JUNCTION BOX RECEIVING PIPES PER DETAIL 6/51.
4. PROVIDE ADDITIONAL REINFORCING AT TOP & BOTTOM BEAM/SLAB OF JUNCTION BOX ABOVE AND BELOW THE TOP AND BOTTOM SLAB OR PRECAST BOX PER DETAILS 8/51 & 9/51.
5. REFER DETAIL 13/51 FOR WALLS RECEIVING PRECAST BOX.

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19



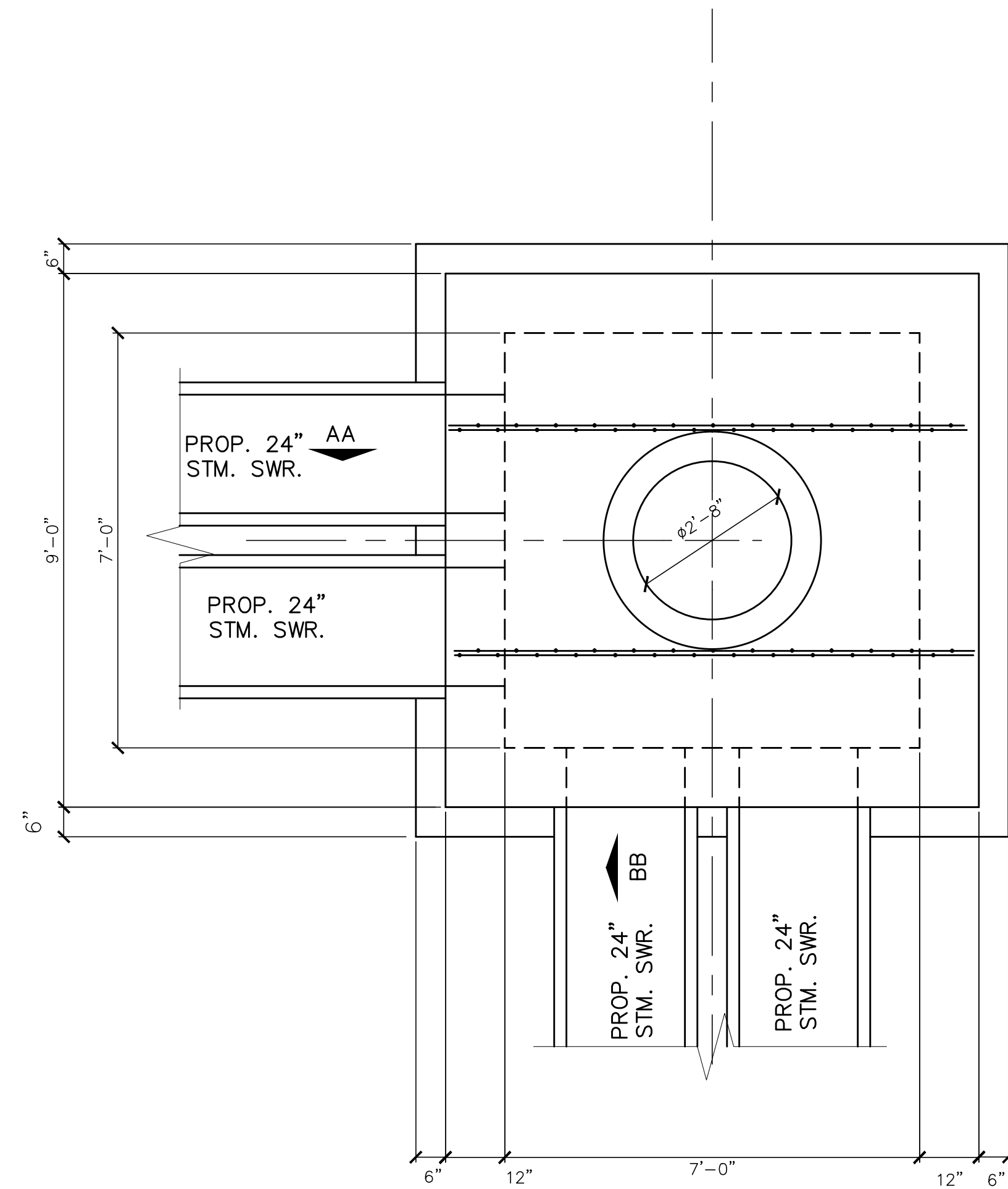
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Galveston County, Texas

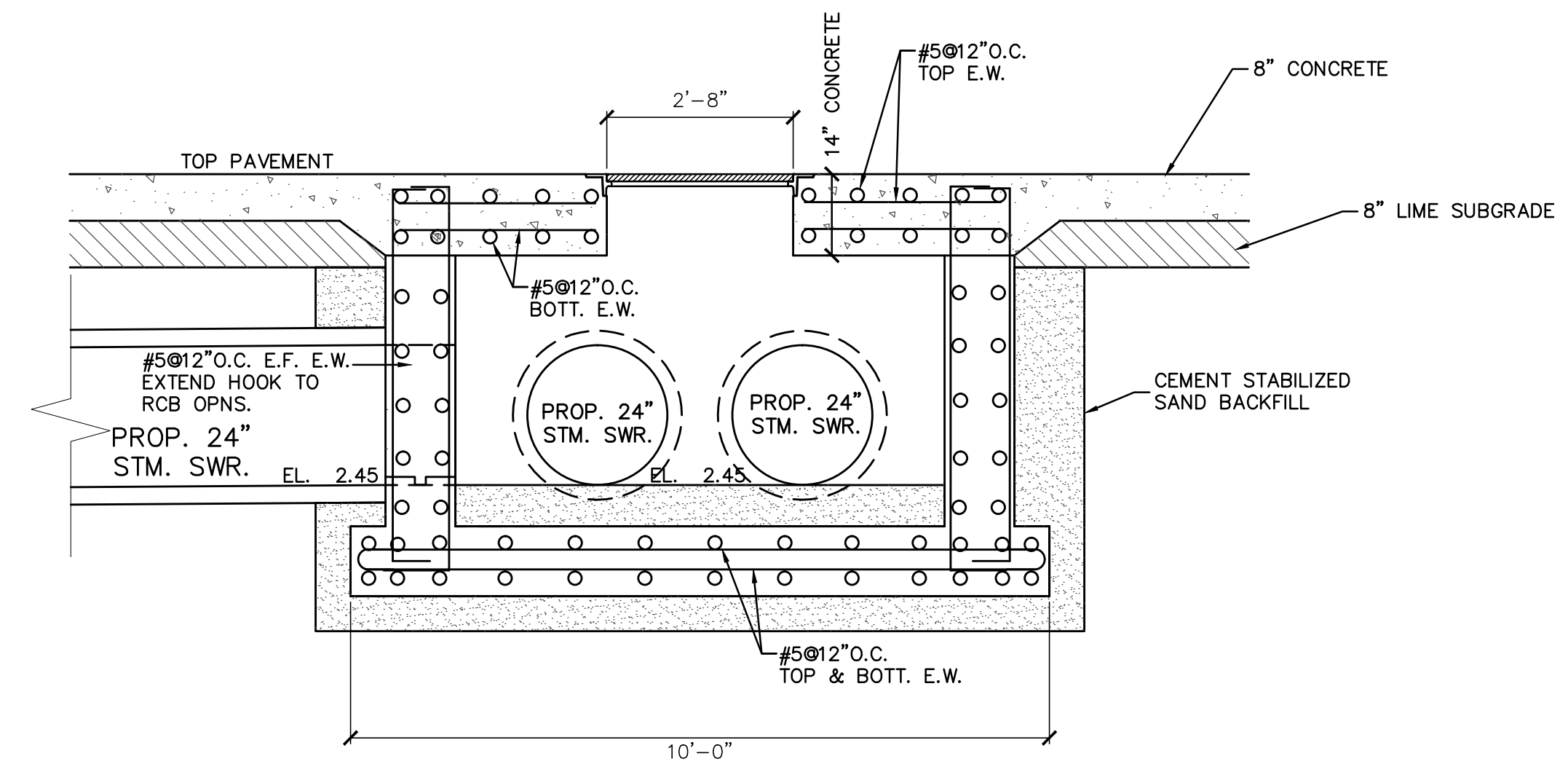
Texas Avenue Reconstruction

Junction Box A4 - Sta. 11+30.00

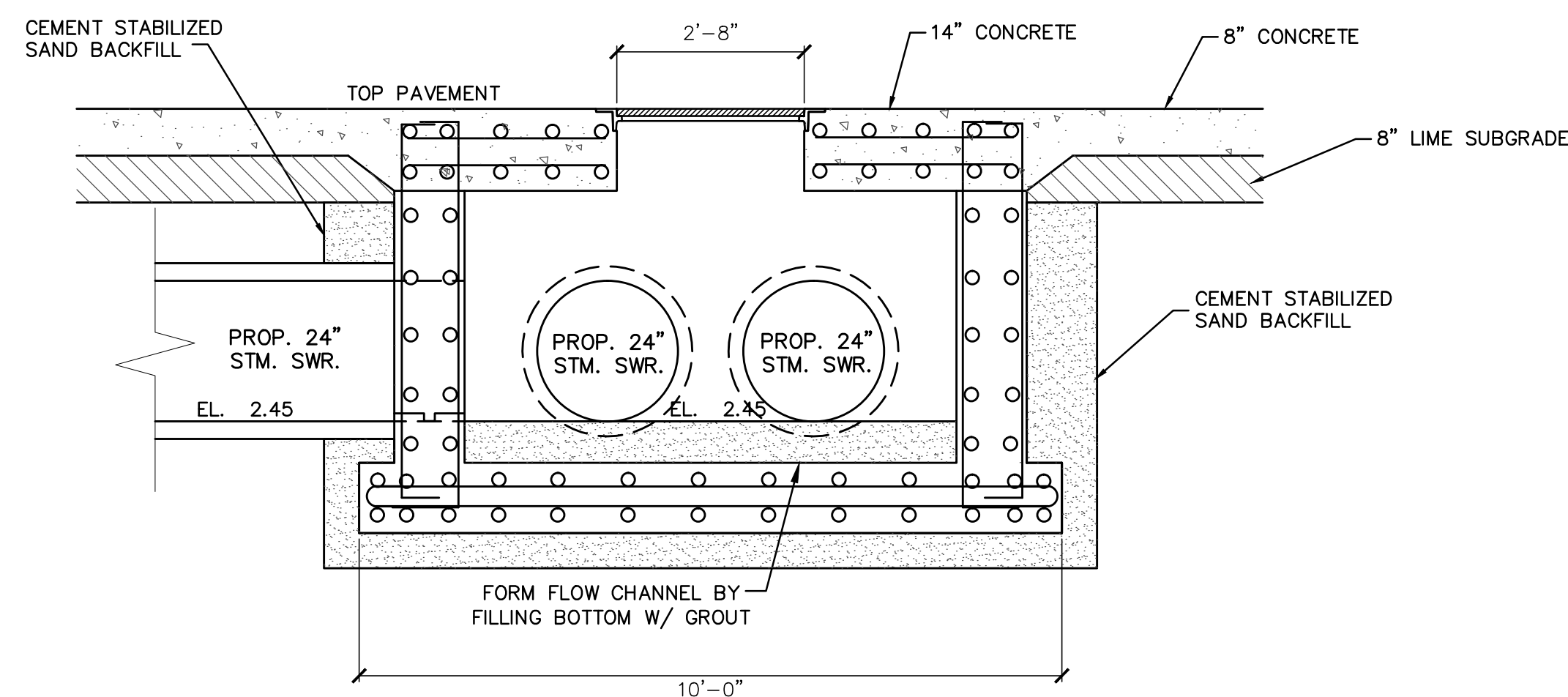
Job No.: 18-015	Scale: HORIZ 1/2" = 1'-0"	SHEET
Date: September, 2019	VERT: 1/2" = 1'-0"	47
Dwn By: D. Fattig		
Chkd By: J Rudloff		OF 52



A PLAN
SCALE: 1/2" = 1'-0"



AA SCALE: 1/2" = 1'-0"

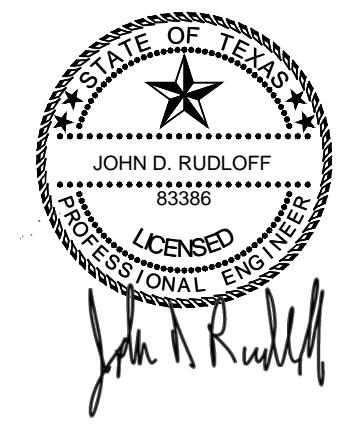


BB SCALE: 1/2" = 1'-0"

NOTES:

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5. REFER DETAIL 13/51 FOR WALLS RECEIVING PRECAST BOX.

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19



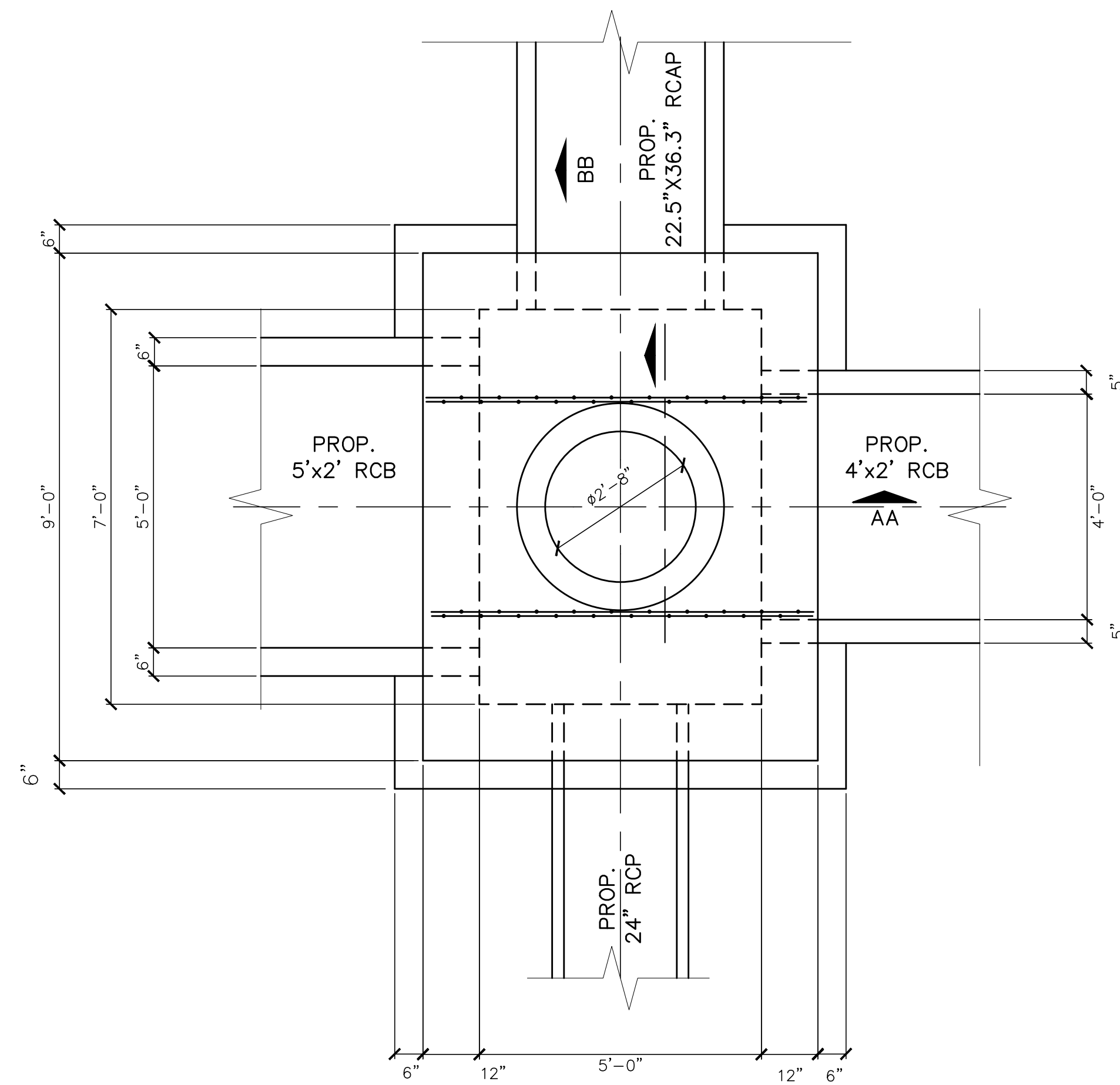
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Galveston County, Texas

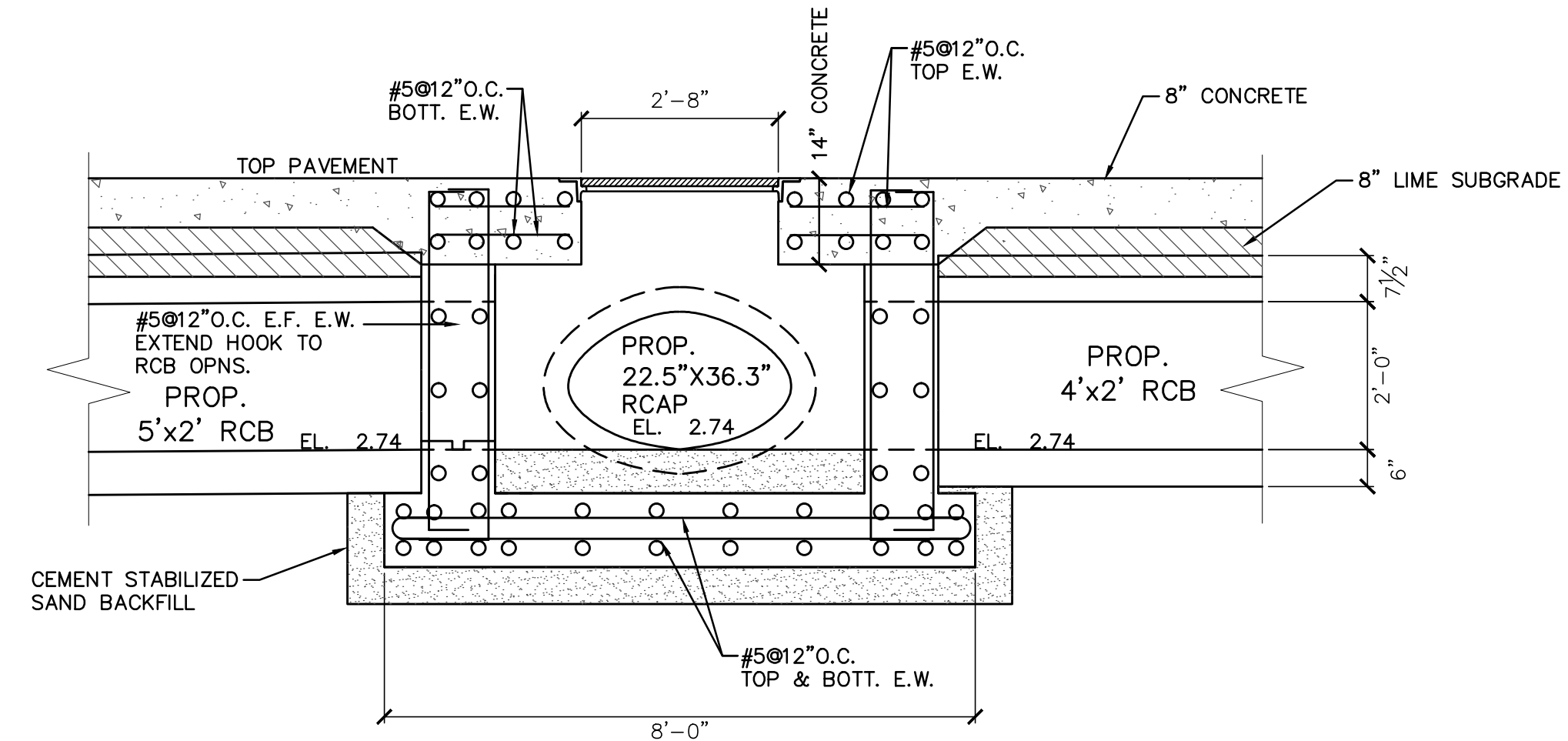
Texas Avenue Reconstruction

Junction Box A5 - Sta. 11+28.50

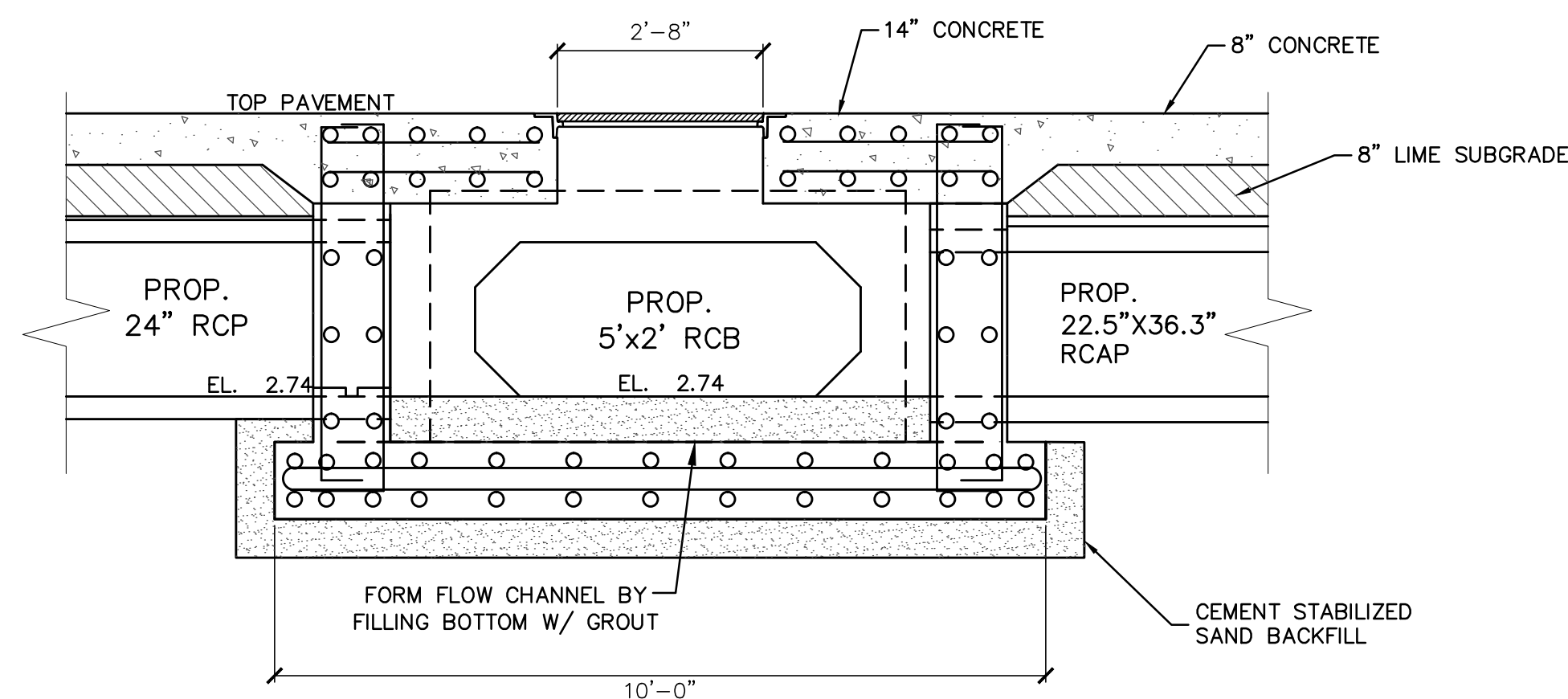
Job No.: 18-015	Scale: HORIZ 1/2" = 1'-0"	SHEET 48 OF 52
Date: September, 2019	VERT:	
Dwn By: D. Fattig		
Chkd By: J Rudloff		



A PLAN
SCALE: 1/2" = 1'-0"



AA SCALE: 1/2" = 1'-0"

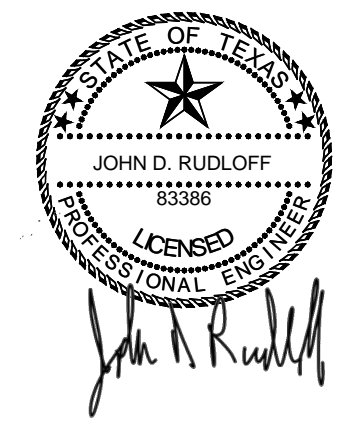


BB SCALE: 1/2" = 1'-0"

NOTES:

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2. REFER SHEET 51 FOR TYPICAL DETAILS.
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5. REFER DETAIL 13/51 FOR WALLS RECEIVING PRECAST BOX.

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19



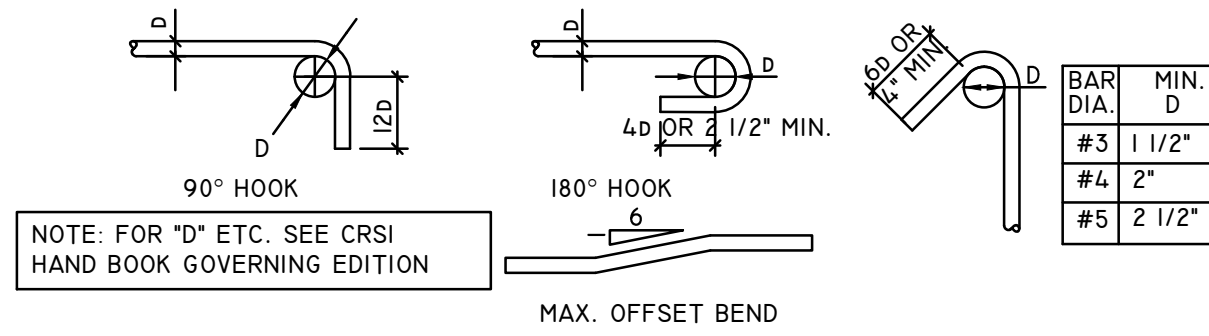
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Galveston County, Texas

Texas Avenue Reconstruction

Junction Box A6 - Sta. 17+15.00

Job No.: 18-015	Scale: HORIZ 1/2" = 1'-0"	SHEET
Date: September, 2019	VERT: 1/2" = 1'-0"	49
Dwn By: D. Fattig		OF 52
Chkd By: J Rudloff		



1 Bar Bending Details
SCALE: N.T.S.

MINIMUM TENSION EMBEDMENT LENGTHS 'LDH' FOR STANDARD HOOKS -GRADE 60 (FY-60,000PSI) REINFORCING BARS

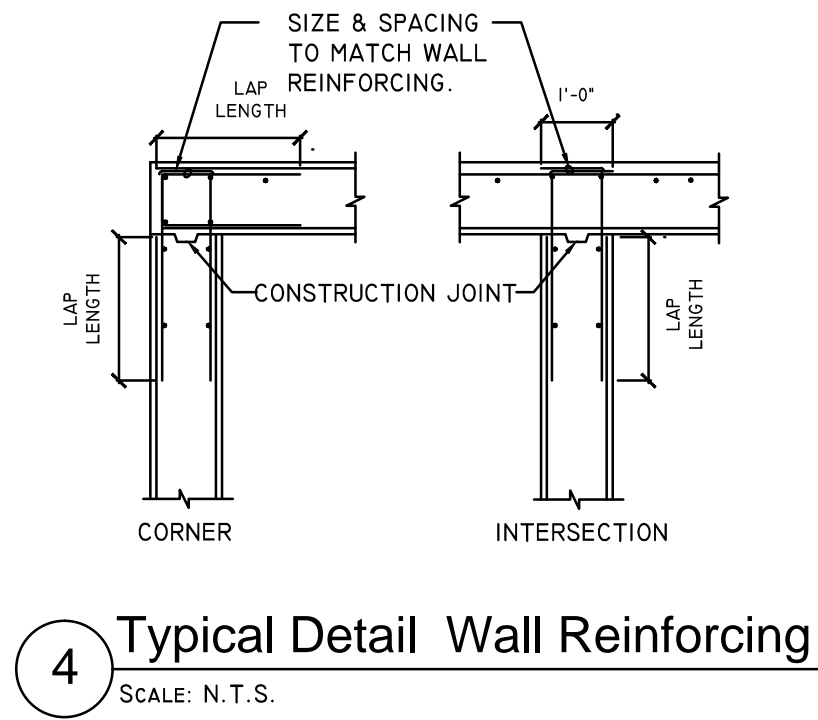
BAR SIZE	NORMAL WEIGHT CONCRETE F'c=3000 PSI	F'c=4000 PSI
#3	6	6
#4	8	7
#5	10	9
#6	12	10
#7	14	12
#8	16	14
#9	18	15
#10	20	17
#11	22	19

2 Reinforcing 'LDH' Lengths
SCALE: N.T.S.

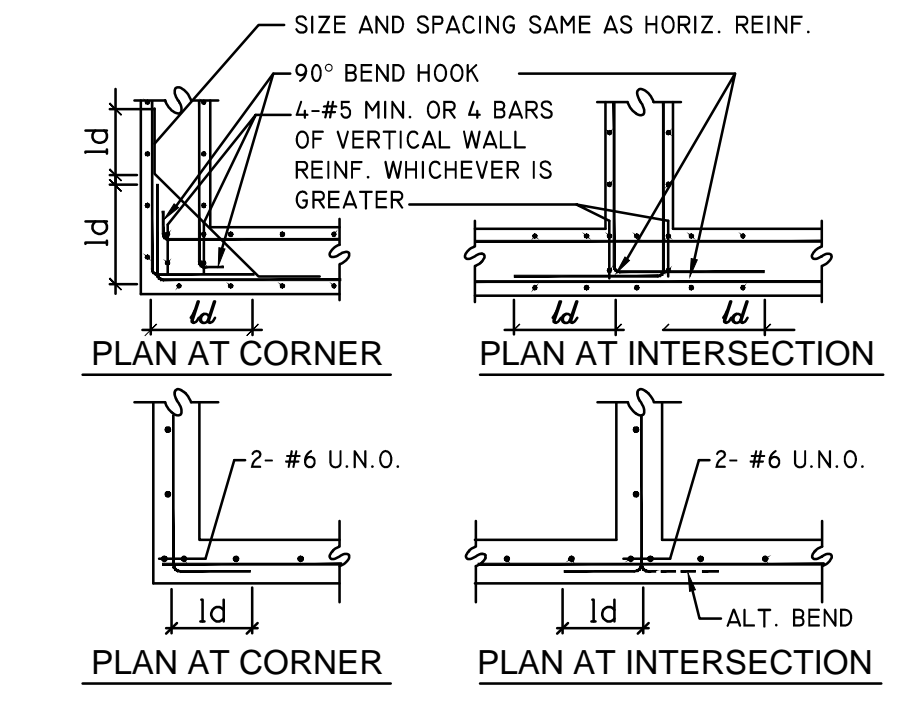
SPLICE LENGTH NORMAL WEIGHT CONC. (REFER NOTES BELOW)

BAR SIZE	LAP CLASS	F'c=3000 PSI		F'c=4000 PSI	
		TOP	OTHER	TOP	OTHER
#3	A	22	17	19	15
	B	28	22	24	19
#4	A	29	22	25	19
	B	37	29	32	25
#5	A	36	28	31	24
	B	47	36	40	31
#6	A	43	33	37	29
	B	56	43	48	37
#7	A	63	48	54	42
	B	81	63	70	54
#8	A	72	55	62	48
	B	93	72	80	62
#9	A	81	62	70	54
	B	105	81	91	70
#10	A	91	70	79	61
	B	118	91	102	79
#11	A	101	78	87	67
	B	131	101	113	87

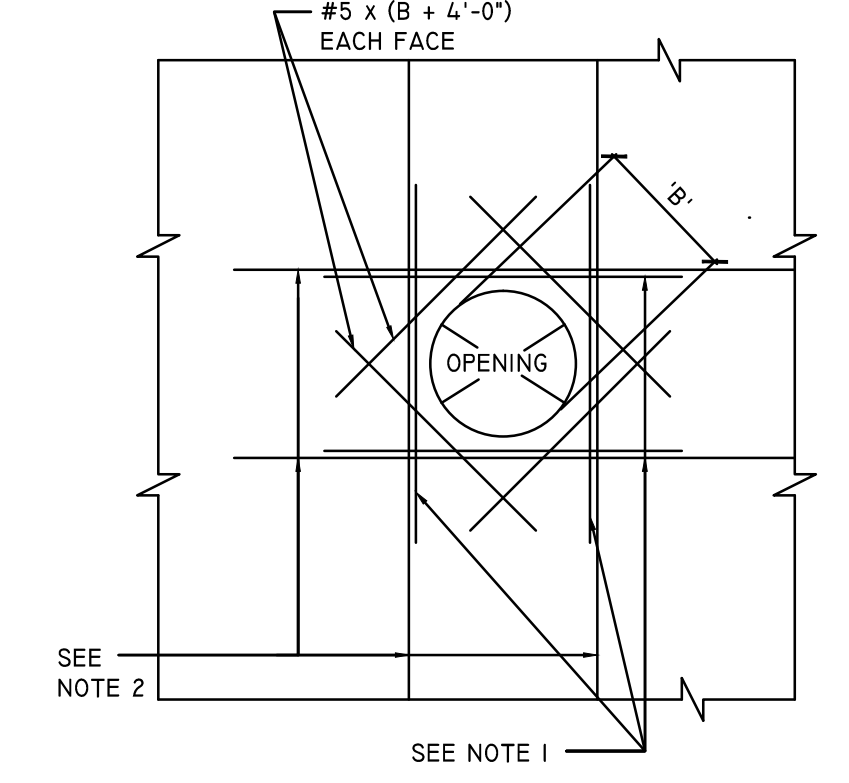
3 Reinforcing Lap Lengths- LD
SCALE: N.T.S.



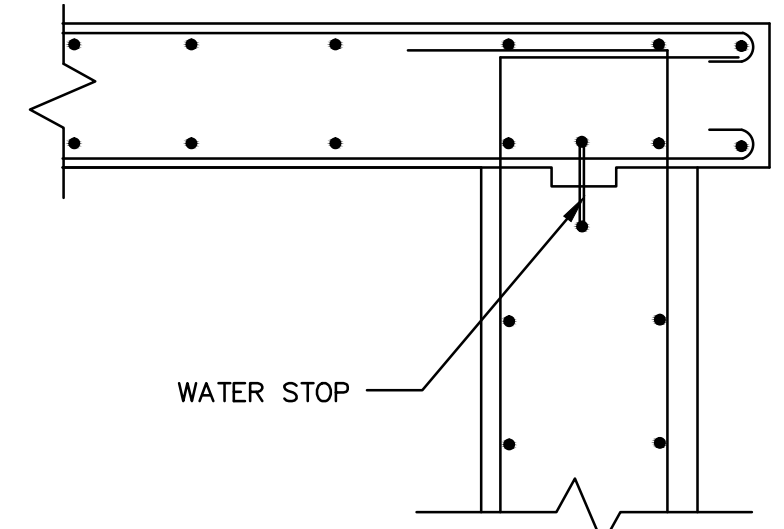
4 Typical Detail Wall Reinforcing
SCALE: N.T.S.



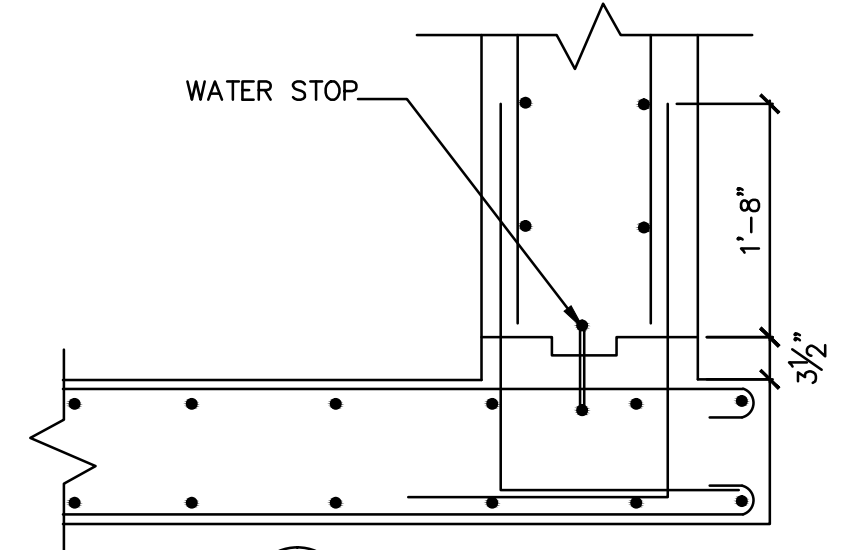
5 Typical Detail - Wall Or Beam Corner Bars
SCALE: N.T.S.



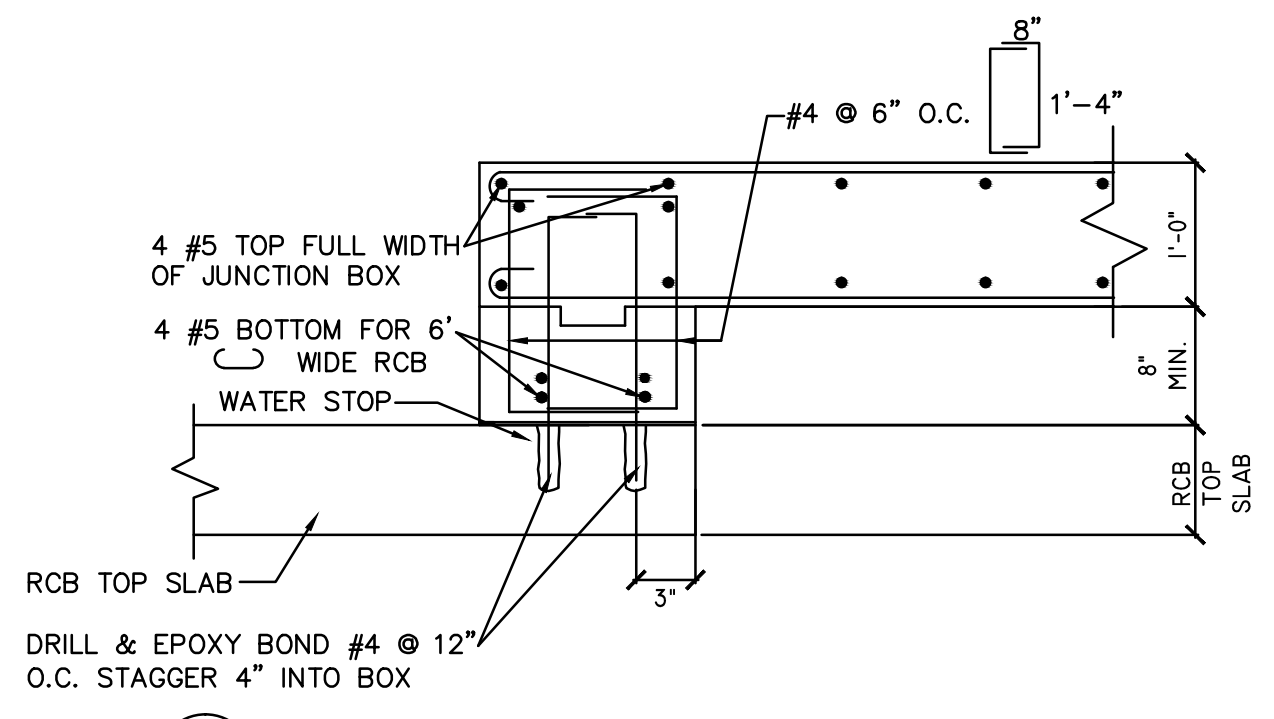
6 Additional Reinforcing At Opening (Slab & Wall)
SCALE: N.T.S.
NOTES:
1. PROVIDE 2 #6 x (B+L') ADDITIONAL REINFORCING BARS AT TOP & BOTTOM & SIDES OF OPENING.
2. PROVIDE ADDITIONAL BARS EQUAL TO ONE HALF OF BARS INTERRUPTED PLUS ONE AT EACH SIDE OF OPENING IN SHORT SPAN DIRECTION OF WALL OR SLAB AT 3' O.C. THESE BARS SHALL BE SAME SIZE & LENGTH AS THOSE OF THE INTERRUPTED BARS.



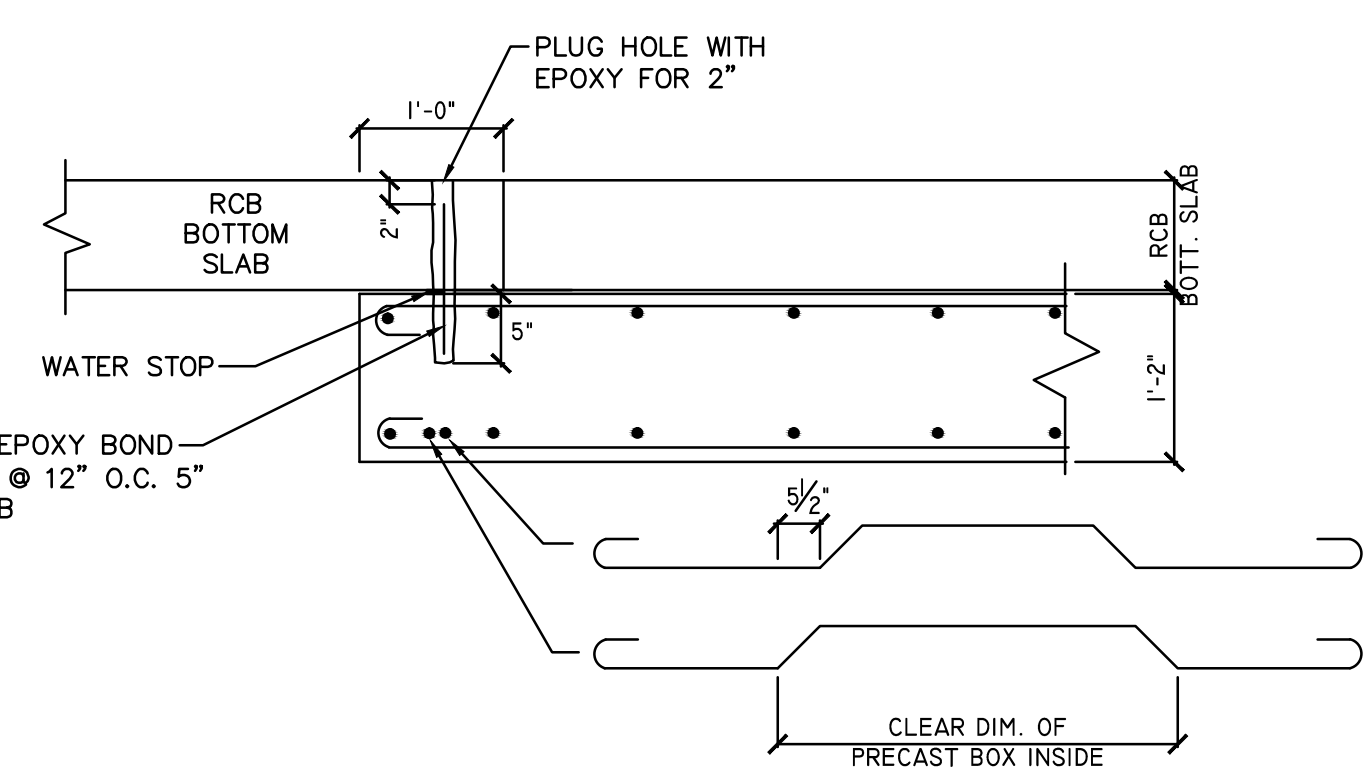
7 SCALE: 3/4"=1'-0"



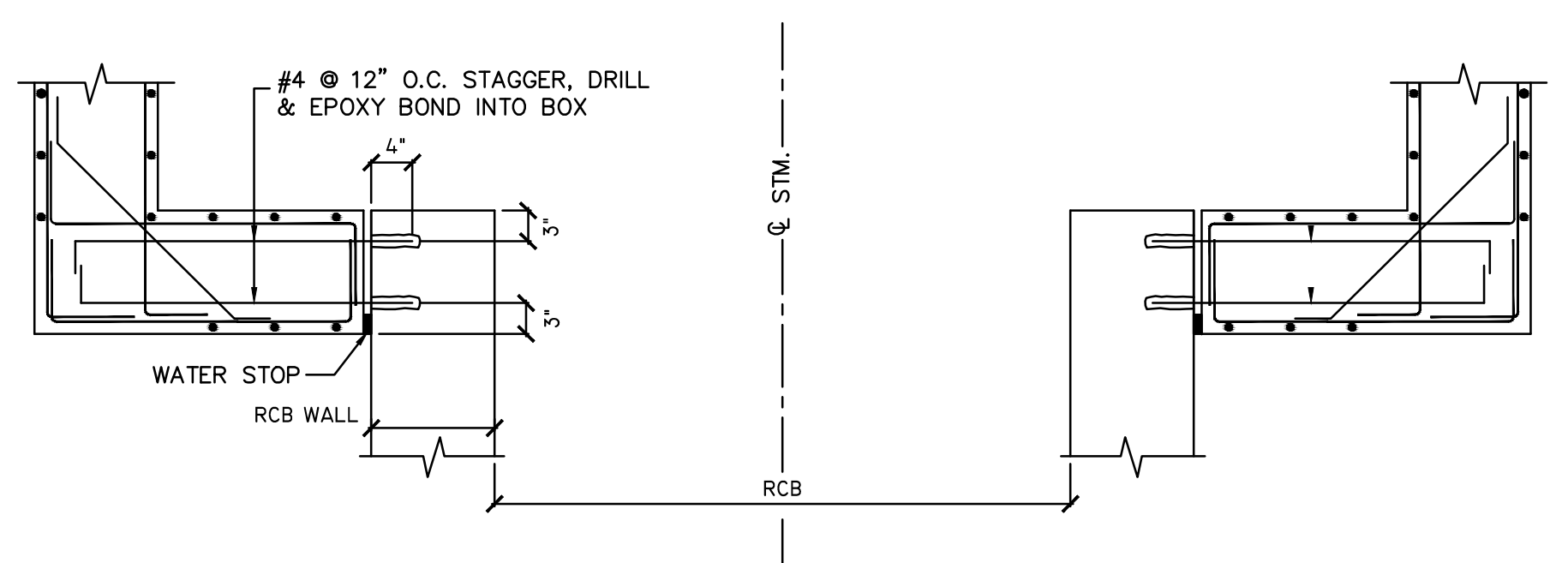
8 SCALE: 3/4"=1'-0"



9 SECTION - PRECAST BOX & JUNCTION BOX SLAB
SCALE: 3/4"=1'-0"

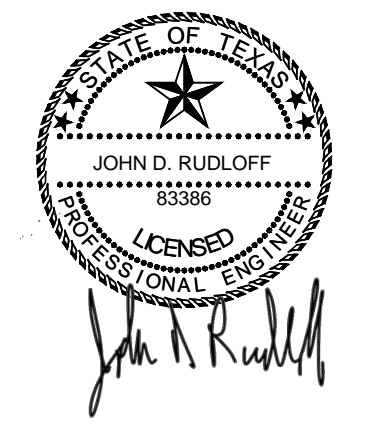


10 SECTION - PRECAST BOX & JUNCTION BOX WALL
SCALE: 3/4"=1'-0"



13 PLAN - PRECAST BOX & JUNCTION BOX WALL
SCALE: 3/4"=1'-0"

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19

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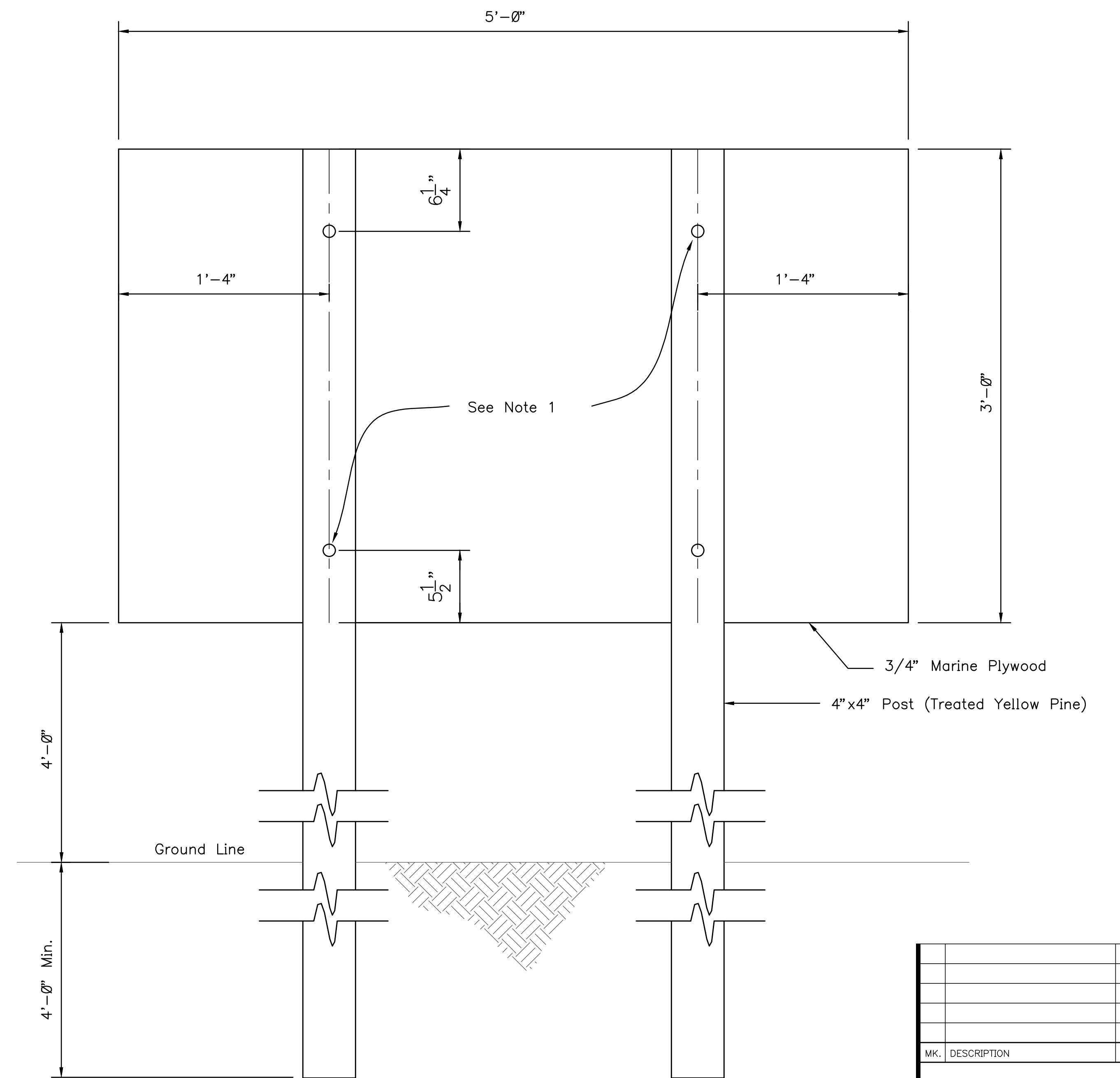
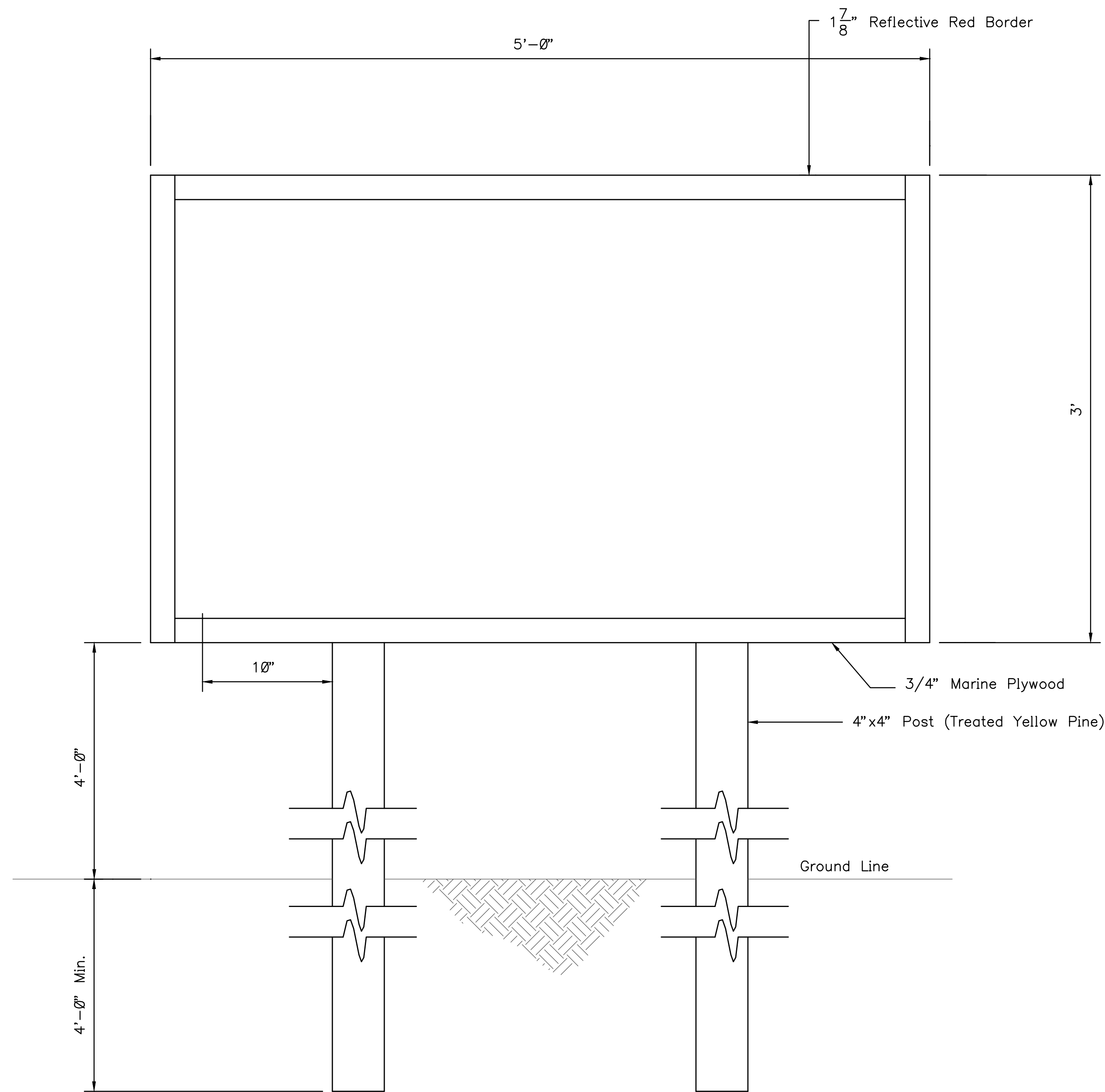
Galveston County, Texas
Texas Avenue Reconstruction

Structural
Typical Details

Job No.: 18-015
Date: September, 2019
Dwn By: D. Fattig
Chkd By: J Rudloff

Scale:
HORZ: N/A
VERT: N/A

SHEET
51
OF 52

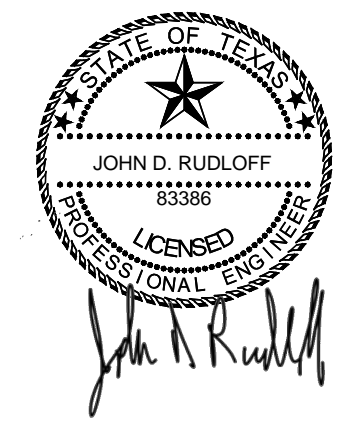


Notes:

1. 4" x 4" Post Fastened to Sign with 1/2" # x 5 1/2" Button Head Carriage Bolts, Nuts and Flat Washers.
2. Verify all information prior to ordering Project Sign.
3. Location(s) of the Project sign(s) will be determined at the pre-construction conference.

Project Sign Detail
Not to Scale

MK.	DESCRIPTION	DATE	DWN.	CHK.



9-13-19

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Galveston County, Texas

Texas Avenue Reconstruction

Project Sign Detail

Job No.: 18-015	Scale: N/A	SHEET 52 OF 52
Date: September, 2019	HORZ: N/A	
Dwn By: D. Fattig	VERT: N/A	
Chkd By: J Rudloff		



THE COUNTY OF GALVESTON

RUFUS G. CROWDER, CPPO, CPPB
PURCHASING AGENT

GWEN MCLAREN, CPPB
ASST. PURCHASING AGENT

COUNTY COURTHOUSE
722 Moody (21st Street)
Fifth (5th) Floor
GALVESTON, TEXAS 77550

November 7, 2019

PROJECT NAME: Texas Avenue Reconstruction

SOLICITATION NO: B201007

RE: ADDENDUM #1

To All Prospective Proposers,

The following information is being provided to aid in preparation of your proposal submittal(s):

Question #1: Is there a geotechnical report?

Response: The geotechnical report is attached with this addendum.

Question #2: Time of Completion is stated to be within 300 calendar days of Notice to Proceed issuance. However, a date for when the Notice to Proceed is projected to be issued is not state. What is the estimated project start date?

Response: The estimated start date is February of 2020.

Question #3: Can you post the pre-bid meeting sign-in sheet please?

Response: The pre-bid meeting sign-in sheet is attached with this addendum.

Question #4: Are there soil boring available? Can you send me any pre-bid notes?

Response: Please refer to the response to question #1. There are no pre-bid notes.

As a reminder, all questions regarding this proposal must be submitted in writing to:

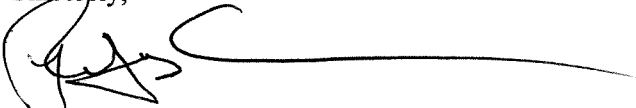
Rufus G. Crowder, CPPO CPPB
Galveston County Purchasing Agent
722 Moody, Fifth (5th) Floor
Galveston, Texas 77550
E-mail: purchasing.bids@co.galveston.tx.us

If you have any further questions regarding this proposal, please address them to Rufus Crowder, CPPO CPPB, Purchasing Agent, via e-mail at purchasing.bids@co.galveston.tx.us, or contact the Purchasing Department at (409) 770-5371.

If you have any further questions regarding this proposal, please address them to Rufus Crowder, CPPO CPPB, Purchasing Agent, via e-mail at purchasing.bids@co.galveston.tx.us, or contact the Purchasing Department at (409) 770-5371.

Please excuse us for any inconvenience that this may have caused.

Sincerely,

A handwritten signature in black ink, appearing to be 'Rufus G. Crowder', with a long horizontal flourish extending to the right.

Rufus G. Crowder, CPPO CPPB
Purchasing Agent
Galveston County

**GEOTECHNICAL INVESTIGATION
TEXAS AVENUE (FM 1765) RECONSTRUCTION
FROM 14TH STREET TO 6TH STREET
CITY OF TEXAS CITY, GALVESTON COUNTY, TEXAS**

REPORT NO. 1140243301

Reported to:

ARKK ENGINEERS, INC.

Houston, Texas

Reported by:

GEOTEST ENGINEERING, INC.

Houston, Texas

Key Map Nos. 738 G & H



GEOTEST ENGINEERING, INC.

Geotechnical Engineers & Materials Testing

5600 Bintliff Drive

Houston, Texas 77036

Telephone: (713) 266-0588

Fax: (713) 266-2977

Report No. 1140243301

June 6, 2019

Mr. Madhu Kilambi, P.E.
ARKK Engineers, Inc.
7322 Southwest Freeway, Suite 1040
Houston, Texas 77074

**Re: Geotechnical Investigation
Texas Avenue (FM 1765) Reconstruction
From 14th Street to 6th Street
City of Texas City, Galveston County, Texas**

Dear Mr. Kilambi:

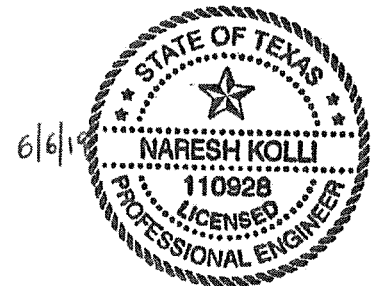
Presented herein is our geotechnical investigation report for the above referenced project. Preliminary field logs were submitted to you on April 17, 2019. This report supersedes all previously submitted reports, transmittals, etc. for the referenced project. This study was authorized by you on April 3, 2019, by accepting our Proposal No. 1140443399, dated March 26, 2019.

We appreciate this opportunity to be of service to you. If you have any questions regarding the report, or if we can be of further service to you, please call us.

Sincerely,
GEOTEST ENGINEERING, INC.
TBPE Registration No. F-410

Krishna M Pradeep, E.I.T.
Graduate Engineer

Naresh Kolli, P.E.
Project Manager



NK\kmp\ego

Copies Submitted: (1+1-pdf)

PC38\GEOTECHNICAL\40243301.DOC

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EXECUTIVE SUMMARY

A geotechnical investigation was conducted for the Texas Avenue (FM 1765) Reconstruction Project in the City of Texas City, Galveston County, Texas. The project includes reconstructing approximately 3,800 LF of existing 5-lane concrete paving along Texas Avenue (FM 1765) from 14th Street to 6th Street, with new concrete pavement. The project also includes storm sewer installation and water line replacement along Texas Avenue. Based on the information provided, we understand that the invert depth of the proposed storm sewer (24" RCP, 4' x 2' RCB, 5' x 2' RCB, and 7' x 2' RCB) ranges from approximately 4 to 6 feet, and will be installed primarily by open-cut method of construction. The proposed water line will be installed by trenchless (auger) method of construction.

This study included drilling and sampling of five (5) soil borings each to a depth of 15 feet, performing laboratory tests on recovered soil samples, performing engineering analyses and preparing a geotechnical report.

The principal findings and conclusions developed from this investigation are summarized below:

- The existing pavement along Texas Avenue from 14th Street to 6th Street, as obtained in borings GB-1 through GB-5 consists of 0.5 inches of asphalt over 8 to 9 inches of concrete.
- The subsurface soils below the existing pavement, as revealed by borings GB-1 through GB-5, consist of soft to hard gray, brown, reddish brown and gray, and yellowish brown and gray fat clay, fat clay with sand, sandy fat clay, lean clay, and lean clay with sand to the explored depth of 15 feet. Fill material consisting of gray and brown fat clay, lean clay, and lean clay with sand, calcareous and ferrous nodules, and shell fragments were encountered to depths ranging from 1 feet to 6 feet in borings GB-1, GB-3 and GB-4.
- No groundwater was encountered in the borings drilled for this investigation.
- All excavation operations should be in accordance with OSHA Standards, and Galveston

County Standard Specification, Section 01526, "Trench Safety Systems".

- The bedding and backfill for the proposed utilities should be in accordance with ARKK Standard Specification, Section 02227, and Galveston County Standard Specification, Section 02227, "Excavation and Backfill for Utilities".
- The auger pits/insertion and reception pits for the water line should be constructed as per the ARKK Standard Specifications Section 02317, "Auguring Pipe for Waterlines."
- The foundation recommendations for new manholes are presented in Section 5.5 of this report.
- The recommended pavement section and subgrade stabilization for Texas Avenue (FM 1765) reconstruction are presented in Section 5.6 of this report.

1.0 INTRODUCTION

1.1 Location and Description of Project

A geotechnical investigation was conducted for the Texas Avenue (FM 1765) Reconstruction Project in the City of Texas City, Galveston County, Texas. The project location is bounded by 14th Street to the west, and 6th Street to the east in Galveston County, Texas within the Key Map Page No. 738 Grid G and H.

The project includes reconstructing approximately 3,800 LF of existing 5-lane concrete paving along Texas Avenue (FM 1765) from 14th Street to 6th Street, with new concrete pavement. The project also includes storm sewer installation and water line replacement along Texas Avenue. Based on the information provided, we understand that the invert depth of the proposed storm sewer (24" RCP, 4' x 2' RCB, 5' x 2' RCB, and 7' x 2' RCB) ranges from approximately 4 to 6 feet, and will be installed primarily by open-cut method of construction. The proposed water line will be installed by trenchless (auger) method of construction. The vicinity map of the project alignment is shown on Figure 1.

1.2 Scope of Work

The purpose of this investigation was to evaluate the soil and groundwater (if any) conditions along Texas Avenue in the City of Texas City, and to provide geotechnical recommendations for the proposed roadway reconstruction and utilities replacement. The scope of this investigation consisted of the following tasks:

- Cored the existing pavement at five (5) locations along Texas Avenue to obtain the existing pavement thickness and for boring access.
- Drilled and sampled five (5) soil borings each to a depth of 15 feet along Texas Avenue (FM 1765) from 14th Street to 6th Street.

- Performed appropriate laboratory tests on selected representative soil samples to develop the engineering properties of the soil.
- Performed engineering analyses to develop geotechnical recommendations for pavement thickness including subgrade stabilization for the pavement construction, bedding and backfill and water level control for open cut construction for storm sewer and water line installation.
- Prepared a geotechnical investigation report including field and laboratory data and geotechnical recommendations.

2.0 FIELD EXPLORATION

Subsurface conditions along the project alignment were investigated by drilling a total of five (5) soil borings (GB-1 through GB-5) drilled each to a depth of 15 feet below existing pavement. All borings were drilled with a truck-mounted rotary drilling rig. Pavement coring was performed at each boring location to verify the existing pavement thickness and to access the subsurface soils. All the boring locations are shown on Plan of Borings, Figure 2. Survey information for the completed borehole locations was not available to us at the time of preparation of this report.

Samples were taken at continuous 2-foot intervals to a depth of 15 feet. Cohesive soil samples were obtained with a 3-inch diameter thin-walled tube sampler in general accordance with ASTM D1587. Each sample was removed from the sampler in the field, carefully examined and logged by an experienced soils technician. Suitable portions of each sample were then sealed and packaged for transportation to Geotest's laboratory. The shear strength of cohesive soil samples was estimated using a calibrated hand penetrometer in the field. After taking water level measurements (if any), all borings were grouted with cement bentonite grout.

Detailed descriptions of the soils encountered along the project alignment are given on the boring logs GB-1 through GB-5 and are presented on Figures A-1 through A-5 in Appendix A. A key to symbols and terms used on the boring logs is presented on Figure A-6 in Appendix A.

Groundwater level observations were made at each boring location during field investigation. The results of these observations are noted on the boring logs.

3.0 LABORATORY TESTING PROGRAM

The laboratory testing program was designed to evaluate the pertinent physical properties and shear strength characteristics of the subsurface soils. Classification tests were performed on selected samples to aid in soil classification.

Undrained shear strengths of selected cohesive samples were measured by unconsolidated undrained (UU) triaxial compression tests (ASTM D2850). The results of the UU triaxial compression tests are plotted on the boring logs as solid squares. The shear strength of cohesive samples was measured in the field with a calibrated hand penetrometer and also in the laboratory with a Torvane. The shear strength values obtained from the penetrometer and Torvane are plotted on the boring logs as open circles and triangles, respectively.

Moisture content and dry unit weight were measured for each unconfined compression test and UU triaxial compression test samples. Moisture content measurements (ASTM D2216) were also made on other samples to establish the moisture profile at each boring location. Atterberg limit tests (ASTM D4318) were performed on soil samples to measure plasticity characteristics. Percent passing No. 200 sieve (ASTM D1140) tests were also performed on selected samples. The result of all these tests are plotted or summarized on the boring logs GB-1 through GB-5 and are presented on Figures A-1 through A-5 in Appendix A.

4.0 GENERAL SUBSURFACE CONDITIONS

4.1 Existing Pavement

The existing pavement along Texas Avenue from 14th Street to 6th Street, as obtained in borings GB-1 through GB-5 consists of 0.5 inches of asphalt over 8 to 9 inches of concrete. The details of the pavement encountered at each boring location are presented below.

Street	Boring Nos.	Asphalt Surface Thickness (in.)	Concrete Thickness (in.)	Total (in.)
Texas Avenue	GB-1	0.5	8.5	9.0
	GB-2	0.5	8.5	9.0
	GB-3	0.5	8.75	9.25
	GB-4	0.5	8.0	8.5
	GB-5	0.5	9.0	9.5

4.2 Subsurface Soil

The subsurface soils below the existing pavement, as revealed by borings GB-1 through GB-5, consist of soft to hard gray, brown, reddish brown and gray, and yellowish brown and gray fat clay, fat clay with sand, sandy fat clay, lean clay, and lean clay with sand to the explored depth of 15 feet. Fill material consisting of gray and brown fat clay, lean clay, and lean clay with sand, calcareous and ferrous nodules, and shell fragments were encountered to depths ranging from 1 feet to 6 feet in borings GB-1, GB-3 and GB-4.

The fat clay, fat clay with sand, and sandy fat clay are of high plasticity with liquid limits ranging from 50 to 53 and plasticity indices ranging from 30 to 31. The lean clay and lean clay with sand are of medium plasticity with liquid limits ranging from 30 to 49 and plasticity indices ranging from 13 to 28. The fines content (passing No. 200 sieve) of fat clay and lean clay ranges from 95 to 97 percent. The fines content of fat clay with sand and lean clay with sand ranges from 74 to 83 percent, and the fines content of sandy fat clay was about 61 percent.

4.3 Water Levels

No groundwater was encountered in the borings drilled for this investigation. However, it should be noted that various environmental and man-made factors such as amount of precipitation, nearby subsurface construction activities, and change in area drainage can substantially influence the groundwater level.

5.0 GEOTECHNICAL RECOMMENDATIONS

5.1 General

The project includes reconstructing approximately 3,800 LF of existing 5-lane concrete paving along Texas Avenue (FM 1765) from 14th Street to 6th Street, with new concrete pavement. The project also includes storm sewer installation and water line replacement along Texas Avenue. Based on the information provided, we understand that the invert depth of the proposed storm sewer (24" RCP, 4' x 2' RCB, 5' x 2' RCB, and 7' x 2' RCB) ranges from approximately 4 to 6 feet, and will be installed primarily by open-cut method of construction. The proposed water line will be installed by trenchless (auger) method of construction.

5.2 Open-Cut Excavation

5.2.1 Geotechnical Parameters. Based on the soil conditions revealed by the borings, geotechnical parameters were developed for the design of open cut excavation for the proposed storm sewer, and auger (insertion/reception) pits planned for the trenchless installation. The geotechnical design parameters for open cut excavation for auger (insertion/reception) pits are provided in Table 1. For design, the groundwater level should be assumed to exist at the ground surface, since this condition may exist after a heavy rain or flooding.

5.2.2 Excavation Stability. The open excavations may be shored, laid back to a stable slope or some other equivalent means used to provide safety for workers and adjacent structures. The excavating and trenching operations should be in accordance with OSHA Standards, OSHA 2207, Subpart P, latest revision and Galveston County Standard Specification, Section 01526, "Trench Safety Systems".

- Excavation Shallower Than 5 Feet – For excavations that are less than 5 feet, the need for protection should be evaluated by a competent person to examine the ground for any indication of ground movement or potential cave-in. When any indication of hazardous ground movement or potential cave-in is anticipated during construction,

adequate protective system should be provided for all excavation even that if the excavations are shallower than 5 feet.

- Excavation Deeper Than 5 Feet - Excavations that are deeper than 5 feet should be sloped, shored, sheeted, braced or laid back to a stable slope or supported by some other equivalent means or protection such that workers are not exposed to moving ground or cave-ins. The slopes and shoring should be in accordance with the trench safety requirements per OSHA Standards. The following items provide design criteria for trench stability.
 - (i) OSHA's Soil Type. Based on the soil conditions revealed by the borings and the assumed groundwater level at surface, OSHA's soil type "C" should be used for the determination of allowable maximum slope and/or the design of a shoring system. For shoring deeper than 20 feet, an engineering evaluation is required.
 - (ii) Excavation Support Earth Pressure. Based on the subsurface conditions indicated by this investigation and laboratory testing results, the excavation support earth pressure diagram was developed and is presented on Figure 5. The pressure diagram can be used for the design of temporary excavation bracing. For a trench box, a lateral earth pressure resulting from an equivalent fluid with a unit weight of 97 pcf is recommended. The above value of equivalent fluid pressure is based upon an assumption that the groundwater level is near the ground surface, since these conditions may exist after a heavy rain or flooding. Effect of surcharge loads at the ground surface should be added to the computed lateral earth pressure. A surcharge load, q , will typically result in a lateral load equal to $0.5 q$.
 - (iii) Bottom Stability. In braced cuts, if tight sheeting is terminated at the base of the cut, the bottom of the excavation can become unstable under certain conditions. The stability of the trench bottom is governed by the shear strength of the soils and by the differential hydrostatic head. For cuts in cohesive soils as encountered in the

borings for excavation depths of 4 to 6 feet, stability of the bottom can be evaluated in accordance with the procedure outlined on Figure 6.

5.2.3 Groundwater Control. Excavations for the proposed utilities installation may encounter groundwater seepage to varying degrees depending on groundwater conditions at the time of construction and the location and depth of excavation. Based on the soil conditions identified in the borings for the proposed utilities installation, all the excavations will be in cohesive soils. In general, for cohesive soils as encountered in all the borings for the excavation depths (maximum depth of 6 feet), groundwater (if encountered) may be managed by collection in excavation bottom sumps for pumped disposal.

The contractor should verify the groundwater level at the time of construction and should provide an adequate dewatering system, where required. The groundwater control should be carried out in accordance with the ARKK Standard Specifications, Section 01563, and Galveston County Standard Specification, Section 01563, "Control of Ground Water and Surface Water".

5.2.4 Live Loads on Pipe Due to Traffic. Loads on pipe due to traffic (if any) should be considered. A graph providing calculated vertical stress on pipe due to traffic loads is given on Figure 7.

5.2.5 Bedding and Backfill for Utilities. The bedding and backfill for the storm sewer and water line should be in accordance with ARKK Standard Specification, Section 02227, and Galveston County Standard Specification, Section 02227, "Excavation and Backfill for Utilities".

5.2.6 Bedding and Backfill for the Auger Pits/Insertion and Receiving Pits. The auger pits or insertion and receiving pits should be constructed and backfilled in accordance with ARKK, Standard Specification Section, 02317, "Auguring Pipe for Waterlines."

5.3 Trenchless Installation

It is understood that the proposed water line will be replaced by auger method of construction. The trenchless method of construction should be per ARKK, Specification Section

02317, “Augering Pipe for Water Lines.”

5.3.1 Geotechnical Parameters. Based on the soil conditions revealed by soil borings (GB-1 through GB-5), laboratory test data and geotechnical design parameters were developed for cohesive soils and are provided in Table 2. The cohesive soils include fat clay, fat clay with sand, sandy fat clay, lean clay, and lean clay with sand. For design conditions, the groundwater level should be assumed to exist at the ground surface.

5.3.2 Earth Pressure on Pipe Casing. The earth pressures on augering should be determined from Figure 8. Equations to calculate the pipe casing loads are also shown on Figure 8.

5.3.3 Carrier Pipe Design Parameters. Carrier pipe must be sufficiently strong to withstand anticipated long-term ground loads and must not be subjected to deterioration by substance either in ground or in the auger casing. The carrier pipe design should include consideration of not only the loads applied to the pipe but also factors other than soil loading. These factors could include minimum structural code requirements, loading from augering and other construction loads. The drained geotechnical design parameters given in Table 2 should be used to analyze the soil structure intersection of the carrier pipe.

5.3.4 Influence of Augering on Adjacent Structures. Surface and near-surface structures near the tunnel alignment consist primarily of private properties, city streets and public and private utilities.

Ground movement, in terms of loss of ground or ground lost, is commonly associated with soft ground tunneling. If such ground movement is excessive, it may cause damage to the structures, roads and services located above the tunnel. While ground movement cannot be eliminated, it can be controlled within certain limits by the use of proper construction techniques and good quality workmanship. These include, but are not limited to, prevention of excessive ground loss during tunneling with the use of grouting and filling the annular space between the pipe or casing and the surrounding soil and prevention of undue loss of fines through dewatering.

The selection and execution of tunneling methods that are best suited to anticipated ground conditions along the proposed tunnel are, in fact, the contractor's primary contribution to successful completion of the proposed auger or directional drilling. On review of the boring logs, the ground conditions for tunneling (excavation face) will be primarily through cohesive soils. The cohesive soils as encountered in borings GB-1 through GB-5 consist of soft to hard gray, brown, reddish brown and gray, and yellowish brown and gray fat clay, fat clay with sand, sandy fat clay, lean clay, and lean clay with sand, and the ground in this area may be expected to behave as firm to raveling ground near the invert. Close monitoring of ground movement should be carried out during the trenchless installation.

The ground conditions for trenchless operation (excavation face) will be through predominantly in cohesive soils near borings GB-1 through GB-5. However, due to spacing of borings, soil conditions other than those encountered in borings could exist.

The proposed auger is parallel with or cross beneath utility lines. The largest potential problems from utilities may result from:

- Leaking water pipes
- Gas pipe breakage leading to a potential explosion
- Breakage of storm or sanitary sewers

In general, it is the contractor's responsibility to investigate these and other possible third party interactions along the proposed tunnel alignment and to accommodate all of these interactions with the use of good construction methods.

5.4 Piping System Thrust Restraint

Unbalanced thrust forces will occur at any point in the pipe where the direction or cross sectional area of the flow changes. The force diagram shown in Figure 9 illustrates the thrust force generated by flow at a bend in the pipe. The equations for computing this thrust force are also given in this figure. The thrust force will often require more resistance or support than is available just from the pipe bearing against the backfill. In order to prevent intolerable

movement and overstressing of the pipe, suitable buttressing should be provided.

Proposed horizontal bends may require restraint in addition to that supplied by the pipe bearing on the backfill. In general, thrust blocks, both horizontal and vertical and restrained joints are common methods of supplying additional reaction. However, it is noted that restrained joints are considered for supplying additional reaction for the project and is discussed below.

5.4.1 Restrained Joints. Where thrust blocks are not practical, restrained joints, allowing thrust and shear forces to be transmitted across the pipe joints, are employed to allow a number of pipe sections to act integrally in bearing. The equations necessary to determine the restrained pipe length on each side of the bend are given below:

$$L = \frac{PA \sin(\theta / 2)}{f(2W_e + W_p + W_w)}$$

- where,
- L = restrained pipe length on each side of the bend, in feet
 - P = internal pressure, in pounds per square inch
 - A = cross sectional area of first unrestrained pipe joint, in square inches
 - θ = deflection angle of bend, in degrees
 - f = co-efficient of friction between pipe and soil (recommended 0.3)
 - W_e = overburden load, in pounds per liner foot = $\Upsilon_b B_c H$
 - W_p = weight of pipe, in pounds per linear foot
 - W_w = weight of water in pipe, in pounds per linear foot
 - Υ_b = wet unit weight of backfill material, in pounds per cubic foot
(recommended 120 pcf)
 - B_c = pipe outer diameter, in feet
 - H = earth cover, in feet

Reinforced concrete encasement may be used in lieu of the manufactured joint restrained system. The equations and soil parameters given above can be used for the design of reinforced concrete encasement.

5.5 Structures

5.5.1 Description. The structure associated with this project will be new manholes. The new manholes for the proposed utilities will be placed at depths ranging from 4 to 6 feet below existing pavement (elevations ranging from approximately 1.0 to 2.2 feet).

5.5.2 Foundation Conditions. Based on the soil conditions revealed by the borings GB-1 through GB-5, the manholes bottom will be in medium stiff to very stiff lean clay, lean clay with sand, sandy fat clay, and fat clay fill soils.

5.5.3 Foundation Design Recommendations. The following items provide recommendations and design criteria for construction of the new manholes.

- Allowable Bearing Pressures. The mat foundation for supporting the new manholes placed at depths ranging from 4 to 6 feet [into medium stiff to very stiff lean clay, lean clay with sand, sandy fat clay, and fat clay] should be designed for an allowable (net) bearing pressure of 1,850 psf. The allowable bearing pressure includes a safety factor of 2.0.

The above recommendation assumes that the final bearing surfaces consist of undisturbed natural soils and that underlying semi-transmissive zones are properly pressure-relieved and stable undisturbed bearing surfaces are attained.

- Bottom Stability. In braced cuts, if tight sheeting is terminated at the base of the cut, the bottom of the excavation can become unstable. The parameters that govern the stability of the excavation base are the soil shear strength and the differential hydrostatic head between the water level within the retained soils and the water level at the interior of the trench excavation. For cuts in cohesive soils as predominantly encountered in the borings, the bottom stability can be evaluated as outlined on Figure 6.

- Lateral Earth Pressure. The pressure diagram presented on Figure 5 can be used for the design of braced excavation. The lateral earth pressure diagram presented on Figure 10 is applicable for the design of the permanent walls.

- Hydrostatic Uplift Resistance. Structures extending below the water level should be designed to resist uplift pressure resulting from excess piezometric head. Design uplift pressures should be computed based on the assumption that the water table is at ground surface. To resist the hydrostatic uplift at the bottom of the structure, one of the following sources of resistance can be utilized in each of the designs.
 - a. Dead weight of structure,
 - b. Weight of soil above base extensions plus weight of structure, or
 - c. Soil-wall friction plus dead weight of structure.

The uplift force and resistance to uplift should be computed as detailed on Figure 11. In determining the configuration and dimensions of the structure using one of the approaches presented on Figure 11, the following factors of safety are recommended.

- a. Dead weight of concrete structure, $S_{f1} = 1.10$,
- b. Weight of soil (backfill) above base extension, $S_{f2} = 1.5$, and
- c. Soil-wall friction, $S_{f3} = 3.0$.

Friction resistance should be discounted for the upper 5 feet, since this zone is affected by seasonal moisture changes.

5.5.4 Protection of Below Grade Structures. The design of the proper means for protection of below grade structures will depend upon the potential of the aggressivity or corrosivity of soil and groundwater properties. Aggressivity testing was not within the scope of this investigation. The design of the protection of below grade structures is beyond the scope of services for this investigation.

5.5.5 Water Level Control During Construction. Water level control should be in accordance with section 5.2.3 of this report.

5.5.6 Structure Backfill. Excavations for the proposed structures should be backfilled in accordance with the ARKK Standard Specifications, and Galveston County Standard Specification, Section 02226, "Excavation and Backfill for Structures."

5.6 Pavement Structure Design

We understand that the existing 5-lane concrete paving along Texas Avenue (FM 1765) from 14th Street to 6th Street, will be reconstructed with new concrete pavement with curb and gutter. The pavement design presented below was developed in accordance with "AASHTO Guide for Design of Pavement Structures," 1993 Edition.

5.6.1 Design Parameters

Subgrade Soil Properties. California Bearing Ratio (CBR) tests were not within the scope of this project. Therefore, the roadbed soil resilient modulus is estimated based on physical properties and strength characteristics of the natural subgrade soils. Based on the physical properties and strength characteristics of the natural subgrade soils obtained from laboratory tests, the effective roadbed soil resilient modulus (M_R) was estimated to be about 1,941 psi from an assumed CBR value of 1.0. Based on an estimated resilient modulus of the 8-inch lime-stabilized subgrade, the effective modulus of subgrade reaction (k) is estimated to be about 49 pci.

Traffic Data. No traffic count and vehicle classification data was provided to us at the time of preparation of this report. Based on the information provided by ARKK, the new concrete pavement section will be constructed in general accordance with a standard pavement design. A traffic loading of 6.2×10^6 kips ESALs was calculated over a 20-year design period and was utilized for the

pavement design.

Other Design Parameters. Other design parameters used in the development of rigid pavement thickness are given below:

Material Properties of Concrete:

Modulus of Elasticity of Concrete (E_c): 3,604,997 psi

Mean value of Modulus of Rupture of Concrete after 28 days

(S'_c): 630 psi (based on compressive strength of 4,000 psi)

Load Transfer coefficient (J): 2.7

Drainage coefficient (C_d): 1.2

Overall Standard Deviation (S_o): 0.35

Reliability Level (R): 90%

Serviceability Index

Initial (P_o): 4.5

Terminal (P_t): 2.25

Reinforcement Variables

Allowable Working Stress (f_s): 45,000 psi (grade 60 steel)

Friction Factor (F): 1.8

5.6.2 Recommended Pavement Section

Based on the design parameters described above and the AASHTO design, the thickness of rigid pavement was determined. The recommended pavement section is given below:

Pavement Course	Thickness, inches
Reinforced Concrete	8
5% Lime-stabilized subgrade	8

For the 8-inch concrete pavement, the required longitudinal reinforcing steel for an expansion joint spacing of 80 feet and transverse reinforcement steel for a pavement width of 24

feet back to back are given below for the grade 60 steel.

Pavement Thickness (Inches)	Longitudinal Steel	Transverse Steel
	Center to Center Spacing (in)	Center to Center Spacing (in)
	# 5 bars	# 5 bars
8	24	30

5.6.3 Preparation of Pavement Subgrade

Based on the field and laboratory test data, the subgrade soils below the existing pavement sections consist of high plasticity lean clay, lean clay with sand, fat clay, fat clay with sand and sandy fat clay. These subgrade soils have high volume change potential. Hence, lime stabilization of the fat clay and lean clay subgrade soils will be required to reduce the swelling and shrinkage potential, to accelerate the construction and provide a stable subgrade on which to construct the pavement sections. The fat clay subgrade soils should be stabilized with 5 percent lime (by dry unit weight of soil) to a depth of at least 8 inches. This corresponds to approximately 33 pounds of lime per square yard based on a dry unit weight of 110 pcf. The actual percentage of lime should be confirmed by laboratory tests at the time of construction.

Subgrade preparation for the proposed pavement after removing the existing pavement should consist of stripping, proof-rolling, and stabilization. The following procedures for subgrade preparation are recommended:

1. Strip the surficial soils to a suitable depth to remove all surficial vegetation and achieve grade. In isolated areas where soft, compressible, or very loose soils are encountered, additional stripping may be required.
2. After stripping, the exposed surface should be proof-rolled with a minimum of 3 passes of a 30-ton pneumatic-tired roller or a partially loaded truck utilizing a tire pressure of approximately 90 psi. If rutting develops, the tire pressure should be reduced. The purpose of the proof-rolling operation is to identify any

underlying zones or pockets of soft soils so these weak materials can be removed and replaced.

3. Lime stabilization of cohesive subgrade should be performed in accordance with ARKK Standard Specification, Section 02241, "Lime Stabilized Subgrade".

6.0 PROVISIONS

The description of subsurface conditions and the design information contained in this report are based on the test borings made at the time of drilling at specific locations. However, some variation in soil conditions may occur between test borings. Should any subsurface conditions other than those described in our boring logs be encountered, Geotest should be immediately notified so that further investigation and supplemental recommendations can be provided. The depth of the groundwater level may vary with changes in environmental conditions such as frequency and magnitude of rainfall. The stratification lines on the log of borings represent the approximate boundaries between soil types, however, the transition between soil types may be more gradual than depicted.

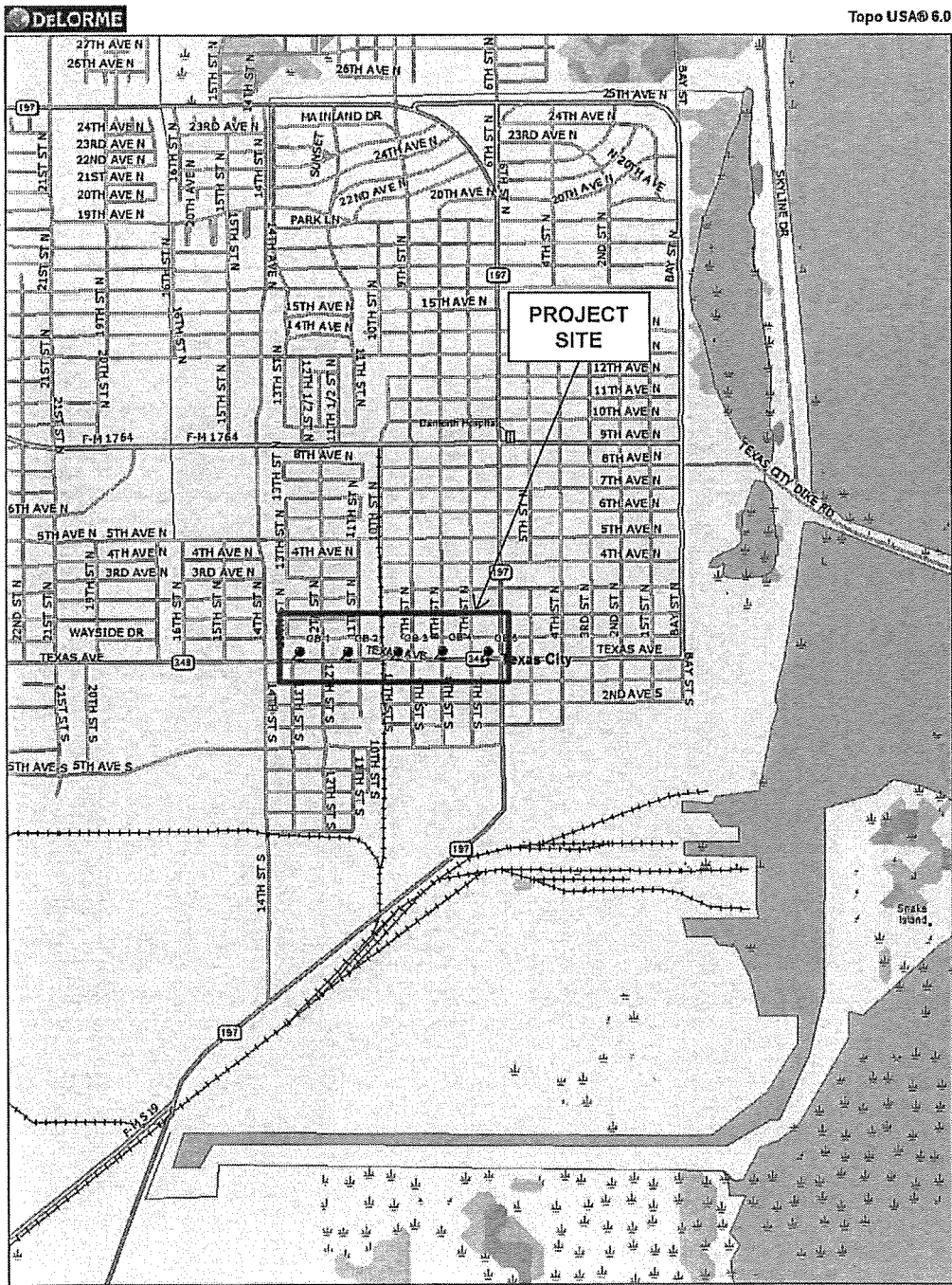
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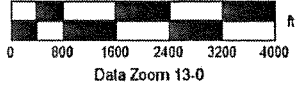
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Job No. 1140243301



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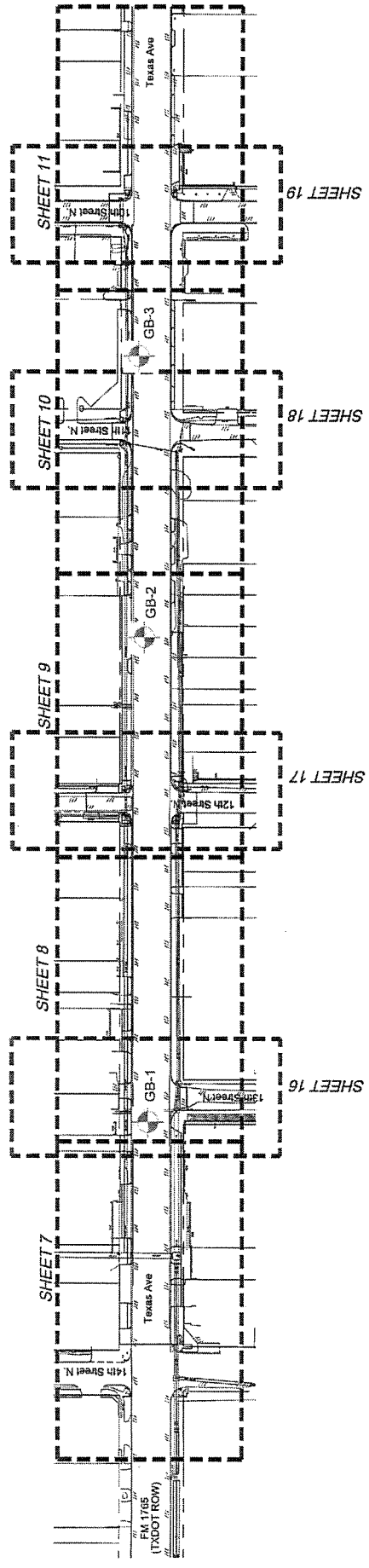


PAVING IMPROVEMENTS ALONG TEXAS AVENUE (FM 1765)
 FROM 14TH STREET TO 6TH STREET
 CITY OF TEXAS CITY, GALVESTON COUNTY, TEXAS

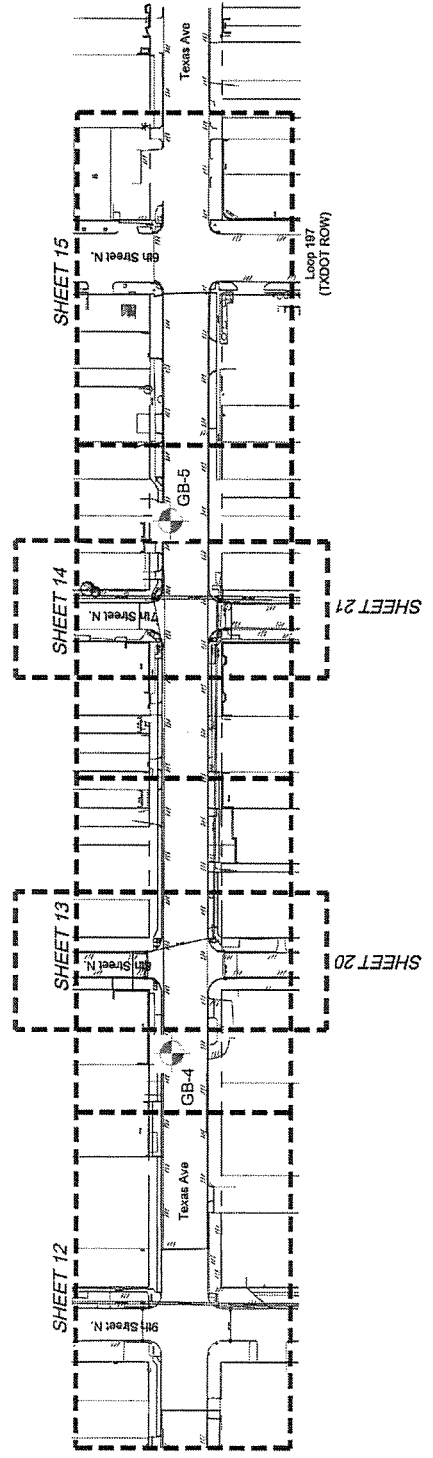
VICINITY MAP

Geotest Engineering, Inc.

FIGURE 1



LEGEND
 Boring



DATE	DESCRPTION	DATE	DESCRPTION

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Galveston County, Texas
 Texas Avenue Reconstruction

Overall Layout Plan

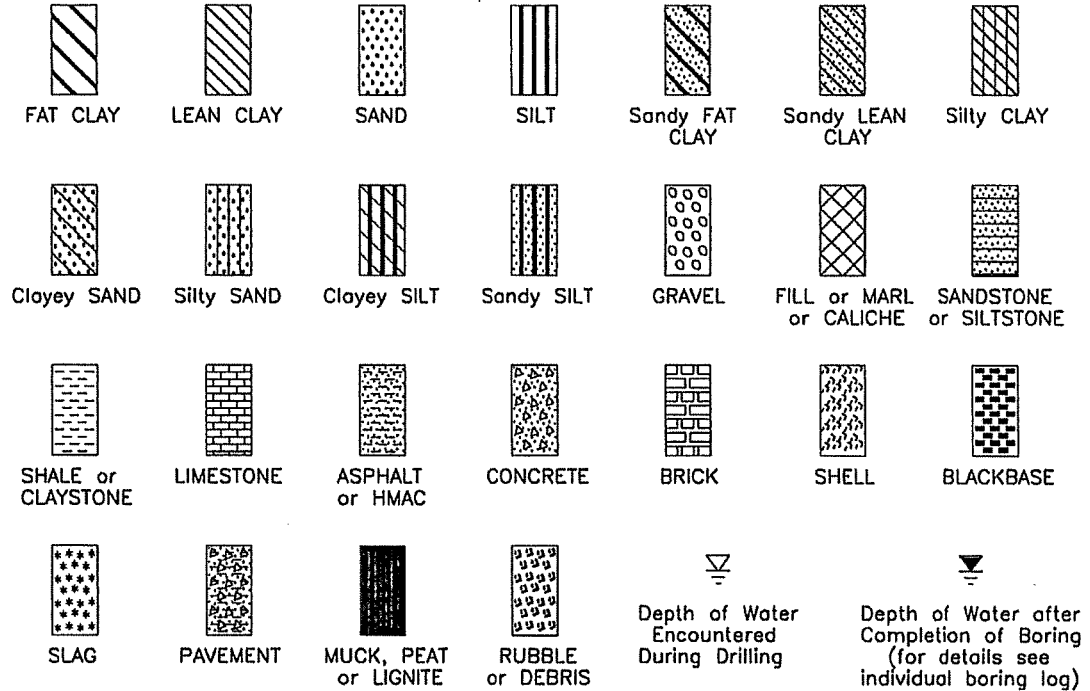
Job No.: 1140243301
 Date: April, 2019
 Sheet No.: 01 of 01
 Scale: 1" = 100'

Prepared by: J. Ruppert
 Checked by: J. Ruppert

FIGURE 2

SYMBOLS AND ABBREVIATIONS USED ON BORING LOG PROFILE

LEGEND



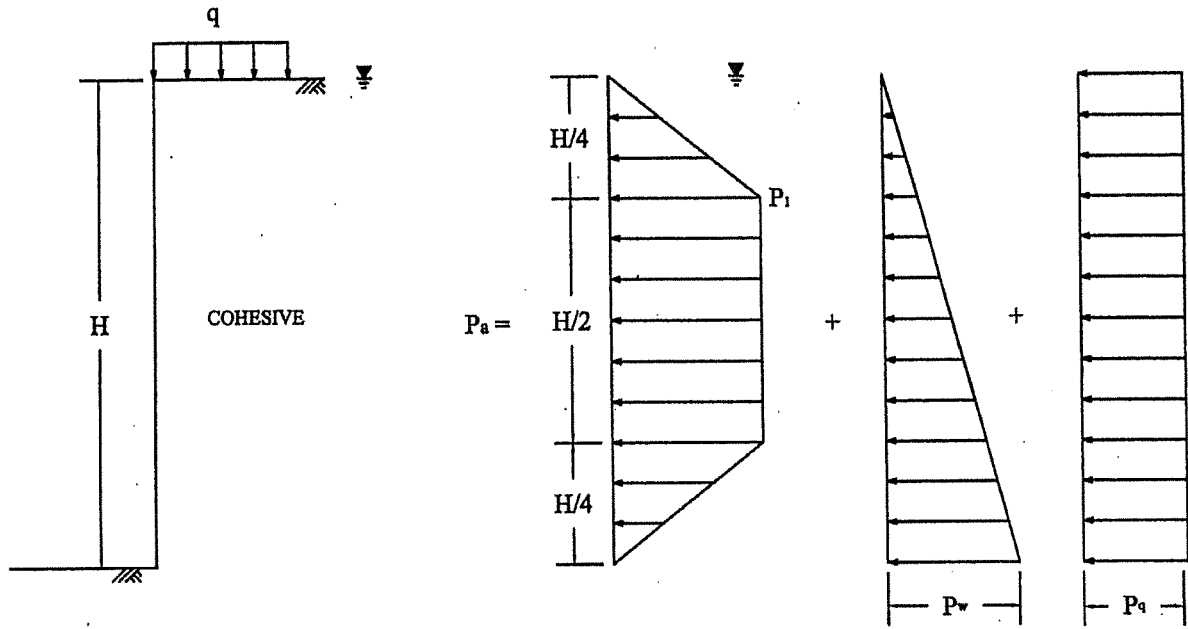
ABBREVIATIONS USED FOR CONSISTENCY/DENSITY

COHESIVE SOILS

V/So : Very Soft
 So : Soft
 Fm : Firm
 M/St : Medium Stiff
 St : Stiff
 V/St : Very Stiff
 Hd : Hard
 V/Hd : Very Hard

COHESIONLESS SOILS

V/Lo : Very Loose
 Lo : Loose
 S/Co : Slightly Compact
 Co : Compact
 M/De : Medium Dense
 De : Dense
 V/De : Very Dense



TYPICAL SOIL PARAMETERS

See Table 1 for typical values of soil parameters

BRACED WALL

For $\gamma H/c \leq 4$

$$P_1 = 0.3 \gamma' H$$

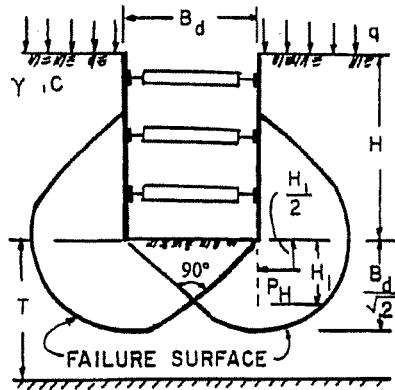
$$P_w = \gamma_w H = 62.4 H$$

$$P_q = 0.5 q$$

- Where:
- γ' = Submerged unit weight of cohesive soil, pcf;
 - γ_w = Unit weight of water, pcf;
 - q = Surcharge load at surface, psf;
 - P_a = Lateral pressure, psf;
 - P_1 = Active earth pressure, psf;
 - P_q = Horizontal pressure due to surcharge, psf;
 - P_w = Hydrostatic pressure due to groundwater, psf;
 - H = Depth of braced excavation, feet
 - c = Shear strength of cohesion soil, psf;

TRENCH SUPPORT EARTH PRESSURE
SUBMERGED COHESIVE SOIL

CUT IN COHESIVE SOIL,
 DEPTH OF COHESIVE SOIL UNLIMITED ($T > 0.7 B_d$)
 L = LENGTH OF CUT



If sheeting terminates at base of cut:

$$\text{Safety factor, } F_s = \frac{N_c C}{\gamma H + q}$$

N_c = Bearing capacity factor, which depends on dimensions of the excavation : B_d , L and H (use N_c from graph below)

C = Undrained shear strength of clay in failure zone beneath and surrounding base of cut

γ = Unit weight of soil (see Table 1)

q = Surface surcharge (assumed q = 500 psf)

If safety factor is less than 1.5, sheeting or soldier piles must be carried below the base of cut to insure stability - (see note)

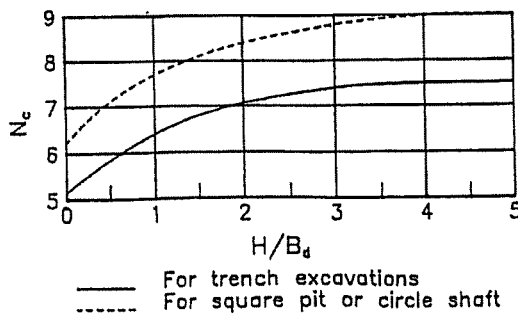
$$H_1 = \text{Buried length} = \frac{B_d}{2} \geq 5 \text{ feet}$$

Note : If soldier piles are used, the center to center spacing should not exceed 3 times the width or diameter of soldier pile .

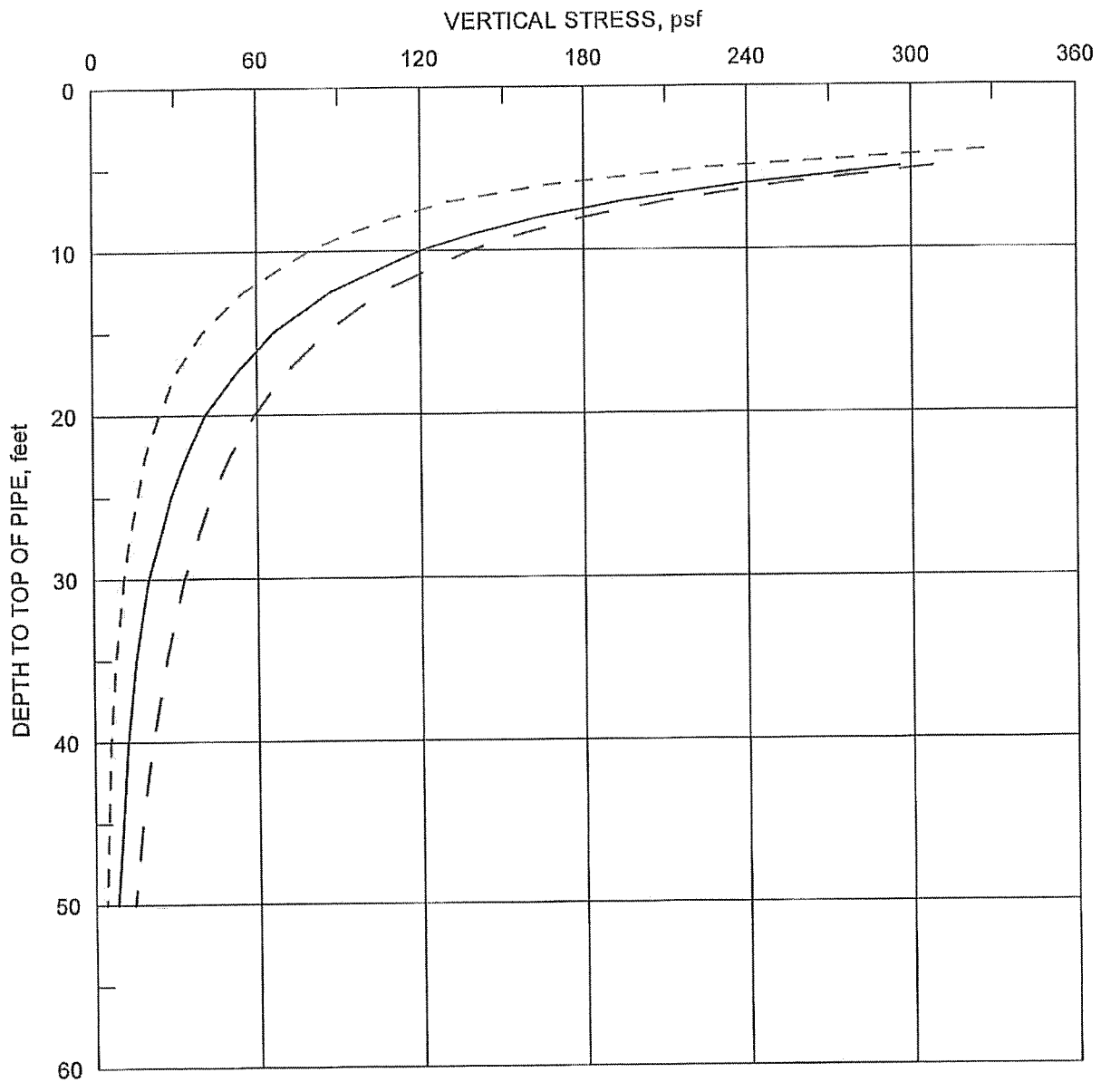
Force on buried length, P_H :

$$\text{If } H_1 > \frac{2 B_d}{3 \sqrt{2}}, P_H = 0.7 (\gamma H B_d - 1.4 C H - \pi C B_d) \text{ in lbs/ linear foot}$$

$$\text{If } H_1 < \frac{2 B_d}{3 \sqrt{2}}, P_H = 1.5 H_1 \left(\gamma H - \frac{1.4 C H}{B_d} - \pi C \right) \text{ in lbs/ linear foot}$$



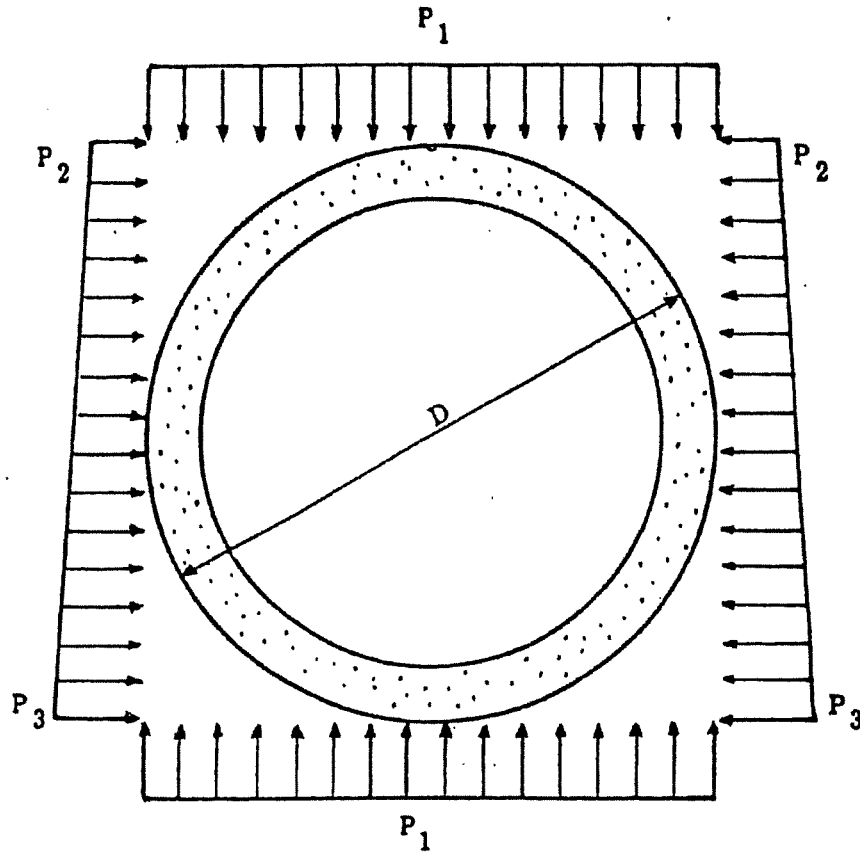
STABILITY OF BOTTOM
 FOR
 BRACED CUT



Legend:
- - - - - One Pass HS20
————— Two Pass HS20
- - - - - Four Pass HS20

Notes:
1. Based on standard AASHTO H20 or HS20 dual wheel truck axle loadings
2. The vertical stress was estimated by using Westergaard solution

VERTICAL STRESS ON PIPE
DUE TO TRAFFIC LOAD



$$P_1 = [(H + \frac{D}{2}) \times (\gamma - \gamma_w) + D_w \times \gamma_w] + q_s, \text{ for } D_w < H + \frac{D}{2}$$

$$P_1 = [(H + \frac{D}{2}) \times \gamma] + q_s, \text{ for } D_w \geq H + \frac{D}{2}$$

$$P_2 = (H \times \gamma) + q_s$$

$$P_3 = [(H + D) \times \gamma] + q_s$$

Where: P_1, P_2, P_3 = Tunnel liner load, psf.

D = Tunnel outside diameter, ft.

H = Depth to top of tunnel; ft.

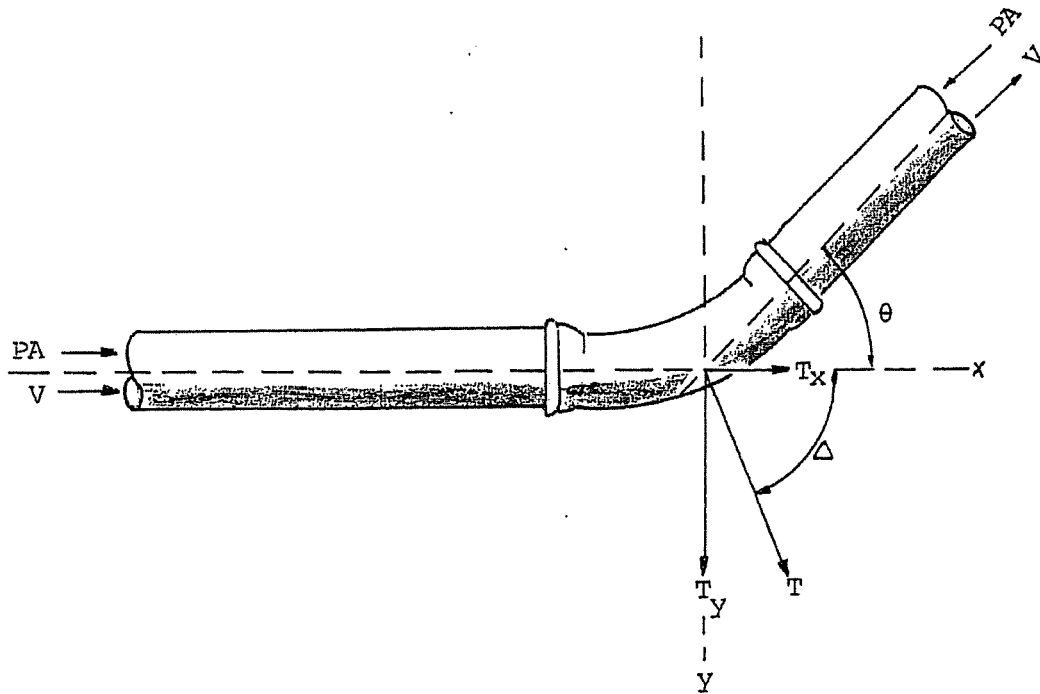
D_w = Depth to ground water level; ft.

γ = Wet unit weight of soil, pcf (see Table 2)

γ_w = Unit weight of water, 62.4 pcf

q_s = Surcharge load, psf.

EARTH PRESSURE ON AUGERING



$$T_x = PA (1 - \cos \theta)$$

$$T_y = PA \sin \theta$$

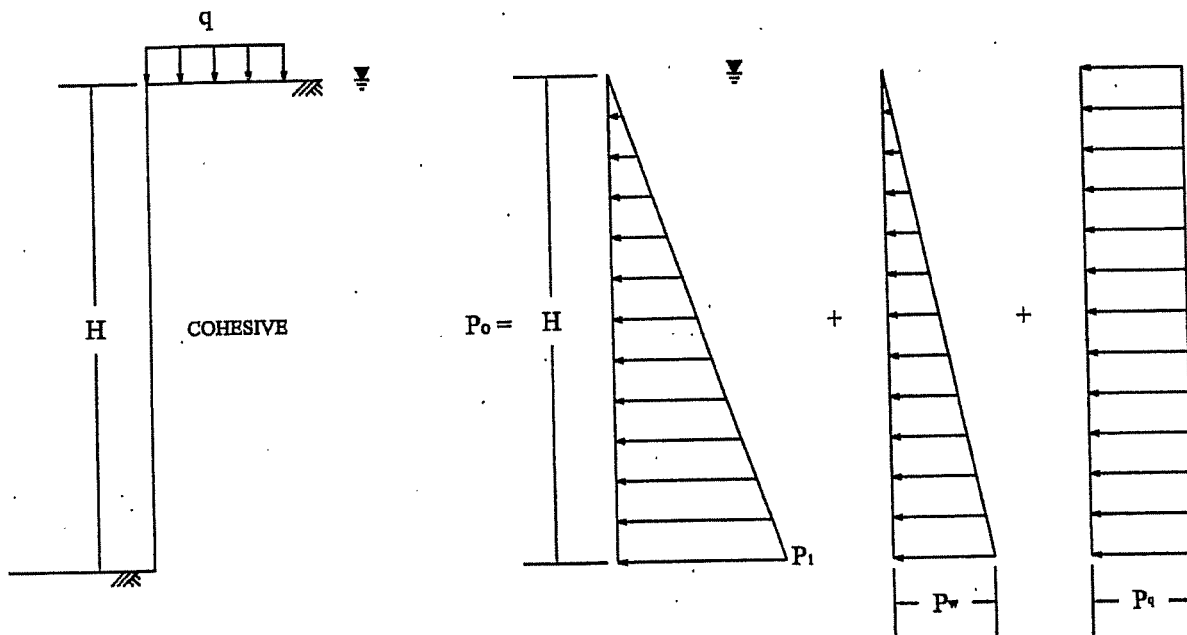
$$T = 2 PA \sin \frac{\theta}{2}$$

$$\Delta = (90 - \frac{\theta}{2})$$

Where:

- T is the resultant force on the bend
- T_x is the component of thrust force in x-direction
- T_y is the component of thrust force in y-direction
- P is the maximum sustained pressure
- A is the pipe cross-sectional area
- θ is the bend deflection angle
- Δ is the angle between T and X-axis
- V is the fluid velocity

**THRUST FORCES ACTING
ON A BEND**



TYPICAL SOIL PARAMETERS

See Table 1 for typical values of soil parameters

$K_{oc} = 1.0$

PERMANENT WALL

$P_1 = K_{oc} \gamma'_c H$
 $P_w = \gamma_w H = 62.4 H$
 $P_q = 0.5 q$

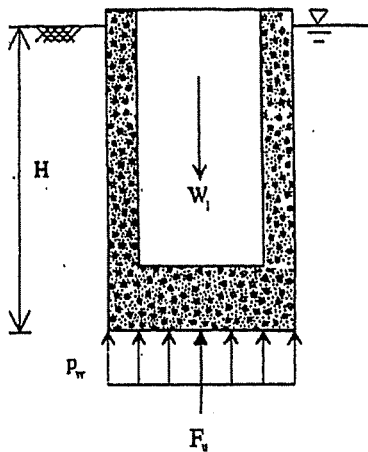
Where:

- γ'_c = Submerged unit weight of cohesive soil, pcf;
- K_{oc} = Coefficient of at-rest earth pressure in cohesive soil;
- γ_w = Unit weight of water, pcf;
- q = Surcharge load at surface, psf;
- P_0 = Lateral pressure, psf;
- P_1 = At-rest earth pressure, psf;
- P_q = Horizontal pressure due to surcharge, psf;
- P_w = Hydrostatic pressure due to groundwater, psf;
- H = Depth of excavation, feet

**LATERAL EARTH PRESSURE DIAGRAM
FOR PERMANENT WALL**

SUBMERGED COHESIVE SOIL

(a) DEAD WEIGHT OF STRUCTURE



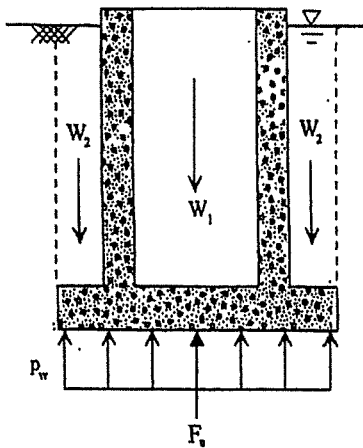
$$P_w = H\gamma_w$$

$$F_u = A_b P_w$$

$$\frac{W_1}{S_{f_1}} = F_u$$

See Table 1 for typical values of soil parameters

(b) WEIGHT OF SOIL ABOVE BASE EXTENSION PLUS DEAD WEIGHT OF STRUCTURE

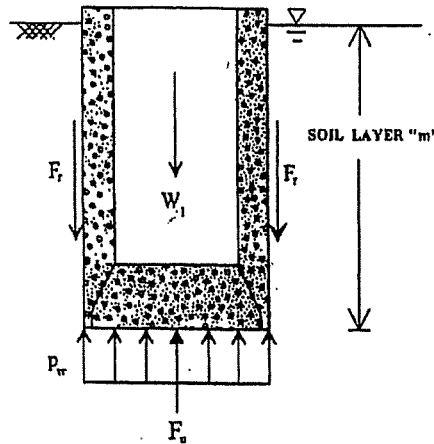


$$P_w = H\gamma_w$$

$$F_u = A_b P_w$$

$$\frac{W_1 + W_2}{S_{f_1}} = F_u$$

(c) SOIL-WALL FRICTION PLUS DEAD WEIGHT OF STRUCTURE



$$P_w = H\gamma_w$$

$$F_u = A_b P_w$$

$$\frac{W_1 + F_r}{S_{f_1}} = F_u$$

Predominantly Cohesive Soils, $F_r = \alpha c_m A_m$

Predominantly Cohesionless Soils, $F_r = p_m A_m K \tan \delta_m$

- Where:
- A_b = area of base, sq. ft.
 - A_m = cylindrical surface area of layer "m", sq. ft.
 - c_m = undrained cohesion of soil layer "m", psf.
 - F_u = hydrostatic uplift force, lbs.
 - F_r = frictional resistance, lbs.
 - H = height of buried structure, ft.
 - K = coefficient of lateral pressure = 0.5.
 - p_m = average overburden pressure for layer "m," psf.
 - P_w = hydrostatic uplift pressure, psf.
 - $S_{f_1, 2, 3}$ = factor of safety.
 - W_1 = dead weight of concrete structure, lbs.
 - W_2 = weight of backfill above base extension, lbs.
 - α = cohesion reduction factor = 0.5.
 - δ_m = friction angle between soil layer "m" and concrete wall, degrees = $0.75 \phi_m$
 - ϕ_m = internal angle of friction of soil layer "m", degrees.
 - γ_w = unit weight of water = 62.4 pcf.

UPLIFT PRESSURE AND RESISTANCE

TABLES

	<u>Table</u>
Geotechnical Design Parameter Summary: Open-Cut Excavation	1
Geotechnical Design Parameter Summary: Trenchless Installation.....	2

TABLE 1**GEOTECHNICAL DESIGN PARAMETER SUMMARY
OPEN-CUT EXCAVATION**

Boring Nos.	Stratigraphic Unit	Range of Depths, ft	Wet Unit Weight, γ, pcf	Submerged Unit Weight, γ', pcf	Undrained Cohesion, psf	Internal Friction Angle, ϕ, degree
GB-1	FILL/Cohesive	0-4	129	65	750	--
thru	Cohesive	4-6	133	67	1,000	--
GB-5		6-10	133	67	500	--
		10-15	132	66	250	--

Notes:

1. Cohesive soils include fat clay, fat clay with sand, sandy fat clay, lean clay, and lean clay with sand.
2. Fill soils include fat clay, lean clay, and lean clay with sand and shell fragments.

TABLE 2
GEOTECHNICAL DESIGN PARAMETER SUMMARY
TRENCHLESS INSTALLATION ALONG TEXAS AVENUE (FM 1765)
(GB-1 THROUGH GB-5)

PROPERTY	COHESIVE SOILS ⁽¹⁾	
Wet Unit Weight, γ , pcf	0-4 ft.	129
	4-6 ft.	133
	6-10 ft.	133
	10-15 ft.	132
Submerged Unit Weight, γ' , pcf	0-4 ft.	65
	4-6 ft.	67
	6-10 ft.	67
	10-15 ft.	66
Moisture Content (%)	0-4 ft.	20
	4-6 ft.	20
	6-10 ft.	25
	10-15 ft.	23
UNDRAINED PROPERTIES *		
Undrained Cohesion, C_u , psf	0-4 ft.	750
	4-6 ft.	1,500
	6-10 ft.	500
	10-12 ft.	250
Angle of Internal, ϕ , degrees	0-4 ft.	0
	4-6 ft.	0
	6-10 ft.	0
	10-12 ft.	0
Elastic Modulus, E, psf	0-4 ft.	225,000
	4-6 ft.	450,000
	6-10 ft.	200,000
	10-12 ft.	100,000
Coefficient of Lateral Earth Pressure at Rest, K_0	0-4 ft.	1.2
	4-6 ft.	1.2
	6-10 ft.	1.2
	10-12 ft.	1.2
Poisson's Ratio	0.45	
DRAINED PROPERTIES *		
Drained Cohesion, C' , psf	0-4 ft.	0
	4-6 ft.	0
	6-10 ft.	0
	10-12 ft.	0
Angle of Internal Friction, ϕ' , degrees	0-4 ft.	25
	4-6 ft.	25
	6-10 ft.	27
	10-12 ft.	27
Elastic Modulus, E, psf	0-4 ft.	135,000
	4-6 ft.	270,000
	6-10 ft.	120,000
	10-12 ft.	60,000

Notes:

1. Cohesive soils include fat clay, fat clay with sand, sandy fat clay, lean clay, and lean clay with sand.
- * Tunnel zone which includes depth plus 6 feet above invert plus 6 feet below invert.

APPENDIX A

	<u>Figure</u>
Log of Borings.....	A-1 thru A-5
Symbols and Terms Used on Boring Logs	A-6

LOG OF BORING NO. GB-1

PROJECT : Paving Improvements along Texas Avenue (FM 1765) from 14th Street to 6th Street
 City of Texas City, Galveston County, Texas
 LOCATION : See Plan of Borings (Figure 2)
 SURFACE ELEVATION : Existing Grade

PROJECT NO. : 1140243301
 COMPLETION DEPTH : 15.0 FT.
 DATE : 04-10-19

ELEVATION, FEET	DEPTH, FEET	SYMBOL	SAMPLES	DESCRIPTION OF MATERIAL	STANDARD PENETRATION TEST, BLOWS PER FOOT	PERCENT PASSING NO. 200 SIEVE	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	UNDRAINED SHEAR STRENGTH, TSF							
												0.5	1.0	1.5	2.0	2.5			
	0			0.5" Asphalt over 8.5" Concrete				14.1											
				FILL: gray lean clay w/calcareous and ferrous nodules		95.7		20.4	49	21	28								
	5			Very stiff to hard gray LEAN CLAY (CL) w/calcareous and ferrous nodules and ferrous stains -very stiff 2'-4' -stiff 4'-8' -w/silt seams 6'-10'			105	24.8											
	10			-medium stiff to stiff 8'-10' -very stiff 10'-12' -reddish brown and gray 10'-15'	94.6	104	26.1	48	21	27									
	15			-medium stiff to stiff w/silt seams 13'-15'				24.0											
								26.4											

DEPTH TO WATER IN BORING :
 NO GROUNDWATER ENCOUNTERED DURING DRILLING.
 HOLE OPEN TO 15.0 FT. AT END OF DRILLING.

Geotest Engineering, Inc.

FIGURE A-1

LOG OF BORING NO. GB-2

PROJECT : Paving Improvements along Texas Avenue (FM 1765)
 from 14th Street to 6th Street
 City of Texas City, Galveston County, Texas

PROJECT NO. : 1140243301

LOCATION : See Plan of Borings (Figure 2)

COMPLETION DEPTH : 15.0 FT.

SURFACE ELEVATION : Existing Grade

DATE : 04-10-19

ELEVATION, FEET	DEPTH, FEET	SYMBOL	SAMPLES	DESCRIPTION OF MATERIAL	STANDARD PENETRATION TEST, BLOWS PER FOOT	PERCENT PASSING NO. 200 SIEVE	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	UNDRAINED SHEAR STRENGTH, TSF						
												0.5	1.0	1.5	2.0	2.5		
0	0	▨		0.5" Asphalt over 8.5" Concrete								△						
		▨		Stiff gray and brown LEAN CLAY WITH SAND (CL) w/ferrous stains				18.2				△						
		▨		-medium stiff to stiff 2'-4'				19.4				△						
	5	▨		-gray and yellowish brown 2'-15'	78.8	113	18.9	38	19	19		△	■					
		▨		-medium stiff 6'-8'				22.7				△						
		▨		-medium stiff to stiff 8'-10'				22.7				△						
	10	▨		-stiff to very stiff 10'-12'	75.8	110	21.9	35	17	18		△	■					
		▨						19.5				○	△					
	15	▨						19.8				○						

DEPTH TO WATER IN BORING :
 NO GROUNDWATER ENCOUNTERED DURING DRILLING.
 HOLE OPEN TO 15.0 FT. AT END OF DRILLING.

Geotest Engineering, Inc.

FIGURE A-2

LOG OF BORING NO. GB-3

PROJECT : Paving Improvements along Texas Avenue (FM 1765)
 from 14th Street to 6th Street
 City of Texas City, Galveston County, Texas

PROJECT NO. : 1140243301

LOCATION : See Plan of Borings (Figure 2)

COMPLETION DEPTH : 15.0 FT.

SURFACE ELEVATION : Existing Grade

DATE : 04-10-19

ELEVATION, FEET	DEPTH, FEET	SYMBOL SAMPLES	DESCRIPTION OF MATERIAL	STANDARD PENETRATION TEST, BLOWS PER FOOT	PERCENT PASSING NO. 200 SIEVE	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	UNDRAINED SHEAR STRENGTH, TSF									
											0.5	1.0	1.5	2.0	2.5					
0	0		0.5" Asphalt over 8.75" Concrete				17.6													
			FILL: stiff to very stiff gray lean clay with sand and ferrous stains -w/shell fragments 9.25"-2' -medium stiff 2'-4'		75.6		26.0	49	21	28										
	5		Medium stiff to stiff yellowish brown LEAN CLAY WITH SAND (CL) w/ferrous nodules and ferrous stains -soft 6'-10' -w/silt seams 8'-12' -soft to medium stiff 10'-12'			112	22.6													
	10						27.5													
	10						24.8													
	10				74.3	103	24.7	33	17	16										
	15		-w/silty sand layer 13'-15'				20.9													
	20																			
	25																			
	30																			
	35																			

DEPTH TO WATER IN BORING :
 NO GROUNDWATER ENCOUNTERED DURING DRILLING.
 HOLE OPEN TO 15.0 FT. AT END OF DRILLING.

Geotest Engineering, Inc.

FIGURE A-3

LOG OF BORING NO. GB-4

PROJECT : Paving Improvements along Texas Avenue (FM 1765)
 from 14th Street to 6th Street
 City of Texas City, Galveston County, Texas

PROJECT NO. : 1140243301

LOCATION : See Plan of Borings (Figure 2)

COMPLETION DEPTH : 15.0 FT.

SURFACE ELEVATION : Existing Grade

DATE : 04-10-19

ELEVATION, FEET	DEPTH, FEET	SYMBOL SAMPLES	DESCRIPTION OF MATERIAL	STANDARD PENETRATION TEST, BLOWS PER FOOT	PERCENT PASSING NO. 200 SIEVE	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	UNDRAINED SHEAR STRENGTH, TSF						
											0.5	1.0	1.5	2.0	2.5		
0	0		0.5" Asphalt over 8" Concrete				20.1				△						
	5		FILL: soft to medium stiff dark gray fat clay w/limestone and shell fragments -stiff gray and brown 4'-6'		96.9		32.3	50	20	30	△	○					
	10		Soft yellowish brown and gray FAT CLAY WITH SAND (CH) w/ferrous nodules and ferrous stains -soft to medium stiff 8'-10'		75.6	109	29.5	53	22	31	△	○	■				
	15		-w/sand seams 13'-15'			109	22.1				○	■					
							23.1										
							22.7										

DEPTH TO WATER IN BORING :
 NO GROUNDWATER ENCOUNTERED DURING DRILLING.
 HOLE OPEN TO 15.0 FT. AT END OF DRILLING.

Geotest Engineering, Inc.

FIGURE A-4

LOG OF BORING NO. GB-5

PROJECT : Paving Improvements along Texas Avenue (FM 1765)
 from 14th Street to 6th Street
 City of Texas City, Galveston County, Texas

PROJECT NO. : 1140243301

LOCATION : See Plan of Borings (Figure 2)

COMPLETION DEPTH : 15.0 FT.

SURFACE ELEVATION : Existing Grade

DATE : 04-10-19
















ELEVATION, FEET	DEPTH, FEET	SYMBOL	SAMPLES	DESCRIPTION OF MATERIAL	STANDARD PENETRATION TEST, BLOWS PER FOOT	PERCENT PASSING NO. 200 SIEVE	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	UNDRAINED SHEAR STRENGTH, TSF								
												0.5	1.0	1.5	2.0	2.5				
0	0			0.5" Asphalt over 9" Concrete				17.0												
	5			Stiff to very stiff gray and brown SANDY FAT CLAY (CH) -w/shell fragments 9.5"-2' -w/calcareous and ferrous nodules 2'-4'	60.7	113	17.6	52	21	31										
	10			Soft to medium stiff brown LEAN CLAY WITH SAND (CL) w/ferrous nodules and ferrous stains -medium stiff to stiff 6'-8' -soft 8'-12'	82.7	112	24.2	30	17	13										
	15			-w/silty sand seams 13'-15'				26.1												
								22.9												
								29.7												

DEPTH TO WATER IN BORING :
 NO GROUNDWATER ENCOUNTERED DURING DRILLING.
 HOLE OPEN TO 15.0 FT. AT END OF DRILLING.

Geotest Engineering, Inc.

FIGURE A-5

SYMBOLS AND TERMS USED ON BORING LOGS

SOIL TYPES (SHOWN IN SYMBOL COLUMN)								SAMPLER TYPES (SHOWN IN SAMPLES COLUMN)						
														
Asphaltic Concrete	Fill	Gravel	Sand	SILT	FAT CLAY	LEAN CLAY	Sandy LEAN CLAY	Pitcher Barrel	Nx Core	Shelby Tube	Piston	Split Spoon	No Recovery	Auger
Predominant type shown heavy														

TERMS DESCRIBING CONSISTENCY OR CONDITION

Basic Soil Type	Density or Consistency	Standard Penetration Resistance, ⁽¹⁾ Blows/ft.	Unconfined Compressive Strength (q _u), ⁽²⁾ Tons/sq. ft.
Cohesionless	Very loose	Less than 4	Not applicable
	Loose	4 to <10	Not applicable
	Medium dense	10 to <30	Not applicable
	Dense	30 to <50	Not applicable
	Very dense	50 or greater	Not applicable
Cohesive	Very soft	Less than 2	Less than 0.25
	Soft	2 to <4	0.25 to <0.5
	Firm/Medium stiff	4 to <8	0.5 to <1.0
	Stiff	8 to <15	1.0 to <2.0
	Very stiff	15 to <30	2.0 to <4.0
	Hard	30 or greater	4 or greater

(1) Number of blows from 140-lb. weight falling 30-in. to drive 2-in. OD, 1-3/8-in. ID, split barrel sampler (ASTM D1586)


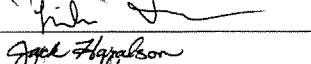
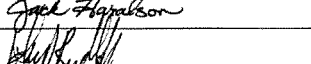
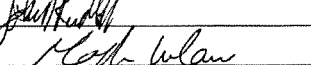
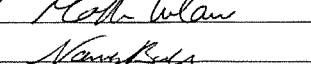
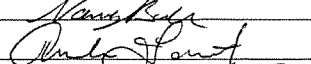
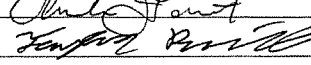
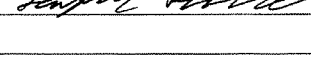
(2) q_u may also be approximated using a pocket penetrometer

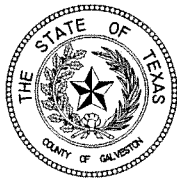
TERMS CHARACTERIZING SOIL STRUCTURE

Parting: -paper thin in size	Seam: -1/8" to 3" thick	Layer: -greater than 3"
Slickensided	- having inclined planes of weakness that are slick and glossy in appearance.	
Fissured	- containing shrinkage cracks, frequently filled with fine sand or silt; usually more or less vertical.	
Laminated	- composed of thin layers of varying color and texture.	
Interbedded	- composed of alternate layers of different soil types.	
Calcareous	- containing appreciable quantities of calcium carbonate.	
Well graded	- having wide range in grain sizes and substantial amounts of all intermediate particle sizes.	
Poorly graded	- predominantly of one grain size, or having a range of sizes with some intermediate size missing.	
Flocculated	- pertaining to cohesive soils that exhibit a loose knit or flakey structure.	

PRE-BID CONFERENCE
 TEXAS AVENUE RECONSTRUCTION
 GALVESTON COUNTY, TEXAS

Pre-bid Conference for Bid #B201007 will be held on Monday, October 28, 2019 at Galveston County Courthouse, Purchasing Department, 722 Moody, 5th Floor, Galveston, TX

PRINTED NAME	SIGNATURE	COMPANY NAME	E-MAIL ADDRESS	PHONE
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Lili Thoreson		Texas Sterling Construction	lili.thoreson@strlco.com	832-364-8145
JACK HARALSON		CITY OF TEXAS CITY	jharalson@texascitytx.gov	409-643-5310
John Rudloff		ARKK ENGINEERS	John.Rudloff@ARKKENGINEERS.COM	713-400-2755
Madhu Kilambi		ARKK ENGINEERS	Madhu.Kilambi@arkkengineers.com	713-400-2755
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Amber Forrest		R.G. Miller Engineers	aforrest@rgmiller.com	281-921-8756
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THE COUNTY OF GALVESTON

RUFUS G. CROWDER, CPPO, CPPB
PURCHASING AGENT

GWEN MCLAREN, CPPB
ASST. PURCHASING AGENT

COUNTY COURTHOUSE
722 Moody (21st Street)
Fifth (5th) Floor
GALVESTON, TEXAS 77550

November 7, 2019

PROJECT NAME: Texas Avenue Reconstruction

SOLICITATION NO: B201007

RE: ADDENDUM #2

To All Prospective Proposers,

The following information is being provided to aid in preparation of your proposal submittal(s):

Question #1: *Is there a geotechnical report?*

Response: The geotechnical report is attached with this addendum.

Question #2: *Time of Completion is stated to be within 300 calendar days of Notice to Proceed issuance. However, a date for when the Notice to Proceed is projected to be issued is not state. What is the estimated project start date?*

Response: The estimated start date is February of 2020.

Question #3: *Can you post the pre-bid meeting sign-in sheet please?*

Response: The pre-bid meeting sign-in sheet is attached with this addendum.

Question #4: *Are there soil boring available? Can you send me any pre-bid notes?*

Response: Please refer to the response to question #1. There are no pre-bid notes.

As a reminder, all questions regarding this proposal must be submitted in writing to:

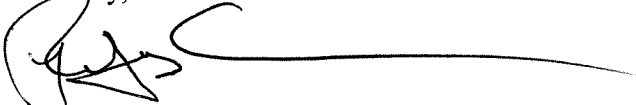
Rufus G. Crowder, CPPO CPPB
Galveston County Purchasing Agent
722 Moody, Fifth (5th) Floor
Galveston, Texas 77550
E-mail: purchasing.bids@co.galveston.tx.us

If you have any further questions regarding this proposal, please address them to Rufus Crowder, CPPO CPPB, Purchasing Agent, via e-mail at purchasing.bids@co.galveston.tx.us, or contact the Purchasing Department at (409) 770-5371.

If you have any further questions regarding this proposal, please address them to Rufus Crowder, CPPO CPPB, Purchasing Agent, via e-mail at purchasing.bids@co.galveston.tx.us, or contact the Purchasing Department at (409) 770-5371.

Please excuse us for any inconvenience that this may have caused.

Sincerely,

A handwritten signature in black ink, appearing to be 'Rufus G. Crowder', with a long horizontal flourish extending to the right.

Rufus G. Crowder, CPPO CPPB
Purchasing Agent
Galveston County

**GEOTECHNICAL INVESTIGATION
TEXAS AVENUE (FM 1765) RECONSTRUCTION
FROM 14TH STREET TO 6TH STREET
CITY OF TEXAS CITY, GALVESTON COUNTY, TEXAS**

REPORT NO. 1140243301

Reported to:

ARKK ENGINEERS, INC.

Houston, Texas

Reported by:

GEOTEST ENGINEERING, INC.

Houston, Texas

Key Map Nos. 738 G & H



GEOTEST ENGINEERING, INC.

Geotechnical Engineers & Materials Testing

5600 Bintliff Drive

Houston, Texas 77036

Telephone: (713) 266-0588

Fax: (713) 266-2977

Report No. 1140243301

June 6, 2019

Mr. Madhu Kilambi, P.E.
ARKK Engineers, Inc.
7322 Southwest Freeway, Suite 1040
Houston, Texas 77074

**Re: Geotechnical Investigation
Texas Avenue (FM 1765) Reconstruction
From 14th Street to 6th Street
City of Texas City, Galveston County, Texas**

Dear Mr. Kilambi:

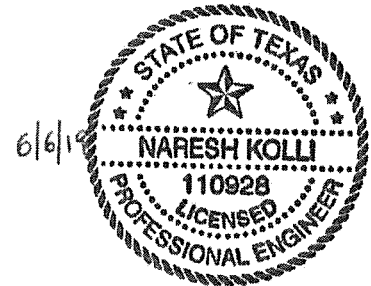
Presented herein is our geotechnical investigation report for the above referenced project. Preliminary field logs were submitted to you on April 17, 2019. This report supersedes all previously submitted reports, transmittals, etc. for the referenced project. This study was authorized by you on April 3, 2019, by accepting our Proposal No. 1140443399, dated March 26, 2019.

We appreciate this opportunity to be of service to you. If you have any questions regarding the report, or if we can be of further service to you, please call us.

Sincerely,
GEOTEST ENGINEERING, INC.
TBPE Registration No. F-410

Krishna M Pradeep, E.I.T.
Graduate Engineer

Naresh Kolli, P.E.
Project Manager



NK\kmp\lego

Copies Submitted: (1+1-pdf)

PC38\GEOTECHNICAL\40243301.DOC

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EXECUTIVE SUMMARY

A geotechnical investigation was conducted for the Texas Avenue (FM 1765) Reconstruction Project in the City of Texas City, Galveston County, Texas. The project includes reconstructing approximately 3,800 LF of existing 5-lane concrete paving along Texas Avenue (FM 1765) from 14th Street to 6th Street, with new concrete pavement. The project also includes storm sewer installation and water line replacement along Texas Avenue. Based on the information provided, we understand that the invert depth of the proposed storm sewer (24" RCP, 4' x 2' RCB, 5' x 2' RCB, and 7' x 2' RCB) ranges from approximately 4 to 6 feet, and will be installed primarily by open-cut method of construction. The proposed water line will be installed by trenchless (auger) method of construction.

This study included drilling and sampling of five (5) soil borings each to a depth of 15 feet, performing laboratory tests on recovered soil samples, performing engineering analyses and preparing a geotechnical report.

The principal findings and conclusions developed from this investigation are summarized below:

- The existing pavement along Texas Avenue from 14th Street to 6th Street, as obtained in borings GB-1 through GB-5 consists of 0.5 inches of asphalt over 8 to 9 inches of concrete.
- The subsurface soils below the existing pavement, as revealed by borings GB-1 through GB-5, consist of soft to hard gray, brown, reddish brown and gray, and yellowish brown and gray fat clay, fat clay with sand, sandy fat clay, lean clay, and lean clay with sand to the explored depth of 15 feet. Fill material consisting of gray and brown fat clay, lean clay, and lean clay with sand, calcareous and ferrous nodules, and shell fragments were encountered to depths ranging from 1 feet to 6 feet in borings GB-1, GB-3 and GB-4.
- No groundwater was encountered in the borings drilled for this investigation.
- All excavation operations should be in accordance with OSHA Standards, and Galveston

County Standard Specification, Section 01526, “Trench Safety Systems”.

- The bedding and backfill for the proposed utilities should be in accordance with ARKK Standard Specification, Section 02227, and Galveston County Standard Specification, Section 02227, “Excavation and Backfill for Utilities”.
- The auger pits/insertion and reception pits for the water line should be constructed as per the ARKK Standard Specifications Section 02317, “Auguring Pipe for Waterlines.”
- The foundation recommendations for new manholes are presented in Section 5.5 of this report.
- The recommended pavement section and subgrade stabilization for Texas Avenue (FM 1765) reconstruction are presented in Section 5.6 of this report.

1.0 INTRODUCTION

1.1 Location and Description of Project

A geotechnical investigation was conducted for the Texas Avenue (FM 1765) Reconstruction Project in the City of Texas City, Galveston County, Texas. The project location is bounded by 14th Street to the west, and 6th Street to the east in Galveston County, Texas within the Key Map Page No. 738 Grid G and H.

The project includes reconstructing approximately 3,800 LF of existing 5-lane concrete paving along Texas Avenue (FM 1765) from 14th Street to 6th Street, with new concrete pavement. The project also includes storm sewer installation and water line replacement along Texas Avenue. Based on the information provided, we understand that the invert depth of the proposed storm sewer (24" RCP, 4' x 2' RCB, 5' x 2' RCB, and 7' x 2' RCB) ranges from approximately 4 to 6 feet, and will be installed primarily by open-cut method of construction. The proposed water line will be installed by trenchless (auger) method of construction. The vicinity map of the project alignment is shown on Figure 1.

1.2 Scope of Work

The purpose of this investigation was to evaluate the soil and groundwater (if any) conditions along Texas Avenue in the City of Texas City, and to provide geotechnical recommendations for the proposed roadway reconstruction and utilities replacement. The scope of this investigation consisted of the following tasks:

- Cored the existing pavement at five (5) locations along Texas Avenue to obtain the existing pavement thickness and for boring access.
- Drilled and sampled five (5) soil borings each to a depth of 15 feet along Texas Avenue (FM 1765) from 14th Street to 6th Street.

- Performed appropriate laboratory tests on selected representative soil samples to develop the engineering properties of the soil.
- Performed engineering analyses to develop geotechnical recommendations for pavement thickness including subgrade stabilization for the pavement construction, bedding and backfill and water level control for open cut construction for storm sewer and water line installation.
- Prepared a geotechnical investigation report including field and laboratory data and geotechnical recommendations.

2.0 FIELD EXPLORATION

Subsurface conditions along the project alignment were investigated by drilling a total of five (5) soil borings (GB-1 through GB-5) drilled each to a depth of 15 feet below existing pavement. All borings were drilled with a truck-mounted rotary drilling rig. Pavement coring was performed at each boring location to verify the existing pavement thickness and to access the subsurface soils. All the boring locations are shown on Plan of Borings, Figure 2. Survey information for the completed borehole locations was not available to us at the time of preparation of this report.

Samples were taken at continuous 2-foot intervals to a depth of 15 feet. Cohesive soil samples were obtained with a 3-inch diameter thin-walled tube sampler in general accordance with ASTM D1587. Each sample was removed from the sampler in the field, carefully examined and logged by an experienced soils technician. Suitable portions of each sample were then sealed and packaged for transportation to Geotest's laboratory. The shear strength of cohesive soil samples was estimated using a calibrated hand penetrometer in the field. After taking water level measurements (if any), all borings were grouted with cement bentonite grout.

Detailed descriptions of the soils encountered along the project alignment are given on the boring logs GB-1 through GB-5 and are presented on Figures A-1 through A-5 in Appendix A. A key to symbols and terms used on the boring logs is presented on Figure A-6 in Appendix A.

Groundwater level observations were made at each boring location during field investigation. The results of these observations are noted on the boring logs.

3.0 LABORATORY TESTING PROGRAM

The laboratory testing program was designed to evaluate the pertinent physical properties and shear strength characteristics of the subsurface soils. Classification tests were performed on selected samples to aid in soil classification.

Undrained shear strengths of selected cohesive samples were measured by unconsolidated undrained (UU) triaxial compression tests (ASTM D2850). The results of the UU triaxial compression tests are plotted on the boring logs as solid squares. The shear strength of cohesive samples was measured in the field with a calibrated hand penetrometer and also in the laboratory with a Torvane. The shear strength values obtained from the penetrometer and Torvane are plotted on the boring logs as open circles and triangles, respectively.

Moisture content and dry unit weight were measured for each unconfined compression test and UU triaxial compression test samples. Moisture content measurements (ASTM D2216) were also made on other samples to establish the moisture profile at each boring location. Atterberg limit tests (ASTM D4318) were performed on soil samples to measure plasticity characteristics. Percent passing No. 200 sieve (ASTM D1140) tests were also performed on selected samples. The result of all these tests are plotted or summarized on the boring logs GB-1 through GB-5 and are presented on Figures A-1 through A-5 in Appendix A.

4.0 GENERAL SUBSURFACE CONDITIONS

4.1 Existing Pavement

The existing pavement along Texas Avenue from 14th Street to 6th Street, as obtained in borings GB-1 through GB-5 consists of 0.5 inches of asphalt over 8 to 9 inches of concrete. The details of the pavement encountered at each boring location are presented below.

Street	Boring Nos.	Asphalt Surface Thickness (in.)	Concrete Thickness (in.)	Total (in.)
Texas Avenue	GB-1	0.5	8.5	9.0
	GB-2	0.5	8.5	9.0
	GB-3	0.5	8.75	9.25
	GB-4	0.5	8.0	8.5
	GB-5	0.5	9.0	9.5

4.2 Subsurface Soil

The subsurface soils below the existing pavement, as revealed by borings GB-1 through GB-5, consist of soft to hard gray, brown, reddish brown and gray, and yellowish brown and gray fat clay, fat clay with sand, sandy fat clay, lean clay, and lean clay with sand to the explored depth of 15 feet. Fill material consisting of gray and brown fat clay, lean clay, and lean clay with sand, calcareous and ferrous nodules, and shell fragments were encountered to depths ranging from 1 feet to 6 feet in borings GB-1, GB-3 and GB-4.

The fat clay, fat clay with sand, and sandy fat clay are of high plasticity with liquid limits ranging from 50 to 53 and plasticity indices ranging from 30 to 31. The lean clay and lean clay with sand are of medium plasticity with liquid limits ranging from 30 to 49 and plasticity indices ranging from 13 to 28. The fines content (passing No. 200 sieve) of fat clay and lean clay ranges from 95 to 97 percent. The fines content of fat clay with sand and lean clay with sand ranges from 74 to 83 percent, and the fines content of sandy fat clay was about 61 percent.

4.3 Water Levels

No groundwater was encountered in the borings drilled for this investigation. However, it should be noted that various environmental and man-made factors such as amount of precipitation, nearby subsurface construction activities, and change in area drainage can substantially influence the groundwater level.

5.0 GEOTECHNICAL RECOMMENDATIONS

5.1 General

The project includes reconstructing approximately 3,800 LF of existing 5-lane concrete paving along Texas Avenue (FM 1765) from 14th Street to 6th Street, with new concrete pavement. The project also includes storm sewer installation and water line replacement along Texas Avenue. Based on the information provided, we understand that the invert depth of the proposed storm sewer (24" RCP, 4' x 2' RCB, 5' x 2' RCB, and 7' x 2' RCB) ranges from approximately 4 to 6 feet, and will be installed primarily by open-cut method of construction. The proposed water line will be installed by trenchless (auger) method of construction.

5.2 Open-Cut Excavation

5.2.1 Geotechnical Parameters. Based on the soil conditions revealed by the borings, geotechnical parameters were developed for the design of open cut excavation for the proposed storm sewer, and auger (insertion/reception) pits planned for the trenchless installation. The geotechnical design parameters for open cut excavation for auger (insertion/reception) pits are provided in Table 1. For design, the groundwater level should be assumed to exist at the ground surface, since this condition may exist after a heavy rain or flooding.

5.2.2 Excavation Stability. The open excavations may be shored, laid back to a stable slope or some other equivalent means used to provide safety for workers and adjacent structures. The excavating and trenching operations should be in accordance with OSHA Standards, OSHA 2207, Subpart P, latest revision and Galveston County Standard Specification, Section 01526, "Trench Safety Systems".

- Excavation Shallower Than 5 Feet – For excavations that are less than 5 feet, the need for protection should be evaluated by a competent person to examine the ground for any indication of ground movement or potential cave-in. When any indication of hazardous ground movement or potential cave-in is anticipated during construction,

adequate protective system should be provided for all excavation even that if the excavations are shallower than 5 feet.

- Excavation Deeper Than 5 Feet - Excavations that are deeper than 5 feet should be sloped, shored, sheeted, braced or laid back to a stable slope or supported by some other equivalent means or protection such that workers are not exposed to moving ground or cave-ins. The slopes and shoring should be in accordance with the trench safety requirements per OSHA Standards. The following items provide design criteria for trench stability.
 - (i) OSHA's Soil Type. Based on the soil conditions revealed by the borings and the assumed groundwater level at surface, OSHA's soil type "C" should be used for the determination of allowable maximum slope and/or the design of a shoring system. For shoring deeper than 20 feet, an engineering evaluation is required.
 - (ii) Excavation Support Earth Pressure. Based on the subsurface conditions indicated by this investigation and laboratory testing results, the excavation support earth pressure diagram was developed and is presented on Figure 5. The pressure diagram can be used for the design of temporary excavation bracing. For a trench box, a lateral earth pressure resulting from an equivalent fluid with a unit weight of 97 pcf is recommended. The above value of equivalent fluid pressure is based upon an assumption that the groundwater level is near the ground surface, since these conditions may exist after a heavy rain or flooding. Effect of surcharge loads at the ground surface should be added to the computed lateral earth pressure. A surcharge load, q , will typically result in a lateral load equal to $0.5 q$.
 - (iii) Bottom Stability. In braced cuts, if tight sheeting is terminated at the base of the cut, the bottom of the excavation can become unstable under certain conditions. The stability of the trench bottom is governed by the shear strength of the soils and by the differential hydrostatic head. For cuts in cohesive soils as encountered in the

borings for excavation depths of 4 to 6 feet, stability of the bottom can be evaluated in accordance with the procedure outlined on Figure 6.

5.2.3 Groundwater Control. Excavations for the proposed utilities installation may encounter groundwater seepage to varying degrees depending on groundwater conditions at the time of construction and the location and depth of excavation. Based on the soil conditions identified in the borings for the proposed utilities installation, all the excavations will be in cohesive soils. In general, for cohesive soils as encountered in all the borings for the excavation depths (maximum depth of 6 feet), groundwater (if encountered) may be managed by collection in excavation bottom sumps for pumped disposal.

The contractor should verify the groundwater level at the time of construction and should provide an adequate dewatering system, where required. The groundwater control should be carried out in accordance with the ARKK Standard Specifications, Section 01563, and Galveston County Standard Specification, Section 01563, "Control of Ground Water and Surface Water".

5.2.4 Live Loads on Pipe Due to Traffic. Loads on pipe due to traffic (if any) should be considered. A graph providing calculated vertical stress on pipe due to traffic loads is given on Figure 7.

5.2.5 Bedding and Backfill for Utilities. The bedding and backfill for the storm sewer and water line should be in accordance with ARKK Standard Specification, Section 02227, and Galveston County Standard Specification, Section 02227, "Excavation and Backfill for Utilities".

5.2.6 Bedding and Backfill for the Auger Pits/Insertion and Receiving Pits. The auger pits or insertion and receiving pits should be constructed and backfilled in accordance with ARKK, Standard Specification Section, 02317, "Auguring Pipe for Waterlines."

5.3 Trenchless Installation

It is understood that the proposed water line will be replaced by auger method of construction. The trenchless method of construction should be per ARKK, Specification Section

02317, “Augering Pipe for Water Lines.”

5.3.1 Geotechnical Parameters. Based on the soil conditions revealed by soil borings (GB-1 through GB-5), laboratory test data and geotechnical design parameters were developed for cohesive soils and are provided in Table 2. The cohesive soils include fat clay, fat clay with sand, sandy fat clay, lean clay, and lean clay with sand. For design conditions, the groundwater level should be assumed to exist at the ground surface.

5.3.2 Earth Pressure on Pipe Casing. The earth pressures on augering should be determined from Figure 8. Equations to calculate the pipe casing loads are also shown on Figure 8.

5.3.3 Carrier Pipe Design Parameters. Carrier pipe must be sufficiently strong to withstand anticipated long-term ground loads and must not be subjected to deterioration by substance either in ground or in the auger casing. The carrier pipe design should include consideration of not only the loads applied to the pipe but also factors other than soil loading. These factors could include minimum structural code requirements, loading from augering and other construction loads. The drained geotechnical design parameters given in Table 2 should be used to analyze the soil structure intersection of the carrier pipe.

5.3.4 Influence of Augering on Adjacent Structures. Surface and near-surface structures near the tunnel alignment consist primarily of private properties, city streets and public and private utilities.

Ground movement, in terms of loss of ground or ground lost, is commonly associated with soft ground tunneling. If such ground movement is excessive, it may cause damage to the structures, roads and services located above the tunnel. While ground movement cannot be eliminated, it can be controlled within certain limits by the use of proper construction techniques and good quality workmanship. These include, but are not limited to, prevention of excessive ground loss during tunneling with the use of grouting and filling the annular space between the pipe or casing and the surrounding soil and prevention of undue loss of fines through dewatering.

The selection and execution of tunneling methods that are best suited to anticipated ground conditions along the proposed tunnel are, in fact, the contractor's primary contribution to successful completion of the proposed auger or directional drilling. On review of the boring logs, the ground conditions for tunneling (excavation face) will be primarily through cohesive soils. The cohesive soils as encountered in borings GB-1 through GB-5 consist of soft to hard gray, brown, reddish brown and gray, and yellowish brown and gray fat clay, fat clay with sand, sandy fat clay, lean clay, and lean clay with sand, and the ground in this area may be expected to behave as firm to raveling ground near the invert. Close monitoring of ground movement should be carried out during the trenchless installation.

The ground conditions for trenchless operation (excavation face) will be through predominantly in cohesive soils near borings GB-1 through GB-5. However, due to spacing of borings, soil conditions other than those encountered in borings could exist.

The proposed auger is parallel with or cross beneath utility lines. The largest potential problems from utilities may result from:

- Leaking water pipes
- Gas pipe breakage leading to a potential explosion
- Breakage of storm or sanitary sewers

In general, it is the contractor's responsibility to investigate these and other possible third party interactions along the proposed tunnel alignment and to accommodate all of these interactions with the use of good construction methods.

5.4 Piping System Thrust Restraint

Unbalanced thrust forces will occur at any point in the pipe where the direction or cross sectional area of the flow changes. The force diagram shown in Figure 9 illustrates the thrust force generated by flow at a bend in the pipe. The equations for computing this thrust force are also given in this figure. The thrust force will often require more resistance or support than is available just from the pipe bearing against the backfill. In order to prevent intolerable

movement and overstressing of the pipe, suitable buttressing should be provided.

Proposed horizontal bends may require restraint in addition to that supplied by the pipe bearing on the backfill. In general, thrust blocks, both horizontal and vertical and restrained joints are common methods of supplying additional reaction. However, it is noted that restrained joints are considered for supplying additional reaction for the project and is discussed below.

5.4.1 Restrained Joints. Where thrust blocks are not practical, restrained joints, allowing thrust and shear forces to be transmitted across the pipe joints, are employed to allow a number of pipe sections to act integrally in bearing. The equations necessary to determine the restrained pipe length on each side of the bend are given below:

$$L = \frac{PA \sin(\theta / 2)}{f(2W_e + W_p + W_w)}$$

- where,
- L = restrained pipe length on each side of the bend, in feet
 - P = internal pressure, in pounds per square inch
 - A = cross sectional area of first unrestrained pipe joint, in square inches
 - θ = deflection angle of bend, in degrees
 - f = co-efficient of friction between pipe and soil (recommended 0.3)
 - W_e = overburden load, in pounds per liner foot = $\Upsilon_b B_c H$
 - W_p = weight of pipe, in pounds per linear foot
 - W_w = weight of water in pipe, in pounds per linear foot
 - Υ_b = wet unit weight of backfill material, in pounds per cubic foot
(recommended 120 pcf)
 - B_c = pipe outer diameter, in feet
 - H = earth cover, in feet

Reinforced concrete encasement may be used in lieu of the manufactured joint restrained system. The equations and soil parameters given above can be used for the design of reinforced concrete encasement.

5.5 Structures

5.5.1 Description. The structure associated with this project will be new manholes. The new manholes for the proposed utilities will be placed at depths ranging from 4 to 6 feet below existing pavement (elevations ranging from approximately 1.0 to 2.2 feet).

5.5.2 Foundation Conditions. Based on the soil conditions revealed by the borings GB-1 through GB-5, the manholes bottom will be in medium stiff to very stiff lean clay, lean clay with sand, sandy fat clay, and fat clay fill soils.

5.5.3 Foundation Design Recommendations. The following items provide recommendations and design criteria for construction of the new manholes.

- Allowable Bearing Pressures. The mat foundation for supporting the new manholes placed at depths ranging from 4 to 6 feet [into medium stiff to very stiff lean clay, lean clay with sand, sandy fat clay, and fat clay] should be designed for an allowable (net) bearing pressure of 1,850 psf. The allowable bearing pressure includes a safety factor of 2.0.

The above recommendation assumes that the final bearing surfaces consist of undisturbed natural soils and that underlying semi-transmissive zones are properly pressure-relieved and stable undisturbed bearing surfaces are attained.

- Bottom Stability. In braced cuts, if tight sheeting is terminated at the base of the cut, the bottom of the excavation can become unstable. The parameters that govern the stability of the excavation base are the soil shear strength and the differential hydrostatic head between the water level within the retained soils and the water level at the interior of the trench excavation. For cuts in cohesive soils as predominantly encountered in the borings, the bottom stability can be evaluated as outlined on Figure 6.

- Lateral Earth Pressure. The pressure diagram presented on Figure 5 can be used for the design of braced excavation. The lateral earth pressure diagram presented on Figure 10 is applicable for the design of the permanent walls.

- Hydrostatic Uplift Resistance. Structures extending below the water level should be designed to resist uplift pressure resulting from excess piezometric head. Design uplift pressures should be computed based on the assumption that the water table is at ground surface. To resist the hydrostatic uplift at the bottom of the structure, one of the following sources of resistance can be utilized in each of the designs.
 - a. Dead weight of structure,
 - b. Weight of soil above base extensions plus weight of structure, or
 - c. Soil-wall friction plus dead weight of structure.

The uplift force and resistance to uplift should be computed as detailed on Figure 11. In determining the configuration and dimensions of the structure using one of the approaches presented on Figure 11, the following factors of safety are recommended.

- a. Dead weight of concrete structure, $S_{F1} = 1.10$,
- b. Weight of soil (backfill) above base extension, $S_{F2} = 1.5$, and
- c. Soil-wall friction, $S_{F3} = 3.0$.

Friction resistance should be discounted for the upper 5 feet, since this zone is affected by seasonal moisture changes.

5.5.4 Protection of Below Grade Structures. The design of the proper means for protection of below grade structures will depend upon the potential of the aggressivity or corrosivity of soil and groundwater properties. Aggressivity testing was not within the scope of this investigation. The design of the protection of below grade structures is beyond the scope of services for this investigation.

5.5.5 Water Level Control During Construction. Water level control should be in accordance with section 5.2.3 of this report.

5.5.6 Structure Backfill. Excavations for the proposed structures should be backfilled in accordance with the ARKK Standard Specifications, and Galveston County Standard Specification, Section 02226, "Excavation and Backfill for Structures."

5.6 Pavement Structure Design

We understand that the existing 5-lane concrete paving along Texas Avenue (FM 1765) from 14th Street to 6th Street, will be reconstructed with new concrete pavement with curb and gutter. The pavement design presented below was developed in accordance with "AASHTO Guide for Design of Pavement Structures," 1993 Edition.

5.6.1 Design Parameters

Subgrade Soil Properties. California Bearing Ratio (CBR) tests were not within the scope of this project. Therefore, the roadbed soil resilient modulus is estimated based on physical properties and strength characteristics of the natural subgrade soils. Based on the physical properties and strength characteristics of the natural subgrade soils obtained from laboratory tests, the effective roadbed soil resilient modulus (M_R) was estimated to be about 1,941 psi from an assumed CBR value of 1.0. Based on an estimated resilient modulus of the 8-inch lime-stabilized subgrade, the effective modulus of subgrade reaction (k) is estimated to be about 49 pci.

Traffic Data. No traffic count and vehicle classification data was provided to us at the time of preparation of this report. Based on the information provided by ARKK, the new concrete pavement section will be constructed in general accordance with a standard pavement design. A traffic loading of 6.2×10^6 kips ESALs was calculated over a 20-year design period and was utilized for the

pavement design.

Other Design Parameters. Other design parameters used in the development of rigid pavement thickness are given below:

Material Properties of Concrete:

Modulus of Elasticity of Concrete (E_c): 3,604,997 psi

Mean value of Modulus of Rupture of Concrete after 28 days

(S'_c): 630 psi (based on compressive strength of 4,000 psi)

Load Transfer coefficient (J): 2.7

Drainage coefficient (C_d): 1.2

Overall Standard Deviation (S_o): 0.35

Reliability Level (R): 90%

Serviceability Index

Initial (P_o): 4.5

Terminal (P_t): 2.25

Reinforcement Variables

Allowable Working Stress (f_s): 45,000 psi (grade 60 steel)

Friction Factor (F): 1.8

5.6.2 Recommended Pavement Section

Based on the design parameters described above and the AASHTO design, the thickness of rigid pavement was determined. The recommended pavement section is given below:

Pavement Course	Thickness, inches
Reinforced Concrete	8
5% Lime-stabilized subgrade	8

For the 8-inch concrete pavement, the required longitudinal reinforcing steel for an expansion joint spacing of 80 feet and transverse reinforcement steel for a pavement width of 24

feet back to back are given below for the grade 60 steel.

Pavement Thickness (Inches)	Longitudinal Steel	Transverse Steel
	Center to Center Spacing (in)	Center to Center Spacing (in)
	# 5 bars	# 5 bars
8	24	30

5.6.3 Preparation of Pavement Subgrade

Based on the field and laboratory test data, the subgrade soils below the existing pavement sections consist of high plasticity lean clay, lean clay with sand, fat clay, fat clay with sand and sandy fat clay. These subgrade soils have high volume change potential. Hence, lime stabilization of the fat clay and lean clay subgrade soils will be required to reduce the swelling and shrinkage potential, to accelerate the construction and provide a stable subgrade on which to construct the pavement sections. The fat clay subgrade soils should be stabilized with 5 percent lime (by dry unit weight of soil) to a depth of at least 8 inches. This corresponds to approximately 33 pounds of lime per square yard based on a dry unit weight of 110 pcf. The actual percentage of lime should be confirmed by laboratory tests at the time of construction.

Subgrade preparation for the proposed pavement after removing the existing pavement should consist of stripping, proof-rolling, and stabilization. The following procedures for subgrade preparation are recommended:

1. Strip the surficial soils to a suitable depth to remove all surficial vegetation and achieve grade. In isolated areas where soft, compressible, or very loose soils are encountered, additional stripping may be required.
2. After stripping, the exposed surface should be proof-rolled with a minimum of 3 passes of a 30-ton pneumatic-tired roller or a partially loaded truck utilizing a tire pressure of approximately 90 psi. If rutting develops, the tire pressure should be reduced. The purpose of the proof-rolling operation is to identify any

underlying zones or pockets of soft soils so these weak materials can be removed and replaced.

3. Lime stabilization of cohesive subgrade should be performed in accordance with ARKK Standard Specification, Section 02241, "Lime Stabilized Subgrade".

6.0 PROVISIONS

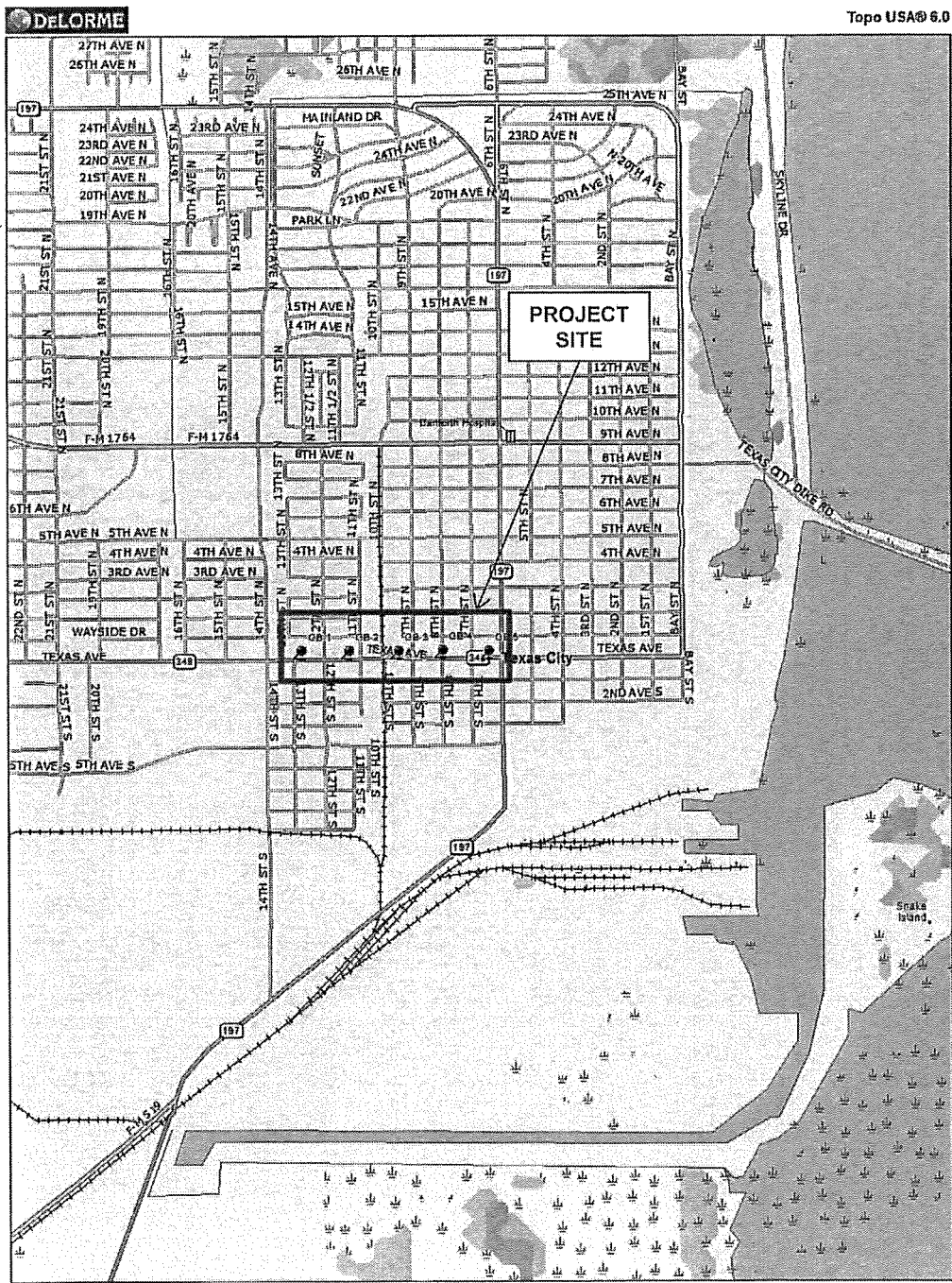
The description of subsurface conditions and the design information contained in this report are based on the test borings made at the time of drilling at specific locations. However, some variation in soil conditions may occur between test borings. Should any subsurface conditions other than those described in our boring logs be encountered, Geotest should be immediately notified so that further investigation and supplemental recommendations can be provided. The depth of the groundwater level may vary with changes in environmental conditions such as frequency and magnitude of rainfall. The stratification lines on the log of borings represent the approximate boundaries between soil types, however, the transition between soil types may be more gradual than depicted.

This report has been prepared for the exclusive use of ARKK Engineers, Inc, for the Texas Avenue (FM 1765) Reconstruction in City of Texas City, Texas.

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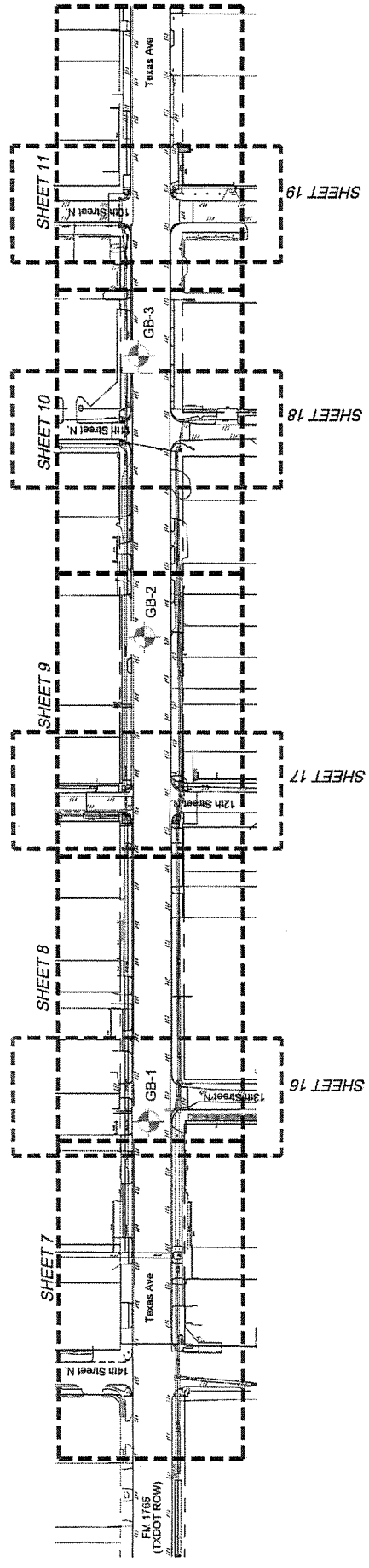
0 800 1600 2400 3200 4000 ft
 Data Zoom 13-0

PAVING IMPROVEMENTS ALONG TEXAS AVENUE (FM 1765)
 FROM 14TH STREET TO 6TH STREET
 CITY OF TEXAS CITY, GALVESTON COUNTY, TEXAS

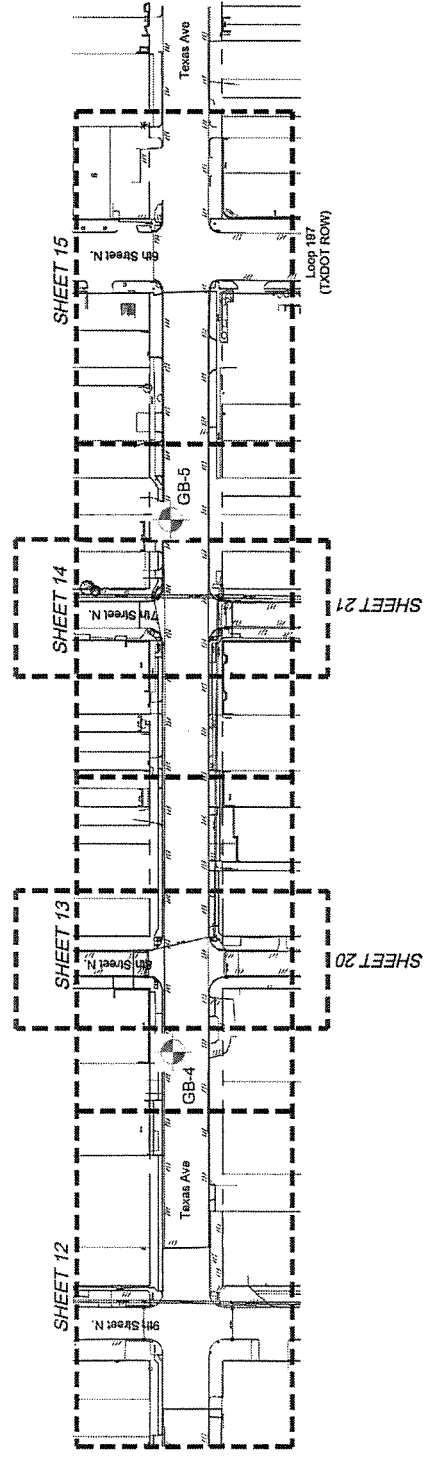
VICINITY MAP

Geotest Engineering, Inc.

FIGURE 1



LEGEND
 Boring



DATE	DESCRIPTION	DATE	BY

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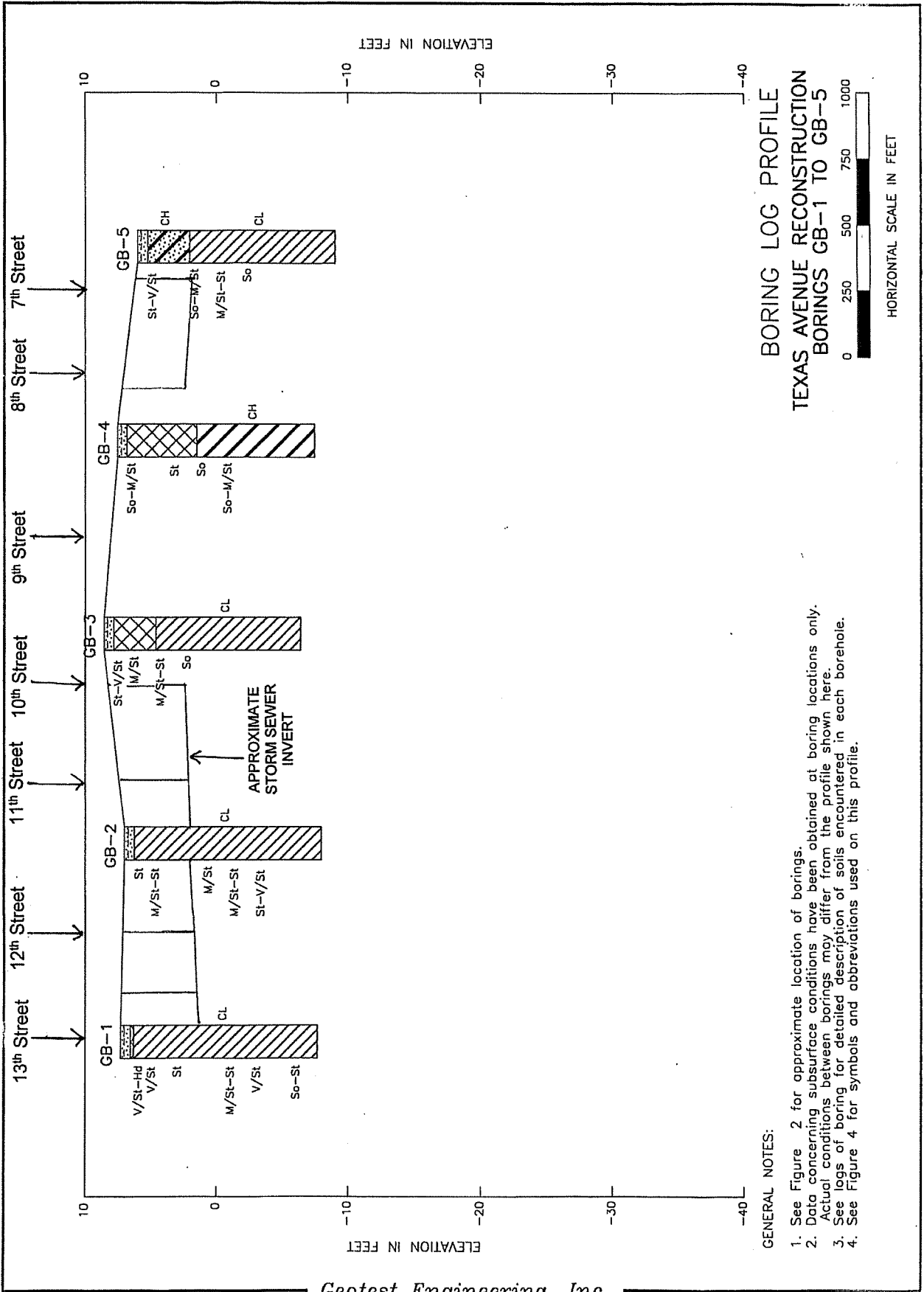
ARIK ENGINEERS
 2225 West Loop, Suite 2000, Dallas, Texas 75201
 (214) 343-1100 • www.arikengineers.com • P&ID No. 1140243301

Galveston County, Texas
 Texas Avenue Reconstruction

Overall Layout Plan

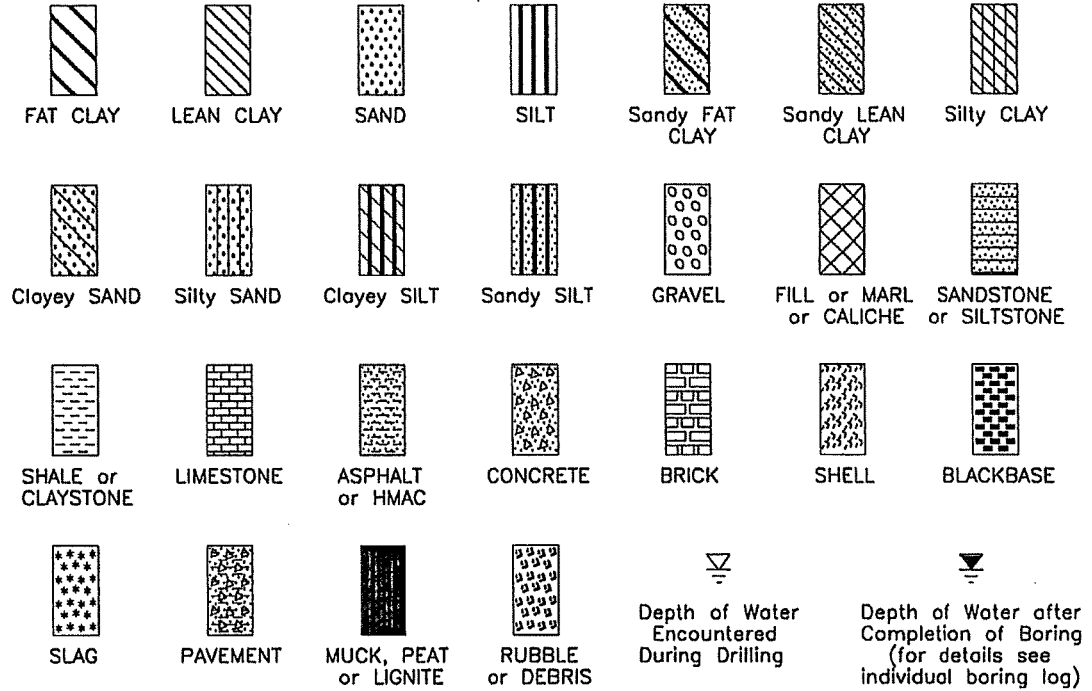
Job No.: 1140243301
 Date: April, 2019
 Drawn By: D. Easton
 Checked By: J. Ruskoff
 Scale: 1" = 100'

FIGURE 2



SYMBOLS AND ABBREVIATIONS USED ON BORING LOG PROFILE

LEGEND



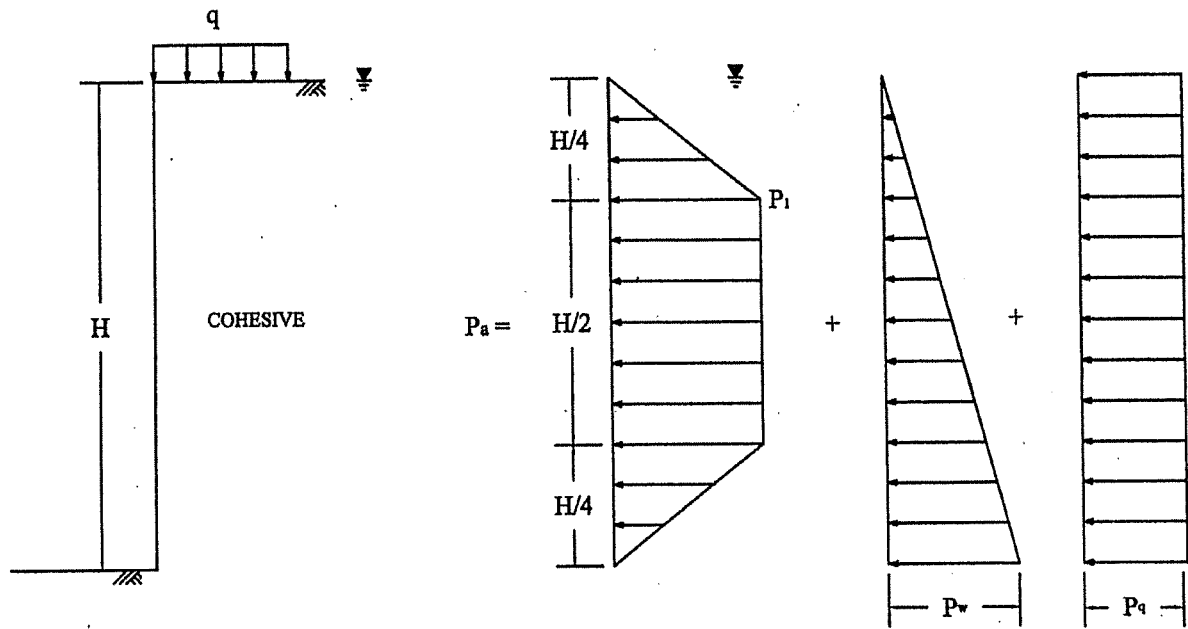
ABBREVIATIONS USED FOR CONSISTENCY/DENSITY

COHESIVE SOILS

V/So : Very Soft
 So : Soft
 Fm : Firm
 M/St : Medium Stiff
 St : Stiff
 V/St : Very Stiff
 Hd : Hard
 V/Hd : Very Hard

COHESIONLESS SOILS

V/Lo : Very Loose
 Lo : Loose
 S/Co : Slightly Compact
 Co : Compact
 M/De : Medium Dense
 De : Dense
 V/De : Very Dense



TYPICAL SOIL PARAMETERS

See Table 1 for typical values of soil parameters

BRACED WALL

For $\gamma H/c \leq 4$

$$P_1 = 0.3 \gamma' H$$

$$P_w = \gamma_w H = 62.4 H$$

$$P_q = 0.5 q$$

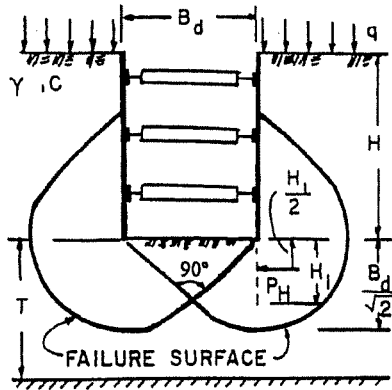
Where:

- γ' = Submerged unit weight of cohesive soil, pcf;
- γ_w = Unit weight of water, pcf;
- q = Surcharge load at surface, psf;
- P_a = Lateral pressure, psf;
- P_1 = Active earth pressure, psf;
- P_q = Horizontal pressure due to surcharge, psf;
- P_w = Hydrostatic pressure due to groundwater, psf;
- H = Depth of braced excavation, feet
- c = Shear strength of cohesion soil, psf;

TRENCH SUPPORT EARTH PRESSURE

SUBMERGED COHESIVE SOIL

CUT IN COHESIVE SOIL,
 DEPTH OF COHESIVE SOIL UNLIMITED ($T > 0.7 B_d$)
 L = LENGTH OF CUT



If sheeting terminates at base of cut:

$$\text{Safety factor, } F_s = \frac{N_c C}{\gamma H + q}$$

N_c = Bearing capacity factor, which depends on dimensions of the excavation : B_d , L and H (use N_c from graph below)

C = Undrained shear strength of clay in failure zone beneath and surrounding base of cut

γ = Unit weight of soil (see Table 1)

q = Surface surcharge (assumed q = 500 psf)

If safety factor is less than 1.5, sheeting or soldier piles must be carried below the base of cut to insure stability - (see note)

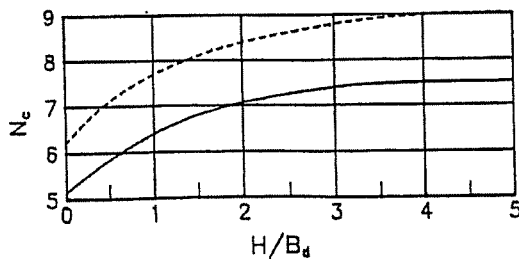
$$H_1 = \text{Buried length} = \frac{B_d}{2} \geq 5 \text{ feet}$$

Note : If soldier piles are used, the center to center spacing should not exceed 3 times the width or diameter of soldier pile .

Force on buried length, P_H :

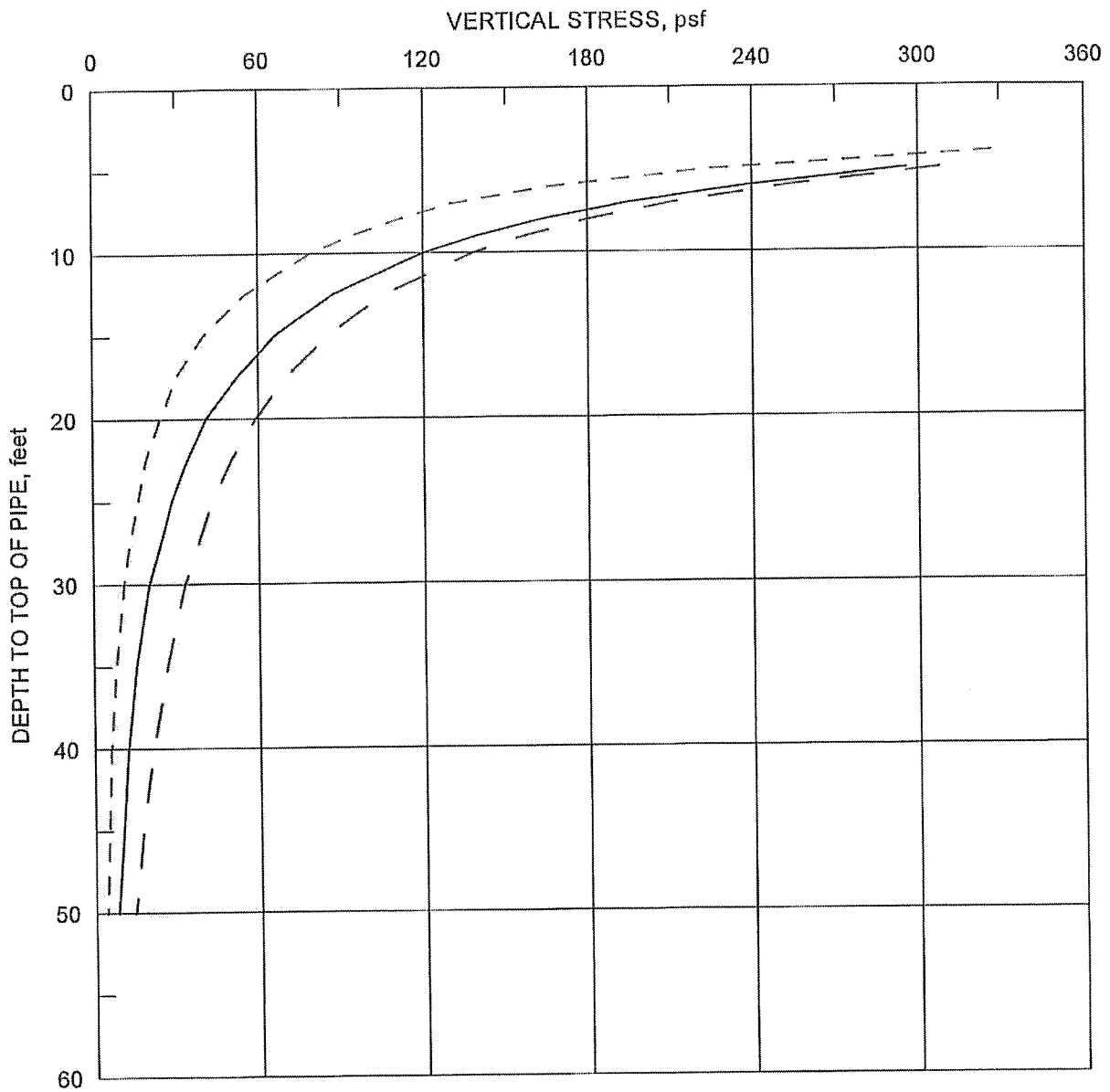
$$\text{If } H_1 > \frac{2 B_d}{3 \sqrt{2}}, P_H = 0.7 (\gamma H B_d - 1.4 C H - \pi C B_d) \text{ in lbs/ linear foot}$$

$$\text{If } H_1 < \frac{2 B_d}{3 \sqrt{2}}, P_H = 1.5 H_1 \left(\gamma H - \frac{1.4 C H}{B_d} - \pi C \right) \text{ in lbs/ linear foot}$$



— For trench excavations
 - - - For square pit or circle shaft

STABILITY OF BOTTOM
 FOR
 BRACED CUT



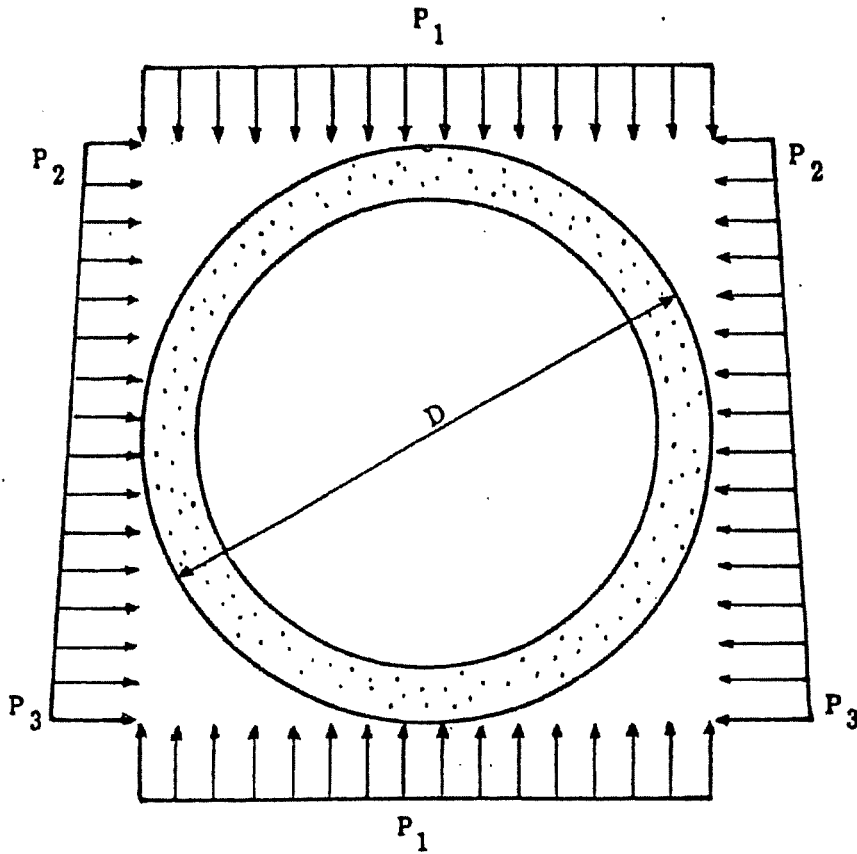
Legend:

- - - - - One Pass HS20
- Two Pass HS20
- . - . - Four Pass HS20

Notes:

1. Based on standard AASHTO H20 or HS20 dual wheel truck axle loadings
2. The vertical stress was estimated by using Westergaard solution

VERTICAL STRESS ON PIPE
DUE TO TRAFFIC LOAD



$$P_1 = [(H + \frac{D}{2}) \times (\gamma - \gamma_w) + D_w \times \gamma_w] + q_s, \text{ for } D_w < H + \frac{D}{2}$$

$$P_1 = [(H + \frac{D}{2}) \times \gamma] + q_s, \text{ for } D_w \geq H + \frac{D}{2}$$

$$P_2 = (H \times \gamma) + q_s$$

$$P_3 = [(H + D) \times \gamma] + q_s$$

Where: P_1, P_2, P_3 = Tunnel liner load, psf.

D = Tunnel outside diameter, ft.

H = Depth to top of tunnel; ft.

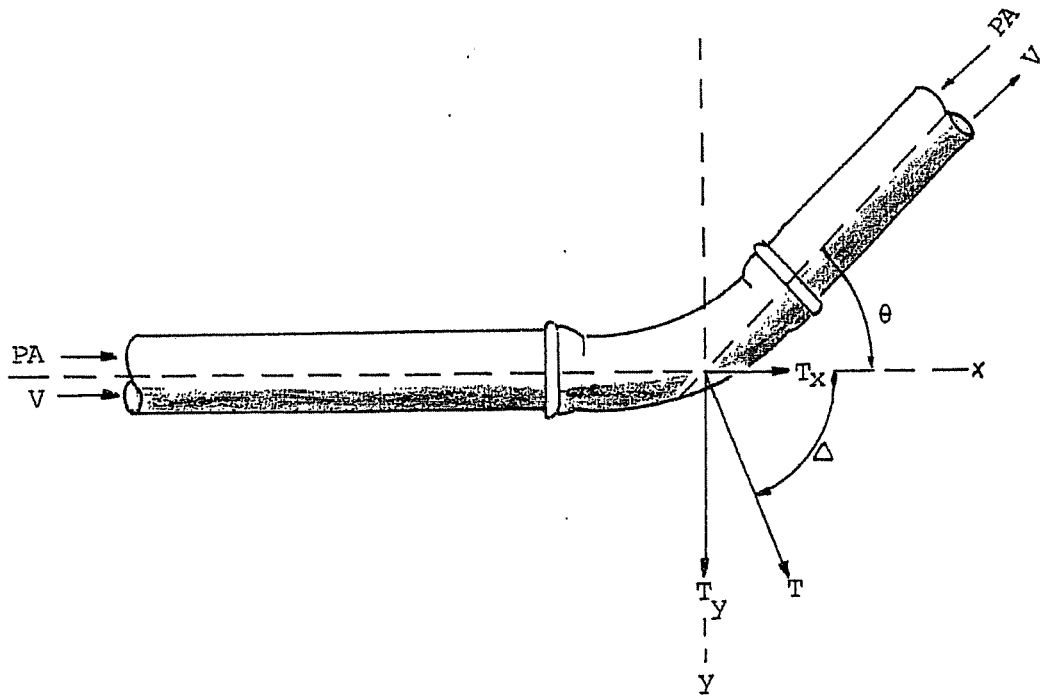
D_w = Depth to ground water level; ft.

γ = Wet unit weight of soil, pcf (see Table 2)

γ_w = Unit weight of water, 62.4 pcf

q_s = Surcharge load, psf.

EARTH PRESSURE ON AUGERING



$$T_x = PA (1 - \cos \theta)$$

$$T_y = PA \sin \theta$$

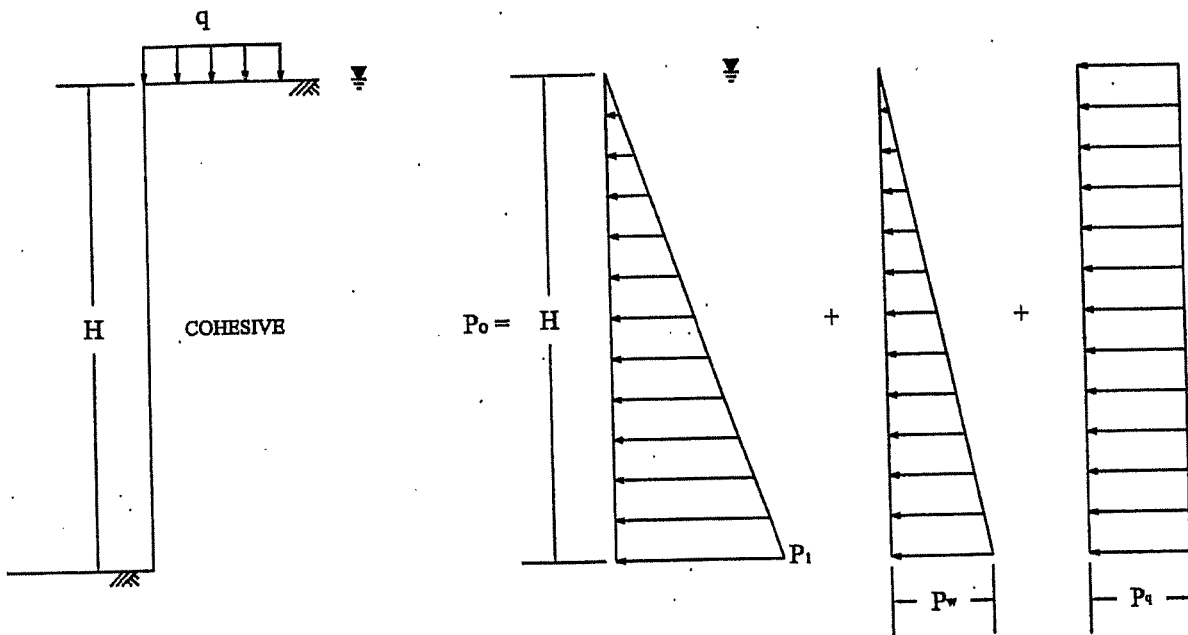
$$T = 2 PA \sin \frac{\theta}{2}$$

$$\Delta = (90 - \frac{\theta}{2})$$

Where:

- T is the resultant force on the bend
- T_x is the component of thrust force in x-direction
- T_y is the component of thrust force in y-direction
- P is the maximum sustained pressure
- A is the pipe cross-sectional area
- θ is the bend deflection angle
- Δ is the angle between T and X-axis
- V is the fluid velocity

**THRUST FORCES ACTING
ON A BEND**



TYPICAL SOIL PARAMETERS

See Table 1 for typical values of soil parameters

$K_{oc} = 1.0$

PERMANENT WALL

$P_1 = K_{oc} \gamma'_c H$
 $P_w = \gamma_w H = 62.4 H$
 $P_q = 0.5 q$

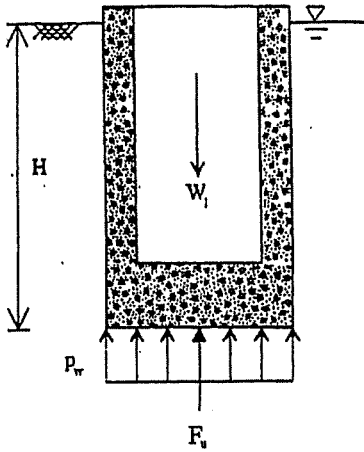
Where:

- γ'_c = Submerged unit weight of cohesive soil, pcf;
- K_{oc} = Coefficient of at-rest earth pressure in cohesive soil;
- γ_w = Unit weight of water, pcf;
- q = Surcharge load at surface, psf;
- P_0 = Lateral pressure, psf;
- P_1 = At-rest earth pressure, psf;
- P_q = Horizontal pressure due to surcharge, psf;
- P_w = Hydrostatic pressure due to groundwater, psf;
- H = Depth of excavation, feet

LATERAL EARTH PRESSURE DIAGRAM FOR PERMANENT WALL

SUBMERGED COHESIVE SOIL

(a) DEAD WEIGHT OF STRUCTURE



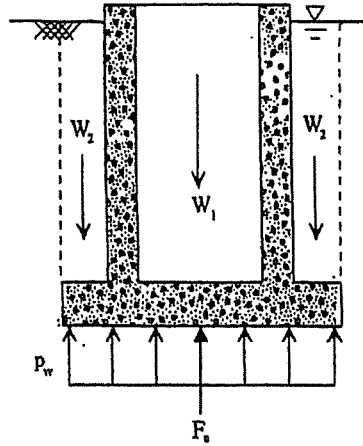
$$P_w = H\gamma_w$$

$$F_u = A_b P_w$$

$$\frac{W_1}{S_{f_1}} = F_u$$

See Table 1 for typical values of soil parameters

(b) WEIGHT OF SOIL ABOVE BASE EXTENSION PLUS DEAD WEIGHT OF STRUCTURE

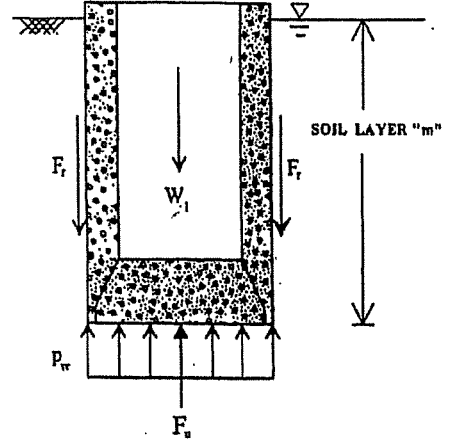


$$P_w = H\gamma_w$$

$$F_u = A_b P_w$$

$$\frac{W_1 + W_2}{S_{f_1}} = F_u$$

(c) SOIL-WALL FRICTION PLUS DEAD WEIGHT OF STRUCTURE



$$P_w = H\gamma_w$$

$$F_u = A_b P_w$$

$$\frac{W_1 + F_r}{S_{f_1}} = F_u$$

Predominantly Cohesive Soils, $F_r = \alpha c_m A_m$

Predominantly Cohesionless Soils, $F_r = p_m A_m K \tan \delta_m$

- Where:
- A_b = area of base, sq. ft.
 - A_m = cylindrical surface area of layer "m", sq. ft.
 - c_m = undrained cohesion of soil layer "m", psf.
 - F_u = hydrostatic uplift force, lbs.
 - F_r = frictional resistance, lbs.
 - H = height of buried structure, ft.
 - K = coefficient of lateral pressure = 0.5.
 - p_m = average overburden pressure for layer "m," psf.
 - P_w = hydrostatic uplift pressure, psf.
 - $S_{f_1, 2, 3}$ = factor of safety.
 - W_1 = dead weight of concrete structure, lbs.
 - W_2 = weight of backfill above base extension, lbs.
 - α = cohesion reduction factor = 0.5.
 - δ_m = friction angle between soil layer "m" and concrete wall, degrees = $0.75 \phi_m$
 - ϕ_m = internal angle of friction of soil layer "m", degrees.
 - γ_w = unit weight of water = 62.4 pcf.

UPLIFT PRESSURE AND RESISTANCE

TABLES

	<u>Table</u>
Geotechnical Design Parameter Summary: Open-Cut Excavation	1
Geotechnical Design Parameter Summary: Trenchless Installation.....	2

TABLE 1

**GEOTECHNICAL DESIGN PARAMETER SUMMARY
OPEN-CUT EXCAVATION**

Boring Nos.	Stratigraphic Unit	Range of Depths, ft	Wet Unit Weight, γ, pcf	Submerged Unit Weight, γ', pcf	Undrained Cohesion, psf	Internal Friction Angle, ϕ, degree
GB-1	FILL/Cohesive	0-4	129	65	750	--
thru	Cohesive	4-6	133	67	1,000	--
GB-5		6-10	133	67	500	--
		10-15	132	66	250	--

Notes:

1. Cohesive soils include fat clay, fat clay with sand, sandy fat clay, lean clay, and lean clay with sand.
2. Fill soils include fat clay, lean clay, and lean clay with sand and shell fragments.

TABLE 2
GEOTECHNICAL DESIGN PARAMETER SUMMARY
TRENCHLESS INSTALLATION ALONG TEXAS AVENUE (FM 1765)
(GB-1 THROUGH GB-5)

PROPERTY	COHESIVE SOILS ⁽¹⁾	
Wet Unit Weight, γ , pcf	0-4 ft.	129
	4-6 ft.	133
	6-10 ft.	133
	10-15 ft.	132
Submerged Unit Weight, γ' , pcf	0-4 ft.	65
	4-6 ft.	67
	6-10 ft.	67
	10-15 ft.	66
Moisture Content (%)	0-4 ft.	20
	4-6 ft.	20
	6-10 ft.	25
	10-15 ft.	23
UNDRAINED PROPERTIES *		
Undrained Cohesion, C_u , psf	0-4 ft.	750
	4-6 ft.	1,500
	6-10 ft.	500
	10-12 ft.	250
Angle of Internal, ϕ , degrees	0-4 ft.	0
	4-6 ft.	0
	6-10 ft.	0
	10-12 ft.	0
Elastic Modulus, E, psf	0-4 ft.	225,000
	4-6 ft.	450,000
	6-10 ft.	200,000
	10-12 ft.	100,000
Coefficient of Lateral Earth Pressure at Rest, K_o	0-4 ft.	1.2
	4-6 ft.	1.2
	6-10 ft.	1.2
	10-12 ft.	1.2
Poisson's Ratio	0.45	
DRAINED PROPERTIES *		
Drained Cohesion, C' , psf	0-4 ft.	0
	4-6 ft.	0
	6-10 ft.	0
	10-12 ft.	0
Angle of Internal Friction, ϕ' , degrees	0-4 ft.	25
	4-6 ft.	25
	6-10 ft.	27
	10-12 ft.	27
Elastic Modulus, E, psf	0-4 ft.	135,000
	4-6 ft.	270,000
	6-10 ft.	120,000
	10-12 ft.	60,000

Notes:

1. Cohesive soils include fat clay, fat clay with sand, sandy fat clay, lean clay, and lean clay with sand.
- * Tunnel zone which includes depth plus 6 feet above invert plus 6 feet below invert.

APPENDIX A

	<u>Figure</u>
Log of Borings.....	A-1 thru A-5
Symbols and Terms Used on Boring Logs	A-6

LOG OF BORING NO. GB-1

PROJECT : Paving Improvements along Texas Avenue (FM 1765)
 from 14th Street to 6th Street
 City of Texas City, Galveston County, Texas

PROJECT NO. : 1140243301

LOCATION : See Plan of Borings (Figure 2)

COMPLETION DEPTH : 15.0 FT.

SURFACE ELEVATION : Existing Grade

DATE : 04-10-19

ELEVATION, FEET	DEPTH, FEET	SYMBOL	SAMPLER : Shelby Tube/Split Spoon DRY AUGER : 0.0 TO 15.0 FT. WET ROTARY : -- TO -- FT.	DESCRIPTION OF MATERIAL	STANDARD PENETRATION TEST, BLOWS PER FOOT	PERCENT PASSING NO. 200 SIEVE	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	UNDRAINED SHEAR STRENGTH, TSF
												○ HAND PENETROMETER ● UNCONFINED COMPRESSION ■ UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION △ TORVANE 0.5 1.0 1.5 2.0 2.5
	0	[Pattern]		0.5" Asphalt over 8.5" Concrete				14.1				△ ○
	5	[Pattern]		FILL: gray lean clay w/calcareous and ferrous nodules		95.7		20.4	49	21	28	△ ○
	10	[Pattern]		Very stiff to hard gray LEAN CLAY (CL) w/calcareous and ferrous nodules and ferrous stains -very stiff 2'-4' -stiff 4'-8' -w/silt seams 6'-10'			105	24.8				■ ○
	15	[Pattern]		-medium stiff to stiff 8'-10' -very stiff 10'-12' -reddish brown and gray 10'-15' -medium stiff to stiff w/silt seams 13'-15'	94.6	104	26.1	48	21	27		△ ■ ○ △
	20	[Pattern]						24.0				○ △
	25	[Pattern]						26.4				○ △
	30	[Pattern]										
	35	[Pattern]										

DEPTH TO WATER IN BORING :
 NO GROUNDWATER ENCOUNTERED DURING DRILLING.
 HOLE OPEN TO 15.0 FT. AT END OF DRILLING.

Geotest Engineering, Inc.

FIGURE A-1

LOG OF BORING NO. GB-2

PROJECT : Paving Improvements along Texas Avenue (FM 1765)
 from 14th Street to 6th Street
 City of Texas City, Galveston County, Texas

PROJECT NO. : 1140243301

LOCATION : See Plan of Borings (Figure 2)

COMPLETION DEPTH : 15.0 FT.

SURFACE ELEVATION : Existing Grade

DATE : 04-10-19

ELEVATION, FEET	DEPTH, FEET	SYMBOL	SAMPLES	SAMPLER : Shelby Tube/Split Spoon DRY AUGER : 0.0 TO 15.0 FT. WET ROTARY : -- TO -- FT.	STANDARD PENETRATION TEST, BLOWS PER FOOT	PERCENT PASSING NO. 200 SIEVE	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	UNDRAINED SHEAR STRENGTH, TSF									
												O HAND PENETROMETER ● UNCONFINED COMPRESSION ■ UNCONSOLIDATED-UNDRAINED TRIAXIAL COMPRESSION Δ TORVANE 0.5 1.0 1.5 2.0 2.5									
				DESCRIPTION OF MATERIAL																	
	0			0.5" Asphalt over 8.5" Concrete				18.2													
	5			Stiff gray and brown LEAN CLAY WITH SAND (CL) w/ferrous stains -medium stiff to stiff 2'-4' -gray and yellowish brown 2'-15' -medium stiff 6'-8'		78.8	113	18.9	38	19	19										
	10			-medium stiff to stiff 8'-10' -stiff to very stiff 10'-12'		75.8	110	21.9	35	17	18										
	15							19.5													
	20							19.8													
	25																				
	30																				
	35																				

DEPTH TO WATER IN BORING :
 NO GROUNDWATER ENCOUNTERED DURING DRILLING.
 HOLE OPEN TO 15.0 FT. AT END OF DRILLING.

Geotest Engineering, Inc.

FIGURE A-2

LOG OF BORING NO. GB-3

PROJECT : Paving Improvements along Texas Avenue (FM 1765)
 from 14th Street to 6th Street
 City of Texas City, Galveston County, Texas

PROJECT NO. : 1140243301

LOCATION : See Plan of Borings (Figure 2)

COMPLETION DEPTH : 15.0 FT.

SURFACE ELEVATION : Existing Grade

DATE : 04-10-19

ELEVATION, FEET	DEPTH, FEET	SYMBOL	SAMPLES	DESCRIPTION OF MATERIAL	STANDARD PENETRATION TEST, BLOWS PER FOOT	PERCENT PASSING NO. 200 SIEVE	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	UNDRAINED SHEAR STRENGTH, TSF							
												0.5	1.0	1.5	2.0	2.5			
0				0.5" Asphalt over 8.75" Concrete				17.6											
				FILL: stiff to very stiff gray lean clay with sand and ferrous stains -w/shell fragments 9.25"-2' -medium stiff 2'-4'	75.6	26.0	49	21	28										
				Medium stiff to stiff yellowish brown LEAN CLAY WITH SAND (CL) w/ferrous nodules and ferrous stains -soft 6'-10' -w/silt seams 8'-12' -soft to medium stiff 10'-12'			112	22.6											
								27.5											
								24.8											
					74.3	103	24.7	33	17	16									
				-w/silty sand layer 13'-15'				20.9											

DEPTH TO WATER IN BORING :
 NO GROUNDWATER ENCOUNTERED DURING DRILLING.
 HOLE OPEN TO 15.0 FT. AT END OF DRILLING.

Geotest Engineering, Inc.

FIGURE A-3

LOG OF BORING NO. GB-4

PROJECT : Paving Improvements along Texas Avenue (FM 1765)
 from 14th Street to 6th Street
 City of Texas City, Galveston County, Texas

PROJECT NO. : 1140243301

LOCATION : See Plan of Borings (Figure 2)

COMPLETION DEPTH : 15.0 FT.

SURFACE ELEVATION : Existing Grade

DATE : 04-10-19

ELEVATION, FEET	DEPTH, FEET	SYMBOL	SAMPLES	DESCRIPTION OF MATERIAL	STANDARD PENETRATION TEST, BLOWS PER FOOT	PERCENT PASSING NO. 200 SIEVE	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	UNDRAINED SHEAR STRENGTH, TSF								
												0.5	1.0	1.5	2.0	2.5				
	0			0.5" Asphalt over 8" Concrete				20.1												
	5			FILL: soft to medium stiff dark gray fat clay w/limestone and shell fragments -stiff gray and brown 4'-6'	96.9	32.3	50	20	30											
	10			Soft yellowish brown and gray FAT CLAY WITH SAND (CH) w/ferrous nodules and ferrous stains -soft to medium stiff 8'-10'	75.6	29.5	53	22	31											
	15			-w/sand seams 13'-15'																
	20																			
	25																			
	30																			
	35																			

DEPTH TO WATER IN BORING :
 NO GROUNDWATER ENCOUNTERED DURING DRILLING.
 HOLE OPEN TO 15.0 FT. AT END OF DRILLING.

Geotest Engineering, Inc.

FIGURE A-4

LOG OF BORING NO. GB-5

PROJECT : Paving Improvements along Texas Avenue (FM 1765)
 from 14th Street to 6th Street
 City of Texas City, Galveston County, Texas

PROJECT NO. : 1140243301

LOCATION : See Plan of Borings (Figure 2)

COMPLETION DEPTH : 15.0 FT.

SURFACE ELEVATION : Existing Grade

DATE : 04-10-19
















ELEVATION, FEET	DEPTH, FEET	SYMBOL	DESCRIPTION OF MATERIAL	STANDARD PENETRATION TEST, BLOWS PER FOOT	PERCENT PASSING NO. 200 SIEVE	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	UNDRAINED SHEAR STRENGTH, TSF						
											0.5	1.0	1.5	2.0	2.5		
	0	●	0.5" Asphalt over 9" Concrete				17.0				○	△					
	5	●	Stiff to very stiff gray and brown SANDY FAT CLAY (CH) -w/shell fragments 9.5"-2' -w/calcareous and ferrous nodules 2'-4'	60.7	113	113	17.6	52	21	31	●	△					
	10	●	Soft to medium stiff brown LEAN CLAY WITH SAND (CL) w/ferrous nodules and ferrous stains -medium stiff to stiff 6'-8' -soft 8'-12'	82.7	112	112	24.2	30	17	13	△	●					
	15	●	-w/silty sand seams 13'-15'				26.1				○						
	20	●					22.9				○						
	25	●					29.7										
	30	●															
	35	●															

DEPTH TO WATER IN BORING :
 NO GROUNDWATER ENCOUNTERED DURING DRILLING.
 HOLE OPEN TO 15.0 FT. AT END OF DRILLING.

Geotest Engineering, Inc.

FIGURE A-5

SYMBOLS AND TERMS USED ON BORING LOGS

SOIL TYPES (SHOWN IN SYMBOL COLUMN)								SAMPLER TYPES (SHOWN IN SAMPLES COLUMN)						
														
Asphaltic Concrete	Fill	Gravel	Sand	SILT	FAT CLAY	LEAN CLAY	Sandy LEAN CLAY	Pitcher Barrel	Nx Core	Shelby Tube	Piston	Split Spoon	No Recovery	Auger

Predominant type shown heavy

TERMS DESCRIBING CONSISTENCY OR CONDITION

Basic Soil Type	Density or Consistency	Standard Penetration Resistance, ⁽¹⁾ Blows/ft.	Unconfined Compressive Strength (q _u), ⁽²⁾ Tons/sq. ft.
Cohesionless	Very loose	Less than 4	Not applicable
	Loose	4 to <10	Not applicable
	Medium dense	10 to <30	Not applicable
	Dense	30 to <50	Not applicable
	Very dense	50 or greater	Not applicable
Cohesive	Very soft	Less than 2	Less than 0.25
	Soft	2 to <4	0.25 to <0.5
	Firm/Medium stiff	4 to <8	0.5 to <1.0
	Stiff	8 to <15	1.0 to <2.0
	Very stiff	15 to <30	2.0 to <4.0
	Hard	30 or greater	4 or greater

(1) Number of blows from 140-lb. weight falling 30-in. to drive 2-in. OD, 1-3/8-in. ID, split barrel sampler (ASTM D1586)

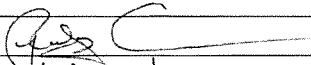
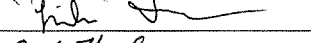
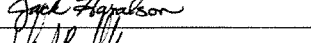
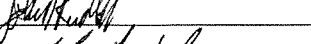
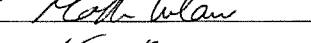
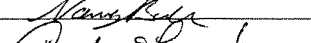
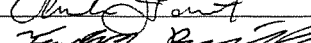
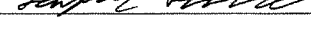
(2) q_u may also be approximated using a pocket penetrometer

TERMS CHARACTERIZING SOIL STRUCTURE

Parting: -paper thin in size	Seam: -1/8" to 3" thick	Layer: -greater than 3"
Slickensided	- having inclined planes of weakness that are slick and glossy in appearance.	
Fissured	- containing shrinkage cracks, frequently filled with fine sand or silt; usually more or less vertical.	
Laminated	- composed of thin layers of varying color and texture.	
Interbedded	- composed of alternate layers of different soil types.	
Calcareous	- containing appreciable quantities of calcium carbonate.	
Well graded	- having wide range in grain sizes and substantial amounts of all intermediate particle sizes.	
Poorly graded	- predominantly of one grain size, or having a range of sizes with some intermediate size missing.	
Flocculated	- pertaining to cohesive soils that exhibit a loose knit or flakey structure.	

PRE-BID CONFERENCE
 TEXAS AVENUE RECONSTRUCTION
 GALVESTON COUNTY, TEXAS

Pre-bid Conference for Bid #B201007 will be held on Monday, October 28, 2019 at Galveston County Courthouse, Purchasing Department, 722 Moody, 5th Floor, Galveston, TX

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